Installazione dell'Opera Artistica di Marinella Senatore nell'Area Archeologica di Santa Mustiola a Peccioli (PI)

PROGETTO ESECUTIVO

FONDAZIONE Peccioli per
COMUNE DI PECCIOLI • BELVEDERE SPA

P.za del Popolo, 10 – 56037, Peccioli (Pisa)

STRUTTURE - FASCICOLO DEI CALCOLI

Committente:
Fondazione Peccioli per l'Arte

Progetto opera artistica:
Marinella Senatore

Progettisti per la parte autorizzativa e di ingegnerizzazione dell'opera:
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Novembre 2026

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1 PREMESSA

La presente relazione si riferisce agli aspetti ingegneristici legati alla **Istallazione di un'opera d'arte di Marinella Senatore nell'area archeologica di Santa Mustiola**, in Loc. Ghizzano nel Comune di Peccioli (PI); l'opera rappresenta la riproduzione, in chiave più moderna e secondo l'ispirazione dell'artista, di una chiesa realmente esistita in epoca longobarda nel sito in oggetto, ed in effetti viene collocata proprio sopra gli scavi che ne hanno rivelato l'esistenza.

Tale documento contiene in forma estesa i calcoli e risulta a corredo della relazione tecnica elaborata secondo il capitolo 10 delle NTC 2018.

2 ANALISI E VERIFICHE DELLA STRUTTURA METALLICA

2.1 Modello "PE_ST_SANTAMUSTIOLA-GHIZZANO_R0"

Introduzione

Sistemi di riferimento
Le coordinate, i carichi concentrati, i cedimenti, le reazioni vincolari e gli spostamenti dei NODI sono riferiti ad una terna destra cartesiana globale con l'asse Z verticale rivolto verso l'alto.
I carichi in coordinate locali e le sollecitazioni delle ASTE sono riferite ad una terna destra cartesiana locale così definita:
- origine nel nodo iniziale dell'asta;
- asse X coincidente con l'asse dell'asta e con verso dal nodo iniziale al nodo finale;
- immaginando la trave a sezione rettangolare l'asse Y è parallelo alla base e l'asse Z è parallelo all'altezza. La rotazione dell'asta comporta quindi una rotazione di tutta la terna locale.

Si può immaginare la terna locale di un'asta comunque disposta nello spazio come derivante da quella globale dopo una serie di trasformazioni:
- una rotazione intorno all'asse Z che porti l'asse X a coincidere con la proiezione dell'asse dell'asta sul piano orizzontale;
- una traslazione lungo il nuovo asse X così definito in modo da portare l'origine a coincidere con la proiezione del nodo iniziale dell'asta sul piano orizzontale;
- una traslazione lungo l'asse Z che porti l'origine a coincidere con il nodo iniziale dell'asta;
- una rotazione intorno all'asse Y così definito che porti l'asse X a coincidere con l'asse dell'asta;
- una rotazione intorno all'asse X così definito pari alla rotazione dell'asta.

In pratica le travi prive di rotazione avranno sempre l'asse Z rivolto verso l'alto e l'asse Y nel piano del solaio, mentre i pilastri privi di rotazione avranno l'asse Y parallelo all'asse Y globale e l'asse Z parallelo ma controverso all'asse X globale. Da notare quindi che per i pilastri la "base" è il lato parallelo a Y.

Le sollecitazioni ed i carichi in coordinate locali negli ELEMENTI BIDIMENSIONALI e nei MURI sono riferiti ad una terna destra cartesiana locale così definita:
- origine nel primo nodo dell'elemento;
- asse X coincidente con la congiungente il primo ed il secondo nodo dell'elemento;
- asse Y definito come prodotto vettoriale fra il versore dell'asse X e il versore della congiungente il primo e il quarto nodo. Asse Z a formare con gli altri due una terna destrorsa.

Praticamente un elemento verticale con l'asse X locale coincidente con l'asse X globale ha anche gli altri assi locali coincidenti con quelli globali.

Rotazioni e momenti
Seguendo il principio adottato per tutti i carichi che sono positivi se CONTROVERSI agli assi, anche i momenti concentrati e le rotazioni impresse in coordinate globali risultano positivi se CONTROVERSI al segno positivo delle rotazioni. Il segno positivo dei momenti e delle rotazioni è quello orario per l'osservatore posto nell'origine: X ruota su Y, Y ruota su Z, Z ruota su X. In pratica è sufficiente adottare la regola della mano destra: col pollice rivolto nella direzione dell'asse, la rotazione che porta a chiudere il palmo della mano corrisponde al segno positivo.

Normativa di riferimento
La normativa di riferimento è la seguente:
- Legge n. 64 del 2/2/1974 - Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche.

- D.M. del 24/1/1986 - Norme tecniche relative alle costruzioni sismiche.

- Legge n. 1086 del 5/11/1971 - Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.

- D.M. del 14/2/1992 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 9/1/1996 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 16/1/1996 - Norme tecniche per le costruzioni in zone sismiche.

- Circolare n. 21745 del 30/7/1981 - Legge n. 219 del 14/5/1981 - Art. 10 - Istruzioni relative al rafforzamento degli edifici in muratura danneggiati dal sisma.

- Regione Autonoma Friuli Venezia Giulia - Legge Regionale n. 30 del 20/6/1977 - Documentazione tecnica per la progettazione e direzione delle opere di riparazione degli edifici - Documento Tecnico n. 2 - Raccomandazioni per la riparazione strutturale degli edifici in muratura.

- D.M. del 20/11/1987 - Norme Tecniche per la progettazione, esecuzione e collaudo degli edifici in

muratura e per il loro consolidamento.

- Norme Tecniche C.N.R. n. 10011-85 del 18/4/1985 - Costruzioni di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Norme Tecniche C.N.R. n. 10025-84 del 14/12/1984 - Istruzioni per il progetto, l'esecuzione ed il controllo delle strutture prefabbricate in conglomerato cementizio e per le strutture costruite con sistemi industrializzati di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Circolare n. 65 del 10/4/1997 - Istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. del 16/1/1996.

- DIN 1052 - Metodi di verifica per il legno.

- D.M. del 17/1/2018 - Norme tecniche per le costruzioni.

- Circolare n. 7 del 21/1/2019 - Istruzioni per l'applicazione dell'«Aggiornamento delle "Norme tecniche per le costruzioni"» di cui al decreto ministeriale 17 gennaio 2018.

- Documento Tecnico CNR-DT 200 R1/2012 - Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati.

- Eurocodice 2 - Progettazione delle strutture di calcestruzzo.

- Eurocodice 3 - Progettazione delle strutture in acciaio.

- Eurocodice 5 - Progettazione delle strutture di legno.

Unità di misura
Le unità di misura adottate sono le seguenti:
- lunghezze : m
- forze : daN
- masse : kg
- temperature : gradi centigradi
- angoli : gradi sessadecimali o radianti

ELENCO VINCOLI NODI

Simbologia

Comm. = Commento
Kt = Coeff. di sottofondo su suolo elastico alla Winkler
Ly = Lunghezza (dir. Y locale)
Lz = Larghezza (dir. Z locale)
RL = Rotazione libera
Rx = Rotazione intorno all'asse X (L=libera, B=bloccata, E=elastica)
Ry = Rotazione intorno all'asse Y (L=libera, B=bloccata, E=elastica)
Rz = Rotazione intorno all'asse Z (L=libera, B=bloccata, E=elastica)
Sx = Spostamento in dir. X (L=libero, B=bloccato, E=elastico)
Sy = Spostamento in dir. Y (L=libero, B=bloccato, E=elastico)
Sz = Spostamento in dir. Z (L=libero, B=bloccato, E=elastico)
Vn = Numero del vincolo nodo

Vn	Comm.	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly <m>	Lz <m>	Kt <daN/cmc>	Vn	Comm.	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly <m>	Lz <m>	Kt <daN/cmc>
1	Libero	L	L	L	L	L	L					2	Incastro	B	B	B	B	B	B				

ELENCO COSTANTI ELASTICHE NODALI

Simbologia

KRx = Costante elastica intorno all'asse X
KRy = Costante elastica intorno all'asse Y
KRz = Costante elastica intorno all'asse Z
Kx = Costante elastica in dir. X
Ky = Costante elastica in dir. Y
Kz = Costante elastica in dir. Z
Nodo = Numero del nodo

Nodo	Kx <daN/cm>	Ky <daN/cm>	Kz <daN/cm>	KRx <daNm/rad>	KRy <daNm/rad>	KRz <daNm/rad>	Nodo	Kx <daN/cm>	Ky <daN/cm>	Kz <daN/cm>	KRx <daNm/rad>	KRy <daNm/rad>	KRz <daNm/rad>

ELENCO NODI

Simbologia

Imp. = Numero dell'impalcato
Nodo = Numero del nodo
Vn = Numero del vincolo nodo
X = Coordinata X del nodo
Y = Coordinata Y del nodo
Z = Coordinata Z del nodo

Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn	Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn	Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn	Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn
-85	10.00	2.20	5.46	0	1	-84	8.60	2.20	5.46	0	1	-83	7.90	2.20	5.46	0	1	-82	7.20	2.20	5.46	0	1
-81	6.50	2.20	5.46	0	1	-80	5.80	2.20	5.46	0	1	-79	5.10	2.20	5.46	0	1	-78	4.40	2.20	5.46	0	1
-77	3.70	2.20	5.46	0	1	-76	3.00	2.20	5.46	0	1	-75	2.25	2.20	5.46	0	1	-74	1.50	2.20	5.46	0	1
-73	0.75	2.20	5.46	0	1	-72	0.00	2.20	5.46	0	1	-71	10.00	2.75	5.29	0	1	-70	6.50	2.75	5.29	0	1
-69	3.00	2.75	5.29	0	1	-68	0.00	2.75	5.29	0	1	-67	8.60	1.65	5.29	0	1	-66	7.90	1.65	5.29	0	1
-65	7.20	1.65	5.29	0	1	-64	6.50	1.65	5.29	0	1	-63	5.80	1.65	5.29	0	1	-62	5.10	1.65	5.29	0	1
-61	4.40	1.65	5.29	0	1	-60	3.70	1.65	5.29	0	1	-59	3.00	1.65	5.29	0	1	-58	2.25	1.65	5.29	0	1
-57	1.50	1.65	5.29	0	1	-56	0.75	1.65	5.29	0	1	-55	0.00	1.65	5.29	0	1	-54	10.00	3.30	5.11	0	1
-53	6.50	3.30	5.11	0	1	-52	3.00	3.30	5.11	0	1	-51	0.00	3.30	5.11	0	1	-50	10.00	1.10	5.11	0	1
-49	8.60	1.10	5.11	0	1	-48	7.20	1.10	5.11	0	1	-47	6.50	1.10	5.11	0	1	-46	5.80	1.10	5.11	0	1
-45	5.10	1.10	5.11	0	1	-44	4.40	1.10	5.11	0	1	-43	3.70	1.10	5.11	0	1	-42	3.00	1.10	5.11	0	1
-41	2.25	1.10	5.11	0	1	-40	1.50	1.10	5.11	0	1	-39	0.75	1.10	5.11	0	1	-38	0.00	1.10	5.11	0	1
-37	8.60	0.55	4.93	0	1	-36	7.90	0.55	4.93	0	1	-35	7.20	0.55	4.93	0	1	-34	6.50	0.55	4.93	0	1
-33	5.80	0.55	4.93	0	1	-32	5.10	0.55	4.93	0	1	-31	4.40	0.55	4.93	0	1	-30	3.70	0.55	4.93	0	1
-29	3.00	0.55	4.93	0	1	-28	2.25	0.55	4.93	0	1	-27	1.50	0.55	4.93	0	1	-26	8.60	0.00	4.76	2	1
-25	7.90	0.00	4.76	2	1	-24	1.50	0.00	4.76	2	1	-23	7.60	0.00	3.86	0	1	-22	7.20	0.00	3.86	0	1
-21	2.25	0.00	3.86	0	1	-20	1.85	0.00	3.86	0	1	-19	10.00	4.40	2.70	0	1	-18	3.00	4.40	2.70	0	1
-17	2.20	4.40	2.00	0	1	-16	0.00	4.40	2.00	0	1	-15	0.00	0.00	2.00	0	1	-14	0.00	4.40	1.50	0	1
-13	6.50	3.67	1.00	1	1	-12	3.00	3.67	1.00	1	1	-11	0.00	3.67	1.00	1	1	-10	6.50	2.95	1.00	1	1
-9	3.00	2.95	1.00	1	1	-8	6.50	2.20	1.00	1	1	-7	3.00	2.20	1.00	1	1	-6	0.00	2.20	1.00	1	1
-5	6.50	1.45	1.00	1	1	-4	3.00	1.45	1.00	1	1	-3	6.50	0.72	1.00	1	1	-2	3.00	0.72	1.00	1	1
-1	0.00	0.72	1.00	1	1	1	0.00	0.00	0.00	0	2	3	1.85	0.00	3.16	0	1	4	2.25	0.00	3.16	0	1
5	3.00	0.00	0.00	0	2	6	3.70	0.00	2.60	0	1	10	6.50	0.00	0.00	0	2	11	7.20	0.00	3.16	0	1
12	7.60	0.00	3.16	0	1	15	10.00	0.00	0.00	0	2	17	0.00	1.45	2.00	0	1	18	10.00	1.45	3.30	0	1
19	10.70	2.20	3.30	0	1	20	0.00	2.20	3.30	0	1	21	10.00	2.20	4.00	0	1	22	0.00	2.95	2.00	0	1
23	10.00	2.95	3.30	0	1	25	0.00	4.40	0.00	0	2	26	2.00	4.40	2.00	0	1	27	2.20	4.40	1.50	0	1
28	2.60	4.40	2.00	0	1	29	3.00	4.40	0.00	0	2	30	3.40	4.40	2.70	0	1	31	4.02	4.40	2.70	0	1
32	4.64	4.40	2.70	0	1	33	5.26	4.40	2.70	0	1	34	5.88	4.40	2.70	0	1	35	6.50	4.40	0.00	0	2
36	6.50	4.40	2.70	0	1	37	6.90	4.40	2.70	0	1	38	7.52	4.40	2.70	0	1	39	8.14	4.40	2.70	0	1
40	8.76	4.40	2.70	0	1	41	9.38	4.40	2.70	0	1	42	10.00	4.40	0.00	0	2	43	3.00	0.00	2.60	0	1
44	0.00	1.45	3.30	0	1	45	10.49	1.66	3.30	0	1	46	10.57	2.72	3.30	0	1	47					

```
0.00 2.95 3.30    0  1
  48 10.00 1.71 3.79    0  1     49 10.00 2.69 3.79    0  1    101  0.00 0.00 1.00    1  1    102
0.95 0.00 1.00    1  1
 103  1.85 0.00 1.00    1  1    104  2.25 0.00 1.00    1  1    105  3.00 0.00 1.00    1  1    106
3.70 0.00 1.00    1  1
 107  4.40 0.00 1.00    1  1    108  5.10 0.00 1.00    1  1    109  5.80 0.00 1.00    1  1    110
6.50 0.00 1.00    1  1
 111  7.20 0.00 1.00    1  1    112  7.60 0.00 1.00    1  1    113  8.40 0.00 1.00    1  1    114
9.20 0.00 1.00    1  1
 115 10.00 0.00 1.00    1  1    116 10.00 0.72 1.00    1  1    117  0.00 1.45 1.00    1  1    118
10.00 1.45 1.00    1  1
 119 10.70 2.20 1.00    0  1    122  0.00 2.95 1.00    1  1    123 10.00 2.95 1.00    1  1    124
10.00 3.67 1.00    1  1
 125  0.00 4.40 1.00    1  1    127  2.20 4.40 1.00    1  1    128  2.60 4.40 1.00    1  1    129
3.00 4.40 1.00    1  1
 130  3.40 4.40 1.00    0  1    135  6.50 4.40 1.00    1  1    142 10.00 4.40 1.00    1  1    143
10.49 1.66 1.00    1  1
 144 10.00 2.20 1.00    0  1    145 10.57 2.72 1.00    1  1    201  0.00 0.00 4.76    2  1    202
0.95 0.00 4.76    2  1
 203  1.85 0.00 4.76    2  1    204  2.25 0.00 4.76    2  1    205  3.00 0.00 4.76    2  1    206
3.70 0.00 4.76    2  1
 207  4.40 0.00 4.76    2  1    208  5.10 0.00 4.76    2  1    209  5.80 0.00 4.76    2  1    210
6.50 0.00 4.76    2  1
 211  7.20 0.00 4.76    2  1    212  7.60 0.00 4.76    2  1    213  8.40 0.00 4.76    2  1    214
9.20 0.00 4.76    2  1
 215 10.00 0.00 4.76    2  1    216 10.00 0.72 4.76    2  1    218 10.00 1.45 4.76    2  1    220
0.00 2.20 4.76    2  1
 221 10.00 2.20 4.76    2  1    223 10.00 2.95 4.76    2  1    224 10.00 3.67 4.76    2  1    225
0.00 4.40 4.76    2  1
 226  2.00 4.40 4.76    0  1    228  2.60 4.40 4.76    0  1    229  3.00 4.40 4.76    2  1    230
3.40 4.40 4.76    2  1
 231  4.02 4.40 4.76    2  1    232  4.64 4.40 4.76    2  1    233  5.26 4.40 4.76    2  1    234
5.88 4.40 4.76    2  1
 236  6.50 4.40 4.76    2  1    237  6.90 4.40 4.76    2  1    238  7.52 4.40 4.76    2  1    239
8.14 4.40 4.76    2  1
 240  8.76 4.40 4.76    2  1    241  9.38 4.40 4.76    2  1    242 10.00 4.40 4.76    2  1
```

ELENCO MATERIALI

Simbologia

α = Coeff. di dilatazione termica
ν = Coeff. di Poisson
Comm. = Commento
E = Modulo elastico
G = Modulo elastico tangenziale
Mat. = Materiale
P = Peso specifico

Mat.	Comm.	P <daN/mc>	E <daN/cmq>	G <daN/cmq>	ν	α
18	Acciaio	7850	2100000.00	800000.00	0.3	1.00E-05

ELENCO SEZIONI ASTE

Simbologia

A = Area
B = Base
C = Numero del criterio di progetto
Chy = Fattore di taglio rispetto all'asse Y
Chz = Fattore di taglio rispetto all'asse Z
Comm. = Commento
Crit. C.F. = Criterio di progetto collegamento finale
Crit. C.I. = Criterio di progetto collegamento iniziale
H = Altezza
Jx = Momento d'inerzia rispetto all'asse X
Jy = Momento d'inerzia rispetto all'asse Y
Jz = Momento d'inerzia rispetto all'asse Z
Ma = Numero del materiale
Mem. = Membratura
  G = Generica
  T = Trave
  P = Pilastro
Sez. = Numero della sezione
Tipo = Tipo sezione
  Ia = Inerzie assegnate

```
            Rc = Rettangolare cava
            Is = I stondata
Ver.      = Verifica prevista
            N = Nessuna
            A = Acciaio
a         = Spessore anima
r         = Raggio raccordo anima-ala
r1        = Raggio in testa ala
s         = Spessore

Sez.                Comm.                Tipo Mem. Ver.   B     H     s    a    r    s   r1      A
Chy         Chz          Jx             Jy             Jz       Ma  C Crit. C.I. Crit. C.F.
                                                        <cm>  <cm> <cm> <cm> <cm> <cm> <cm>   <cmq>
<cm4>          <cm4>          <cm4>
-------------------------------------------------------------------------------------------------------
-------------------------------------------------------------------------------------------------------
   1 Travi principali_sottostruttura     Is   T    A    18.00 17.10 0.95 0.60 1.50      0.00 --
18  1          1          1
   2 Travi principali_copertura          Is   T    A    20.00 20.00 1.50 0.90 1.80      0.00 --
18  2          1          1
   3 Travi secondarie_copertura          Is   T    A    12.00 11.40 0.80 0.50 1.20      0.00 --
18  3          1          1
   4 Colonne principali                  Is   P    A    20.00 20.00 1.50 0.90 1.80      0.00 --
18  4          1          1
   5 Traversi_facciata                   Is   T    A     7.30 14.00 0.69 0.47 0.70      0.00 --
18  5          1          1
   6 Montanti principali_facciata        Is   P    A     7.30 14.00 0.69 0.47 0.70      0.00 --
18  6          1          1
   7 Profili per pannelli_copertura      Rc   T    A     4.00  4.00               0.40      --
18  7          1          1
   8 Travi terziarie_copertura           Is   T    A     6.40 12.00 0.63 0.44 0.70      0.00 --
18  3          1          1
   9 Travi_facciata                      Is   T    A    14.00 13.30 0.85 0.55 1.20      0.00 --
18  5          1          1
  10 Travi secondarie_sottostruttura     Is   T    A    10.00 20.00 0.85 0.56 1.20      0.00 --
18  8          1          1
  11 Travi terziarie_sottostruttura      Is   T    A     8.20 16.00 0.74 0.50 0.90      0.00 --
18  9          1          1
  12 Montanti secondari                  Is   P    A     8.20 16.00 0.74 0.50 0.90      0.00 --
18 10          1          1
  13 inf rig                             Ia   G    N                                        1.000000
1000.000000 1000.000000      1.000E+13      1.000E+13      1.000E+12 18
  14 Montanti secondari_facciata vetrata Is   P    A    12.00 12.00 1.10 0.65 1.20      0.00 --
18 10          1          1
  15 Traversi secondari_facciata vetrata Is   T    A    12.00 12.00 1.10 0.65 1.20      0.00 --
18  5          1          1


ELENCO VINCOLI ASTE


Simbologia

Comm. = Commento
Kt    = Coeff. di sottofondo su suolo elastico alla Winkler
Mxf   = Momento intorno all'asse X locale nodo finale
Mxi   = Momento intorno all'asse X locale nodo iniziale
Myf   = Momento intorno all'asse Y locale nodo finale
Myi   = Momento intorno all'asse Y locale nodo iniziale
Mzf   = Momento intorno all'asse Z locale nodo finale
Mzi   = Momento intorno all'asse Z locale nodo iniziale
Nf    = Sforzo normale nodo finale
Ni    = Sforzo normale nodo iniziale
Tipo  = Tipologia
        SVI = Definizione di vincolamenti interni (L=libero, B=bloccato, valore svincolamento
parziale)
        ELA = Vincolo su suolo elastico alla Winkler
        BIE-RTC = Biella resistente a trazione e a compressione
        BIE-RC = Biella resistente solo a compressione
        BIE-RT = Biella resistente solo a trazione
        CP = Cerniera plastica (L=libero, B=bloccato, A=automatica, valori resistenza residua (b,c))
Tyf   = Taglio in dir. Y locale nodo finale
Tyi   = Taglio in dir. Y locale nodo iniziale
Tzf   = Taglio in dir. Z locale nodo finale
Tzi   = Taglio in dir. Z locale nodo iniziale
Va    = Numero del vincolo asta

Va    Comm.    Tipo Ni Tyi Tzi Mxi Myi Mzi Nf Tyf Tzf Mxf Myf Mzf     Kt
                                                                  <daN/cmc>
-------------------------------------------------------------------------
 1 Inc+Inc     SVI  B  B   B   B   B   B   B  B   B   B   B   B
```

11	Inc+CerYZ	SVI	B	B	B	B	B	B	B	B	B	L	L
12	CerYZ+Inc	SVI	B	B	B	B	L	L	B	B	B	B	B	B
13	CerYZ+CerYZ	SVI	B	B	B	B	L	L	B	B	B	B	L	L

ELENCO PARAMETRI AGGIUNTIVI ASTE

Simbologia

βx = Coeff. βx (D=default da criterio)
βy = Coeff. βy (D=default da criterio)
βz = Coeff. βz (D=default da criterio)
Comm. = Commento
Molt. Area = Moltiplicatore Area
Molt. Ay = Moltiplicatore Ay
Molt. Az = Moltiplicatore Az
Molt. Jy = Moltiplicatore Jy
Molt. Jz = Moltiplicatore Jz
Offy = Considerare offset Y
S = Sì
N = No
D = Default indicato in fase di calcolo
Offz = Considerare offset Z
S = Sì
N = No
D = Default indicato in fase di calcolo
Par. = Numero dei parametri aggiuntivi
Z.R. = Considerare zone rigide
S = Sì
N = No
D = Default indicato in fase di calcolo

Par.	Comm.	βx	βy	βz	Z.R.	Offy	Offz	Molt. Area	Molt. Jy	Molt. Jz	Molt. Ay	Molt. Az
1	Mensola	D	2.00	2.00	D	D	D	D	D	D	D	D

ELENCO ASTE

Simbologia

Asta = Numero dell'asta
Dy1 = Scost. filo fisso Y1
Dy2 = Scost. filo fisso Y2
Dz1 = Scost. filo fisso Z1
Dz2 = Scost. filo fisso Z2
FF = Filo fisso
Kt = Coeff. di sottofondo su suolo elastico alla Winkler
N1 = Nodo iniziale
N2 = Nodo finale
Par. = Numero dei parametri aggiuntivi
Rot. = Rotazione
Sez. = Numero della sezione
Va = Numero del vincolo asta

Asta	N1	N2	Sez.	Va	Par.	Rot. <grad>	FF	Dy1 <cm>	Dy2 <cm>	Dz1 <cm>	Dz2 <cm>	Kt <daN/cmc>
0	143	45		1		0.00	55	0.00	0.00	0.00	0.00	
0	145	46		1		0.00	55	0.00	0.00	0.00	0.00	
0	18	48	5	1		0.00	55	0.00	0.00	0.00	0.00	
0	48	21	5	1		0.00	55	0.00	0.00	0.00	0.00	
0	49	21	5	1		0.00	55	0.00	0.00	0.00	0.00	
0	23	49	5	1		0.00	55	0.00	0.00	0.00	0.00	
1	1	101	4	12		90.00	55	0.00	0.00	0.00	0.00	
1	101	-15	4	1		90.00	55	0.00	0.00	0.00	0.00	
1	-15	201	4	1		90.00	55	0.00	0.00	0.00	0.00	
2	102	202	12	13		90.00	55	0.00	0.00	0.00	0.00	
3	103	3	12	12		90.00	55	0.00	0.00	0.00	0.00	
3	3	-20	12	1		90.00	55	0.00	0.00	0.00	0.00	
3	-20	203	12	11		90.00	55	0.00	0.00	0.00	0.00	
4	104	4	12	12		90.00	55	0.00	0.00	0.00	0.00	
4	4	-21	12	1		90.00	55	0.00	0.00	0.00	0.00	
4	-21	204	12	11		90.00	55	0.00	0.00	0.00	0.00	
5	5	105	4	12		90.00	55	0.00	0.00	0.00	0.00	
5	105	43	4	1		90.00	55	0.00	0.00	0.00	0.00	
5	43	205	4	1		90.00	55	0.00	0.00	0.00	0.00	
6	106	6	12	12		90.00	55	0.00	0.00	0.00	0.00	
6	6	206	12	11		90.00	55	0.00	0.00	0.00	0.00	
7	107	207	12	13		90.00	55	0.00	0.00	0.00	0.00	

8	108	208	12	13	90.00	55	0.00	0.00	0.00	0.00
9	109	209	12	13	90.00	55	0.00	0.00	0.00	0.00
10	10	110	4	12	90.00	55	0.00	0.00	0.00	0.00
10	110	210	4	1	90.00	55	0.00	0.00	0.00	0.00
11	111	11	12	12	90.00	55	0.00	0.00	0.00	0.00
11	11	-22	12	1	90.00	55	0.00	0.00	0.00	0.00
11	-22	211	12	11	90.00	55	0.00	0.00	0.00	0.00
12	112	12	12	12	90.00	55	0.00	0.00	0.00	0.00
12	12	-23	12	1	90.00	55	0.00	0.00	0.00	0.00
12	-23	212	12	11	90.00	55	0.00	0.00	0.00	0.00
13	113	213	12	13	90.00	55	0.00	0.00	0.00	0.00
14	114	214	12	13	90.00	55	0.00	0.00	0.00	0.00
15	15	115	4	12	90.00	55	0.00	0.00	0.00	0.00
15	115	215	4	1	90.00	55	0.00	0.00	0.00	0.00
16	116	216	12	13	0.00	55	0.00	0.00	0.00	0.00
17	117	17	14	12	0.00	55	0.00	0.00	0.00	0.00
17	17	44	14	1	0.00	55	0.00	0.00	0.00	0.00
18	118	18	12	12	0.00	55	0.00	0.00	0.00	0.00
18	18	218	12	11	0.00	55	0.00	0.00	0.00	0.00
19	119	19	12	13	0.00	55	0.00	0.00	0.00	0.00
20	20	220	14	11	0.00	55	0.00	0.00	0.00	0.00
21	21	221	12	11	0.00	55	0.00	0.00	0.00	0.00
22	122	22	14	12	0.00	55	0.00	0.00	0.00	0.00
22	22	47	14	1	0.00	55	0.00	0.00	0.00	0.00
23	123	23	12	12	0.00	55	0.00	0.00	0.00	0.00
23	23	223	12	11	0.00	55	0.00	0.00	0.00	0.00
24	124	224	12	13	0.00	55	0.00	0.00	0.00	0.00
25	25	125	4	12	90.00	55	0.00	0.00	0.00	0.00
25	125	-14	4	1	90.00	55	0.00	0.00	0.00	0.00
25	-14	-16	4	1	90.00	55	0.00	0.00	0.00	0.00
25	-16	225	4	1	90.00	55	0.00	0.00	0.00	0.00
26	26	226	6	13	90.00	55	0.00	0.00	0.00	0.00
27	127	27	6	12	90.00	55	0.00	0.00	0.00	0.00
27	27	-17	6	11	90.00	55	0.00	0.00	0.00	0.00
28	128	28	12	12	90.00	55	0.00	0.00	0.00	0.00
28	28	228	12	11	90.00	55	0.00	0.00	0.00	0.00
29	29	129	4	12	90.00	55	0.00	0.00	0.00	0.00
29	129	-18	4	1	90.00	55	0.00	0.00	0.00	0.00
29	-18	229	4	1	90.00	55	0.00	0.00	0.00	0.00
30	130	30	6	13	90.00	55	0.00	0.00	0.00	0.00
30	30	230	6	13	90.00	55	0.00	0.00	0.00	0.00
31	31	231	6	13	90.00	55	0.00	0.00	0.00	0.00
32	32	232	6	13	90.00	55	0.00	0.00	0.00	0.00
33	33	233	6	13	90.00	55	0.00	0.00	0.00	0.00
34	34	234	6	13	90.00	55	0.00	0.00	0.00	0.00
35	35	135	4	12	90.00	55	0.00	0.00	0.00	0.00
36	36	236	6	13	90.00	55	0.00	0.00	0.00	0.00
37	37	237	6	13	90.00	55	0.00	0.00	0.00	0.00
38	38	238	6	13	90.00	55	0.00	0.00	0.00	0.00
39	39	239	6	13	90.00	55	0.00	0.00	0.00	0.00
40	40	240	6	13	90.00	55	0.00	0.00	0.00	0.00
41	41	241	6	13	90.00	55	0.00	0.00	0.00	0.00
42	42	142	4	12	90.00	55	0.00	0.00	0.00	0.00
42	142	-19	4	1	90.00	55	0.00	0.00	0.00	0.00
42	-19	242	4	1	90.00	55	0.00	0.00	0.00	0.00
1001	101	102	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	102	103	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	103	104	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	104	105	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	105	106	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	106	107	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	107	108	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	108	109	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	109	110	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	110	111	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	111	112	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	112	113	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	113	114	1	1	0.00	22	0.00	0.00	0.00	0.00
1001	114	115	1	1	0.00	22	0.00	0.00	0.00	0.00
1003	-1	-2	11	13	0.00	22	0.00	0.00	0.00	0.00
1003	-2	-3	11	13	0.00	22	0.00	0.00	0.00	0.00
1003	-3	116	11	13	0.00	22	0.00	0.00	0.00	0.00
1005	117	-4	11	13	0.00	22	0.00	0.00	0.00	0.00
1005	-4	-5	11	13	0.00	22	0.00	0.00	0.00	0.00
1005	-5	118	11	13	0.00	22	0.00	0.00	0.00	0.00
1007	-6	-7	11	13	0.00	22	0.00	0.00	0.00	0.00
1007	-7	-8	11	13	0.00	22	0.00	0.00	0.00	0.00
1007	-8	144	11	13	0.00	22	0.00	0.00	0.00	0.00
1009	122	-9	11	13	0.00	22	0.00	0.00	0.00	0.00
1009	-9	-10	11	13	0.00	22	0.00	0.00	0.00	0.00
1009	-10	123	11	13	0.00	22	0.00	0.00	0.00	0.00

1011	-11	-12	11	13	0.00	22	0.00	0.00	0.00	0.00
1011	-12	-13	11	13	0.00	22	0.00	0.00	0.00	0.00
1011	-13	124	11	13	0.00	22	0.00	0.00	0.00	0.00
1012	125	127	1	1	0.00	22	0.00	0.00	0.00	0.00
1012	127	128	1	1	0.00	22	0.00	0.00	0.00	0.00
1012	128	129	1	1	0.00	22	0.00	0.00	0.00	0.00
1012	129	130	1	1	0.00	22	0.00	0.00	0.00	0.00
1012	130	135	1	1	0.00	22	0.00	0.00	0.00	0.00
1012	135	142	1	1	0.00	22	0.00	0.00	0.00	0.00
1013	101	-1	1	1	0.00	22	0.00	0.00	0.00	0.00
1013	-1	117	1	1	0.00	22	0.00	0.00	0.00	0.00
1013	117	-6	1	1	0.00	22	0.00	0.00	0.00	0.00
1013	-6	122	1	1	0.00	22	0.00	0.00	0.00	0.00
1013	122	-11	1	1	0.00	22	0.00	0.00	0.00	0.00
1013	-11	125	1	1	0.00	22	0.00	0.00	0.00	0.00
1017	105	-2	10	1	0.00	22	0.00	0.00	0.00	0.00
1017	-2	-4	10	1	0.00	22	0.00	0.00	0.00	0.00
1017	-4	-7	10	1	0.00	22	0.00	0.00	0.00	0.00
1017	-7	-9	10	1	0.00	22	0.00	0.00	0.00	0.00
1017	-9	-12	10	1	0.00	22	0.00	0.00	0.00	0.00
1017	-12	129	10	1	0.00	22	0.00	0.00	0.00	0.00
1022	110	-3	10	1	0.00	22	0.00	0.00	0.00	0.00
1022	-3	-5	10	1	0.00	22	0.00	0.00	0.00	0.00
1022	-5	-8	10	1	0.00	22	0.00	0.00	0.00	0.00
1022	-8	-10	10	1	0.00	22	0.00	0.00	0.00	0.00
1022	-10	-13	10	1	0.00	22	0.00	0.00	0.00	0.00
1022	-13	135	10	1	0.00	22	0.00	0.00	0.00	0.00
1026	115	116	1	1	0.00	22	0.00	0.00	0.00	0.00
1026	116	118	1	1	0.00	22	0.00	0.00	0.00	0.00
1026	118	144	1	1	0.00	22	0.00	0.00	0.00	0.00
1026	144	123	1	1	0.00	22	0.00	0.00	0.00	0.00
1026	123	124	1	1	0.00	22	0.00	0.00	0.00	0.00
1026	124	142	1	1	0.00	22	0.00	0.00	0.00	0.00
1027	118	143	5	1	0.00	11	0.00	0.00	0.00	0.00
1028	143	119	5	1	0.00	11	0.00	0.00	0.00	0.00
1030	119	145	5	1	0.00	11	0.00	0.00	0.00	0.00
1031	145	123	5	1	0.00	11	0.00	0.00	0.00	0.00
2001	201	202	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	202	-24	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	-24	203	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	203	204	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	204	205	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	205	206	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	206	207	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	207	208	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	208	209	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	209	210	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	210	211	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	211	212	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	212	-25	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	-25	213	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	213	-26	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	-26	214	2	1	0.00	22	0.00	0.00	0.00	0.00
2001	214	215	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	225	226	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	226	228	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	228	229	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	229	230	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	230	231	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	231	232	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	232	233	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	233	234	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	234	236	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	236	237	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	237	238	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	238	239	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	239	240	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	240	241	2	1	0.00	22	0.00	0.00	0.00	0.00
2012	241	242	2	1	0.00	22	0.00	0.00	0.00	0.00
2013	201	220	2	1	0.00	22	0.00	0.00	0.00	0.00
2013	220	225	2	1	0.00	22	0.00	0.00	0.00	0.00
2017	205	229	2	1	0.00	22	0.00	0.00	0.00	0.00
2022	210	236	2	13	0.00	22	0.00	0.00	0.00	0.00
2026	215	216	2	1	0.00	22	0.00	0.00	0.00	0.00
2026	216	218	2	1	0.00	22	0.00	0.00	0.00	0.00
2026	218	221	2	1	0.00	22	0.00	0.00	0.00	0.00
2026	221	223	2	1	0.00	22	0.00	0.00	0.00	0.00
2026	223	224	2	1	0.00	22	0.00	0.00	0.00	0.00
2026	224	242	2	1	0.00	22	0.00	0.00	0.00	0.00
3002	-27	-28	7	13	17.65	22	0.00	0.00	0.00	0.00
3002	-28	-29	7	13	17.65	22	0.00	0.00	0.00	0.00
3002	-29	-30	7	13	17.65	22	0.00	0.00	0.00	0.00
3002	-30	-31	7	13	17.65	22	0.00	0.00	0.00	0.00

3002	-31	-32	7	13	17.65	22	0.00	0.00	0.00	0.00
3002	-32	-33	7	13	17.65	22	0.00	0.00	0.00	0.00
3002	-33	-34	7	13	17.65	22	0.00	0.00	0.00	0.00
3002	-34	-35	7	13	17.65	22	0.00	0.00	0.00	0.00
3002	-35	-36	7	12	17.65	22	0.00	0.00	0.00	0.00
3002	-36	-37	7	11	17.65	22	0.00	0.00	0.00	0.00
3004	-38	-39	3	12	17.65	22	0.00	0.00	0.00	0.00
3004	-39	-40	3	1	17.65	22	0.00	0.00	0.00	0.00
3004	-40	-41	3	1	17.65	22	0.00	0.00	0.00	0.00
3004	-41	-42	3	11	17.65	22	0.00	0.00	0.00	0.00
3004	-42	-43	3	12	17.65	22	0.00	0.00	0.00	0.00
3004	-43	-44	3	1	17.65	22	0.00	0.00	0.00	0.00
3004	-44	-45	3	1	17.65	22	0.00	0.00	0.00	0.00
3004	-45	-46	3	1	17.65	22	0.00	0.00	0.00	0.00
3004	-46	-47	3	11	17.65	22	0.00	0.00	0.00	0.00
3004	-47	-48	3	12	17.65	22	0.00	0.00	0.00	0.00
3004	-48	-49	3	1	17.65	22	0.00	0.00	0.00	0.00
3004	-49	-50	3	11	17.65	22	0.00	0.00	0.00	0.00
3006	-55	-56	3	12	17.65	22	0.00	0.00	0.00	0.00
3006	-56	-57	3	1	17.65	22	0.00	0.00	0.00	0.00
3006	-57	-58	3	1	17.65	22	0.00	0.00	0.00	0.00
3006	-58	-59	3	11	17.65	22	0.00	0.00	0.00	0.00
3006	-59	-60	3	12	17.65	22	0.00	0.00	0.00	0.00
3006	-60	-61	3	1	17.65	22	0.00	0.00	0.00	0.00
3006	-61	-62	3	1	17.65	22	0.00	0.00	0.00	0.00
3006	-62	-63	3	1	17.65	22	0.00	0.00	0.00	0.00
3006	-63	-64	3	11	17.65	22	0.00	0.00	0.00	0.00
3006	-64	-65	3	12	17.65	22	0.00	0.00	0.00	0.00
3006	-65	-66	3	1	17.65	22	0.00	0.00	0.00	0.00
3006	-66	-67	3	11	17.65	22	0.00	0.00	0.00	0.00
3007	-72	-73	3	12	0.00	22	0.00	0.00	0.00	0.00
3007	-73	-74	3	1	0.00	22	0.00	0.00	0.00	0.00
3007	-74	-75	3	1	0.00	22	0.00	0.00	0.00	0.00
3007	-75	-76	3	11	0.00	22	0.00	0.00	0.00	0.00
3007	-76	-77	3	12	0.00	22	0.00	0.00	0.00	0.00
3007	-77	-78	3	1	0.00	22	0.00	0.00	0.00	0.00
3007	-78	-79	3	1	0.00	22	0.00	0.00	0.00	0.00
3007	-79	-80	3	1	0.00	22	0.00	0.00	0.00	0.00
3007	-80	-81	3	11	0.00	22	0.00	0.00	0.00	0.00
3007	-81	-82	3	12	0.00	22	0.00	0.00	0.00	0.00
3007	-82	-83	3	1	0.00	22	0.00	0.00	0.00	0.00
3007	-83	-84	3	1	0.00	22	0.00	0.00	0.00	0.00
3007	-84	-85	3	11	0.00	22	0.00	0.00	0.00	0.00
3008	-68	-69	3	13	342.35	22	0.00	0.00	0.00	0.00
3010	-51	-52	3	13	342.35	22	0.00	0.00	0.00	0.00
3010	-52	-53	3	13	342.35	22	0.00	0.00	0.00	0.00
3010	-53	-54	3	13	342.35	22	0.00	0.00	0.00	0.00
3013	201	-38	2	1	0.00	22	0.00	0.00	0.00	0.00
3013	-38	-55	2	1	0.00	22	0.00	0.00	0.00	0.00
3013	-55	-72	2	1	0.00	22	0.00	0.00	0.00	0.00
3014	-39	-56	8	13	0.00	22	0.00	0.00	0.00	0.00
3014	-56	-73	8	13	0.00	22	0.00	0.00	0.00	0.00
3015	-24	-27	8	12	0.00	22	0.00	0.00	0.00	0.00
3015	-27	-40	8	11	0.00	22	0.00	0.00	0.00	0.00
3015	-40	-57	8	13	0.00	22	0.00	0.00	0.00	0.00
3015	-57	-74	8	13	0.00	22	0.00	0.00	0.00	0.00
3016	204	-28	8	12	0.00	22	0.00	0.00	0.00	0.00
3016	-28	-41	8	11	0.00	22	0.00	0.00	0.00	0.00
3017	205	-29	2	1	0.00	22	0.00	0.00	0.00	0.00
3017	-29	-42	2	1	0.00	22	0.00	0.00	0.00	0.00
3017	-42	-59	2	1	0.00	22	0.00	0.00	0.00	0.00
3017	-59	-76	2	1	0.00	22	0.00	0.00	0.00	0.00
3018	206	-30	8	12	0.00	22	0.00	0.00	0.00	0.00
3018	-30	-43	8	11	0.00	22	0.00	0.00	0.00	0.00
3019	207	-31	8	12	0.00	22	0.00	0.00	0.00	0.00
3019	-31	-44	8	11	0.00	22	0.00	0.00	0.00	0.00
3020	208	-32	8	12	0.00	22	0.00	0.00	0.00	0.00
3020	-32	-45	8	11	0.00	22	0.00	0.00	0.00	0.00
3021	209	-33	8	12	0.00	22	0.00	0.00	0.00	0.00
3021	-33	-46	8	11	0.00	22	0.00	0.00	0.00	0.00
3022	210	-34	2	12	0.00	22	0.00	0.00	0.00	0.00
3022	-34	-47	2	1	0.00	22	0.00	0.00	0.00	0.00
3022	-47	-64	2	1	0.00	22	0.00	0.00	0.00	0.00
3022	-64	-81	2	1	0.00	22	0.00	0.00	0.00	0.00
3023	211	-35	8	12	0.00	22	0.00	0.00	0.00	0.00
3023	-35	-48	8	11	0.00	22	0.00	0.00	0.00	0.00
3024	-25	-36	7	13	0.00	22	0.00	0.00	0.00	0.00
3025	-26	-37	3	12	0.00	22	0.00	0.00	0.00	0.00
3025	-37	-49	3	11	0.00	22	0.00	0.00	0.00	0.00
3025	-49	-67	3	12	0.00	22	0.00	0.00	0.00	0.00
3025	-67	-84	3	11	0.00	22	0.00	0.00	0.00	0.00

```
3026 215 -50    2  1        0.00 22 0.00 0.00 0.00 0.00
3026 -50 -85    2  1        0.00 22 0.00 0.00 0.00 0.00
3039 -70 -71    3 13      342.35 22 0.00 0.00 0.00 0.00
3044 -72 -68    2  1        0.00 22 0.00 0.00 0.00 0.00
3044 -68 -51    2  1        0.00 22 0.00 0.00 0.00 0.00
3044 -51 225    2  1        0.00 22 0.00 0.00 0.00 0.00
3047 -58 -75    8 13        0.00 22 0.00 0.00 0.00 0.00
3048 -76 -69    2  1        0.00 22 0.00 0.00 0.00 0.00
3048 -69 -52    2  1        0.00 22 0.00 0.00 0.00 0.00
3048 -52 229    2  1        0.00 22 0.00 0.00 0.00 0.00
3049 -60 -77    8 13        0.00 22 0.00 0.00 0.00 0.00
3050 -61 -78    8 13        0.00 22 0.00 0.00 0.00 0.00
3051 -62 -79    8 13        0.00 22 0.00 0.00 0.00 0.00
3052 -63 -80    8 13        0.00 22 0.00 0.00 0.00 0.00
3053 -81 -70    2  1        0.00 22 0.00 0.00 0.00 0.00
3053 -70 -53    2  1        0.00 22 0.00 0.00 0.00 0.00
3053 -53 236    2 11        0.00 22 0.00 0.00 0.00 0.00
3054 -65 -82    8 13        0.00 22 0.00 0.00 0.00 0.00
3055 -66 -83    8 13        0.00 22 0.00 0.00 0.00 0.00
3057 -85 -71    2  1        0.00 22 0.00 0.00 0.00 0.00
3057 -71 -54    2  1        0.00 22 0.00 0.00 0.00 0.00
3057 -54 242    2  1        0.00 22 0.00 0.00 0.00 0.00
5001 -20 -21    5 13       90.00 55 0.00 0.00 0.00 0.00
5012  27 -14    5 13       90.00 55 0.00 0.00 0.00 0.00
5013 -15  17   15 13       90.00 55 0.00 0.00 0.00 0.00
5027  18  45    5  1        0.00 11 0.00 0.00 0.00 0.00
5028  45  19    5  1        0.00 11 0.00 0.00 0.00 0.00
5029  19  21    5  1        0.00 55 0.00 0.00 0.00 0.00
5030  19  46    5  1        0.00 11 0.00 0.00 0.00 0.00
5031  46  23    5  1        0.00 11 0.00 0.00 0.00 0.00
5032   3   4    5 13       90.00 55 0.00 0.00 0.00 0.00
5043  26 -16    5 11       90.00 55 0.00 0.00 0.00 0.00
5043 -17  26    5  1       90.00 55 0.00 0.00 0.00 0.00
5043  28 -17    5 12       90.00 55 0.00 0.00 0.00 0.00
5044  44  20   13  1       90.00 55 0.00 0.00 0.00 0.00
5044  20  47   13  1       90.00 55 0.00 0.00 0.00 0.00
5063  43   6    5 13       90.00 55 0.00 0.00 0.00 0.00
5074  30 -18    9 11       90.00 55 0.00 0.00 0.00 0.00
5074  31  30    9  1       90.00 55 0.00 0.00 0.00 0.00
5074  32  31    9  1       90.00 55 0.00 0.00 0.00 0.00
5074  33  32    9  1       90.00 55 0.00 0.00 0.00 0.00
5074  34  33    9  1       90.00 55 0.00 0.00 0.00 0.00
5074  36  34    9  1       90.00 55 0.00 0.00 0.00 0.00
5074  37  36    9  1       90.00 55 0.00 0.00 0.00 0.00
5074  38  37    9  1       90.00 55 0.00 0.00 0.00 0.00
5074  39  38    9  1       90.00 55 0.00 0.00 0.00 0.00
5074  40  39    9  1       90.00 55 0.00 0.00 0.00 0.00
5074  41  40    9  1       90.00 55 0.00 0.00 0.00 0.00
5074 -19  41    9 12       90.00 55 0.00 0.00 0.00 0.00
5075  22 -16   15 13       90.00 55 0.00 0.00 0.00 0.00
5094  11  12    5 13       90.00 55 0.00 0.00 0.00 0.00
5125 -22 -23    5 13       90.00 55 0.00 0.00 0.00 0.00
```

ELENCO TIPI SOLAI

Simbologia

```
Comm.      = Commento
Lfl        = Larghezza fascia laterale
QA         = Primo carico accidentale
QA2        = Secondo carico accidentale
QA3        = Terzo carico accidentale
Qpn        = Carico permanente non strutturale
Qps        = Carico permanente strutturale
Rc         = Ripartizione carichi
             UN = Unidirezionale
             PP = A piastra perimetrale
Rip. int.  = Ripartizione su aste interne
Rip. ter.  = Ripartizione su aste terminali
Ts         = Numero del tipo solaio
s          = Coeff. di riduzione
```

Ts	Comm.	Rc	Qps <daN/mq>	Qpn <daN/mq>	QA <daN/mq>	QA2 <daN/mq>	QA3 <daN/mq>	Rip. ter.	Rip. int.	Lfl <m>	s
1	Tavolato in legno	PP	36.00	0.00	300.00	0.00	0.00	--	--	--	0.33
2	Copertura	UN	0.00	10.00	0.00	50.00	48.00	50.00	50.00	0.00	0.33

ELENCO SOLAI

Simbologia

Nodi = Nodi del solaio
Ord. = Orditura
Sol. = Numero del solaio
Ts = Numero del tipo solaio

Sol.	Ts	Ord. <grad>	Nodi	Sol.	Ts	Ord. <grad>	Nodi
100	1	0.00	-4 -5 -8 -7	101	1	0.00	-2 -3 -5 -4
102	1	0.00	105 106 107 108 109 110 -3 -2	103	1	0.00	101 102 103 104 105 -2 -1
104	1	0.00	-1 -2 -4 117	105	1	0.00	117 -4 -7 -6
106	1	0.00	-6 -7 -9 122	107	1	0.00	122 -9 -12 -11
108	1	0.00	-11 -12 129 128 127 125	109	1	0.00	-7 -8 -10 -9
110	1	0.00	-9 -10 -13 -12	111	1	0.00	-12 -13 135 130 129
112	1	0.00	-13 124 142 135	113	1	0.00	-10 123 124 -13
114	1	0.00	-8 144 123 -10	115	1	0.00	-5 118 144 -8
116	1	0.00	-3 116 118 -5	117	1	0.00	110 111 112 113 114 115 116 -3
300	2	0.00	-39 -40 -57 -56	301	2	0.00	-38 -39 -56 -55
302	2	0.00	210 211 -35 -34	303	2	0.00	-34 -35 -48 -47
304	2	0.00	209 210 -34 -33	305	2	0.00	-33 -34 -47 -46
306	2	0.00	-32 -33 -46 -45	307	2	0.00	208 209 -33 -32
308	2	0.00	207 208 -32 -31	309	2	0.00	-31 -32 -45 -44
310	2	0.00	-30 -31 -44 -43	311	2	0.00	206 207 -31 -30
312	2	0.00	205 206 -30 -29	313	2	0.00	-29 -30 -43 -42
314	2	0.00	-25 213 -26 -37 -36	315	2	0.00	204 205 -29 -28
316	2	0.00	-24 203 204 -28 -27	317	2	0.00	211 212 -25 -36 -35
318	2	0.00	-56 -57 -74 -73	319	2	0.00	-55 -56 -73 -72
320	2	0.00	-58 -59 -76 -75	321	2	0.00	-57 -58 -75 -74
322	2	0.00	-59 -60 -77 -76	323	2	0.00	-60 -61 -78 -77
324	2	0.00	-61 -62 -79 -78	325	2	0.00	-63 -64 -81 -80
326	2	0.00	-62 -63 -80 -79	327	2	0.00	-64 -65 -82 -81
328	2	0.00	-66 -67 -84 -83	329	2	0.00	-65 -66 -83 -82
330	2	90.00	-85 -84 -83 -82 -81 -70 -71	331	2	90.00	-71 -70 -53 -54
332	2	0.00	-28 -29 -42 -41	333	2	0.00	-27 -28 -41 -40
334	2	90.00	-76 -75 -74 -73 -72 -68 -69	335	2	90.00	-69 -68 -51 -52

ELENCO TIPI TAMPONATURE

Simbologia

Comm. = Commento
Crit. = Criterio di progetto
P = Puntoni equivalenti
  S = Genera i puntoni equivalenti
  N = Non genera i puntoni equivalenti
Qpn = Carico permanente non strutturale
Rcg = Ripartizione carichi gravitazionali
  AP = Sull'asta di piede
  AL = Sulle aste laterali
  APT = Sulle aste di piede e di testa
Rcv = Ripartizione carichi vento
  AL = Sulle aste laterali
  APT = Sulle aste di piede e di testa
Tipo = Tipologia
  C = Area di carico
  V = Area di carico e verifica
Tt = Numero del tipo tamponatura

Tt	Comm.	Qpn <daN/mq>	Rcg	Rcv	P	Tipo	Crit.	Tt	Comm.	Qpn <daN/mq>	Rcg	Rcv	P	Tipo	Crit.
1	Pannello Alucobond_vert	10.00	APT	APT	N	C	--	2	Pannello Alucobond_oriz	10.00	AL	AL	N	C	--

ELENCO TAMPONATURE

Simbologia

Nodi = Nodi della tamponatura
Tam. = Numero della tamponatura
Tt = Numero del tipo tamponatura

Tam.	Tt	Nodi	Tam.	Tt	Nodi
110	2	111 112 12 11	125	2	-19 41 241 242
136	2	124 142 -19 242 224	333	1	215 216 218 221 223 224 242 -54 -71 -85 -50
113	2	114 115 215 214	111	2	112 113 213 -25 212 -23 12
107	2	108 109 209 208	112	2	113 114 214 -26 213
106	2	107 108 208 207	131	1	225 220 20 47 22 -16
232	2	115 116 216 215	133	2	116 118 18 218 216
135	2	123 124 224 223 23	124	2	41 40 240 241
123	2	40 39 239 240	122	2	39 38 238 239
121	2	38 37 237 238	120	2	36 34 234 236
119	2	34 33 233 234	118	2	33 32 232 233
117	2	32 31 231 232	116	2	31 30 230 231
315	2	30 -18 229 230	215	2	30 -18 129 130
314	2	28 -17 26 226 228	115	2	28 -17 27 127 128
214	1	27 -14 -16 26 -17	114	1	27 -14 125 127
330	1	-51 -68 -72 -55 -38 201 220 225	132	1	-14 -16 22 122 -11 125
230	1	44 20 220 201 -15 17	130	1	17 -15 101 -1 117
109	2	110 111 11 -22 211 210	210	2	-22 -23 212 211
108	2	109 110 210 209	105	2	106 107 207 206 6
204	2	43 6 206 205	104	2	104 105 43 205 204 -21 4
103	2	103 104 4 3	203	2	-20 -21 204 203
102	2	102 103 3 -20 203 -24 202	101	2	101 102 202 201 -15
126	2	118 143 45 18	128	2	143 119 19 45
129	2	119 145 46 19	127	2	145 123 23 46
233	2	18 48 21 221 218	134	2	21 49 23 223 221

CONDIZIONI DI CARICO ELEMENTARI:

Simbologia

CCE = Numero della condizione di carico elementare
Comm. = Commento
Dir. = Direzione del vento
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Sic. = Contributo alla sicurezza
S = a sfavore
Tipo = Tipologia di pressione vento
M = Massimizzata
E = Esterna
I = Interna
Tipo CCE = Tipo di CCE per calcolo agli stati limite
Var. = Tipo di variabilità
B = di base
A = ambigua
s = Coeff. di riduzione (T.A. o S.L. D.M. 96)

Condizioni di carico elementari

CCE	Comm.	Tipo CCE	Sic.	Var.	s	Dir. <grad>	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
1	Permanenti strutturali	1	S	--	1.00	--	--	1.00	1.00	0.00	0.00	0.00	1.00
2	Permanenti non strutturali	2	S	--	1.00	--	--	1.00	1.00	0.00	0.00	0.00	1.00
3	Esercizio cat.C	5	S	B	1.00	--	--	1.00	1.00	0.00	0.00	0.00	1.00
4	Esercizio cat.H	10	S	B	1.00	--	--	1.00	1.00	0.00	0.00	0.00	1.00
5	Neve	12	S	B	1.00	--	--	1.00	1.00	0.00	0.00	0.00	1.00
6	Vento X+_1	11	S	A	1.00	0.00	M	--	--	--	--	--	--
7	Vento Y+_1	11	S	A	1.00	90.00	M	--	--	--	--	--	--
8	Vento X-_1	11	S	A	1.00	0.00	M	--	--	--	--	--	--
9	Vento Y-_1	11	S	A	1.00	90.00	M	--	--	--	--	--	--
10	Vento X+_2	11	S	A	1.00	0.00	M	--	--	--	--	--	--
11	Vento Y+_2	11	S	A	1.00	90.00	M	--	--	--	--	--	--
12	Vento X-_2	11	S	A	1.00	0.00	M	--	--	--	--	--	--
13	Vento Y-_2	11	S	A	1.00	90.00	M	--	--	--	--	--	--
14	Azione termica +	14	S	B	1.00	--	--	1.00	1.00	0.00	0.00	0.00	1.00
15	Azione termica -	14	S	B	1.00	--	--	1.00	1.00	0.00	0.00	0.00	1.00

ELENCO CARICHI NODI

CONDIZIONE DI CARICO 1: Permanenti strutturali

CARICHI CONCENTRATI

Simbologia

Fx = Componente X della forza applicata
Fy = Componente Y della forza applicata
Fz = Componente Z della forza applicata
Mx = Momento intorno all'asse X
My = Momento intorno all'asse Y
Mz = Momento intorno all'asse Z
Nodo = Numero del nodo

Nodo	Fx <daN>	Fy <daN>	Fz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>	Nodo	Fx <daN>	Fy <daN>	Fz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>
1	0.00	0.00	312.50	0.00	0.00	0.00	5	0.00	0.00	312.50	0.00	0.00	0.00
10	0.00	0.00	312.50	0.00	0.00	0.00	15	0.00	0.00	312.50	0.00	0.00	0.00
25	0.00	0.00	312.50	0.00	0.00	0.00	29	0.00	0.00	312.50	0.00	0.00	0.00
35	0.00	0.00	312.50	0.00	0.00	0.00	42	0.00	0.00	312.50	0.00	0.00	0.00

ELENCO CARICHI ASTE

CONDIZIONE DI CARICO 1: Permanenti strutturali

ELENCO PESO PROPRIO ASTE

Simbologia

A = Area
Comm. = Commento
Mat. = Materiale
P = Peso specifico
PL = Peso specifico a metro lineare
Sez. = Numero della sezione

Sez.	Comm.	A <cmq>	Mat.	P <daN/mc>	PL <daN/m>
1	Travi principali_sottostruttura	45.252600	Acciaio	7850.00	35.52
2	Travi principali_copertura	78.083000	Acciaio	7850.00	61.30
3	Travi secondarie_copertura	25.336900	Acciaio	7850.00	19.89
4	Colonne principali	78.083000	Acciaio	7850.00	61.30
5	Traversi_facciata	16.426300	Acciaio	7850.00	12.89
6	Montanti principali_facciata	16.426300	Acciaio	7850.00	12.89
7	Profili per pannelli_copertura	5.760000	Acciaio	7850.00	4.52
8	Travi terziarie_copertura	13.210500	Acciaio	7850.00	10.37
9	Travi_facciata	31.416900	Acciaio	7850.00	24.66
10	Travi secondarie_sottostruttura	28.484900	Acciaio	7850.00	22.36
11	Travi terziarie_sottostruttura	20.091700	Acciaio	7850.00	15.77
12	Montanti secondari	20.091700	Acciaio	7850.00	15.77
13	inf rig	1.000000	Acciaio	7850.00	0.79
14	Montanti secondari_facciata vetrata	34.006900	Acciaio	7850.00	26.70
15	Traversi secondari_facciata vetrata	34.006900	Acciaio	7850.00	26.70

CONDIZIONE DI CARICO 1: Permanenti strutturali

CARICHI DISTRIBUITI

Simbologia

Asta = Numero dell'asta
DC = Direzione del carico
  XG,YG,ZG = secondo gli assi globali
  XL,YL,ZL = secondo gli assi locali
E = Elemento provenienza del carico
  S = Solaio
  T = Tamponatura
N1 = Nodo iniziale
N2 = Nodo finale
NE = Numero elemento di provenienza del carico
Qf = Carico finale
Qi = Carico iniziale
T = Tipo di carico
  QA = Primo carico accidentale
  QA2 = Secondo carico accidentale
  QA3 = Terzo carico accidentale
  QPS = Carico permanente strutturale
  QPN = Carico permanente non strutturale
  VE = Vento
  M = Manuale

Xf = Distanza finale
Xi = Distanza iniziale

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
1001	101	102	S	103	QPS	ZG	0.00	10.51	0.95	10.51	1001	102	103	S	103	QPS	ZG	0.00	10.51	0.90	10.51
1001	103	104	S	103	QPS	ZG	0.00	10.51	0.40	10.51	1001	104	105	S	103	QPS	ZG	0.00	10.51	0.75	10.51
1001	105	106	S	102	QPS	ZG	0.00	10.81	0.70	10.81	1001	106	107	S	102	QPS	ZG	0.00	10.81	0.70	10.81
1001	107	108	S	102	QPS	ZG	0.00	10.81	0.70	10.81	1001	108	109	S	102	QPS	ZG	0.00	10.81	0.70	10.81
1001	109	110	S	102	QPS	ZG	0.00	10.81	0.70	10.81	1001	110	111	S	117	QPS	ZG	0.00	10.81	0.70	10.81
1001	111	112	S	117	QPS	ZG	0.00	10.81	0.40	10.81	1001	112	113	S	117	QPS	ZG	0.00	10.81	0.80	10.81
1001	113	114	S	117	QPS	ZG	0.00	10.81	0.80	10.81	1001	114	115	S	117	QPS	ZG	0.00	10.81	0.80	10.81
1003	-1	-2	S	103	QPS	ZG	0.00	10.51	3.00	10.51	1003	-1	-2	S	104	QPS	ZG	0.00	10.51	3.00	10.51
1003	-2	-3	S	101	QPS	ZG	0.00	10.81	3.50	10.81	1003	-2	-3	S	102	QPS	ZG	0.00	10.81	3.50	10.81
1003	-3	116	S	116	QPS	ZG	0.00	10.81	3.50	10.81	1003	-3	116	S	117	QPS	ZG	0.00	10.81	3.50	10.81
1005	117	-4	S	104	QPS	ZG	0.00	10.51	3.00	10.51	1005	117	-4	S	105	QPS	ZG	0.00	10.80	3.00	10.80
1005	-4	-5	S	100	QPS	ZG	0.00	11.12	3.50	11.12	1005	-4	-5	S	101	QPS	ZG	0.00	10.81	3.50	10.81
1005	-5	118	S	115	QPS	ZG	0.00	11.12	3.50	11.12	1005	-5	118	S	116	QPS	ZG	0.00	10.81	3.50	10.81
1007	-6	-7	S	105	QPS	ZG	0.00	10.80	3.00	10.80	1007	-6	-7	S	106	QPS	ZG	0.00	10.80	3.00	10.80
1007	-7	-8	S	100	QPS	ZG	0.00	11.12	3.50	11.12	1007	-7	-8	S	109	QPS	ZG	0.00	11.12	3.50	11.12
1007	-8	144	S	114	QPS	ZG	0.00	11.12	3.50	11.12	1007	-8	144	S	115	QPS	ZG	0.00	11.12	3.50	11.12
1009	122	-9	S	106	QPS	ZG	0.00	10.80	3.00	10.80	1009	122	-9	S	107	QPS	ZG	0.00	10.51	3.00	10.51
1009	-9	-10	S	109	QPS	ZG	0.00	11.12	3.50	11.12	1009	-9	-10	S	110	QPS	ZG	0.00	10.81	3.50	10.81
1009	-10	123	S	113	QPS	ZG	0.00	10.81	3.50	10.81	1009	-10	123	S	114	QPS	ZG	0.00	11.12	3.50	11.12
1011	-11	-12	S	107	QPS	ZG	0.00	10.51	3.00	10.51	1011	-11	-12	S	108	QPS	ZG	0.00	10.51	3.00	10.51
1011	-12	-13	S	110	QPS	ZG	0.00	10.81	3.50	10.81	1011	-12	-13	S	111	QPS	ZG	0.00	10.81	3.50	10.81
1011	-13	124	S	112	QPS	ZG	0.00	10.81	3.50	10.81	1011	-13	124	S	113	QPS	ZG	0.00	10.81	3.50	10.81
1012	125	127	S	108	QPS	ZG	0.00	10.51	2.20	10.51	1012	127	128	S	108	QPS	ZG	0.00	10.51	0.40	10.51
1012	128	129	S	108	QPS	ZG	0.00	10.51	0.40	10.51	1012	129	130	S	111	QPS	ZG	0.00	10.81	0.40	10.81
1012	130	135	S	111	QPS	ZG	0.00	10.81	3.10	10.81	1012	135	142	S	112	QPS	ZG	0.00	10.81	3.50	10.81
1013	101	-1	S	103	QPS	ZG	0.00	10.51	0.72	10.51	1013	-1	117	S	104	QPS	ZG	0.00	10.51	0.72	10.51
1013	117	-6	S	105	QPS	ZG	0.00	10.80	0.75	10.80	1013	-6	122	S	106	QPS	ZG	0.00	10.80	0.75	10.80
1013	122	-11	S	107	QPS	ZG	0.00	10.51	0.72	10.51	1013	-11	125	S	108	QPS	ZG	0.00	10.51	0.72	10.51
1017	105	-2	S	102	QPS	ZG	0.00	10.81	0.72	10.81	1017	105	-2	S	103	QPS	ZG	0.00	10.51	0.72	10.51
1017	-2	-4	S	101	QPS	ZG	0.00	10.81	0.72	10.81	1017	-2	-4	S	104	QPS	ZG	0.00	10.51	0.72	10.51
1017	-4	-7	S	100	QPS	ZG	0.00	11.12	0.75	11.12	1017	-4	-7	S	105	QPS	ZG	0.00	10.80	0.75	10.80
1017	-7	-9	S	106	QPS	ZG	0.00	10.80	0.75	10.80	1017	-7	-9	S	109	QPS	ZG	0.00	11.12	0.75	11.12
1017	-9	-12	S	107	QPS	ZG	0.00	10.51	0.72	10.51	1017	-9	-12	S	110	QPS	ZG	0.00	10.81	0.72	10.81
1017	-12	129	S	108	QPS	ZG	0.00	10.51	0.72	10.51	1017	-12	129	S	111	QPS	ZG	0.00	10.81	0.72	10.81
1022	110	-3	S	102	QPS	ZG	0.00	10.81	0.72	10.81	1022	110	-3	S	117	QPS	ZG	0.00	10.81	0.72	10.81
1022	-3	-5	S	101	QPS	ZG	0.00	10.81	0.72	10.81	1022	-3	-5	S	116	QPS	ZG	0.00	10.81	0.72	10.81
1022	-5	-8	S	100	QPS	ZG	0.00	11.12	0.75	11.12	1022	-5	-8	S	115	QPS	ZG	0.00	11.12	0.75	11.12

```
1022  -8 -10 S 109 QPS ZG 0.00   11.12 0.75   11.12   1022  -8 -10 S 114 QPS ZG 0.00   11.12 0.75
11.12
1022 -10 -13 S 110 QPS ZG 0.00   10.81 0.72   10.81   1022 -10 -13 S 113 QPS ZG 0.00   10.81 0.72
10.81
1022 -13 135 S 111 QPS ZG 0.00   10.81 0.72   10.81   1022 -13 135 S 112 QPS ZG 0.00   10.81 0.72
10.81
1026 115 116 S 117 QPS ZG 0.00   10.81 0.72   10.81   1026 116 118 S 116 QPS ZG 0.00   10.81 0.72
10.81
1026 118 144 S 115 QPS ZG 0.00   11.12 0.75   11.12   1026 144 123 S 114 QPS ZG 0.00   11.12 0.75
11.12
1026 123 124 S 113 QPS ZG 0.00   10.81 0.72   10.81   1026 124 142 S 112 QPS ZG 0.00   10.81 0.72
10.81


CONDIZIONE DI CARICO 2: Permanenti non strutturali

CARICHI DISTRIBUITI

Asta  N1  N2 E  NE  T  DC  Xi     Qi     Xf     Qf     Asta  N1  N2 E  NE  T  DC  Xi     Qi     Xf
Qf
                           <m> <daN/m>  <m> <daN/m>                           <m> <daN/m>  <m>
<daN/m>
-------------------------------------------------   -------------------------------------------
----
   0 143  45 T 126 QPN ZG 0.00    2.68 2.30    2.68      0 143  45 T 128 QPN ZG 0.00    2.91 2.30
2.91
   0 145  46 T 129 QPN ZG 0.00    2.67 2.30    2.67      0 145  46 T 127 QPN ZG 0.00    3.06 2.30
3.06
   0  18  48 T 233 QPN ZG 0.00    0.00 0.56    1.13      0  48  21 T 233 QPN ZG 0.00    0.49 0.54
1.44
   0  49  21 T 134 QPN ZG 0.00    0.49 0.54    1.44      0  23  49 T 134 QPN ZG 0.00    0.00 0.56
1.13
   1 101 -15 T 101 QPN ZG 0.00    4.75 1.00    4.75      1 -15 201 T 101 QPN ZG 0.00    4.75 2.76
4.75
   2 102 202 T 102 QPN ZG 0.00    4.50 3.76    4.50      2 102 202 T 101 QPN ZG 0.00    4.75 3.76
4.75
   3 103   3 T 103 QPN ZG 0.00    2.00 2.16    2.00      3 103   3 T 102 QPN ZG 0.00    4.50 2.16
4.50
   3   3 -20 T 102 QPN ZG 0.00    4.50 0.70    4.50      3 -20 203 T 203 QPN ZG 0.00    2.00 0.90
2.00
   3 -20 203 T 102 QPN ZG 0.00    4.50 0.90    4.50      4 104   4 T 104 QPN ZG 0.00    3.75 2.16
3.75
   4 104   4 T 103 QPN ZG 0.00    2.00 2.16    2.00      4   4 -21 T 104 QPN ZG 0.00    3.75 0.70
3.75
   4 -21 204 T 104 QPN ZG 0.00    3.75 0.90    3.75      4 -21 204 T 203 QPN ZG 0.00    2.00 0.90
2.00
   5 105  43 T 104 QPN ZG 0.00    3.75 1.60    3.75      5  43 205 T 204 QPN ZG 0.00    3.50 2.16
3.50
   5  43 205 T 104 QPN ZG 0.00    3.75 2.16    3.75      6 106   6 T 105 QPN ZG 0.00    3.50 1.60
3.50
   6   6 206 T 105 QPN ZG 0.00    3.50 2.16    3.50      6   6 206 T 204 QPN ZG 0.00    3.50 2.16
3.50
   7 107 207 T 106 QPN ZG 0.00    3.50 3.76    3.50      7 107 207 T 105 QPN ZG 0.00    3.50 3.76
3.50
   8 108 208 T 107 QPN ZG 0.00    3.50 3.76    3.50      8 108 208 T 106 QPN ZG 0.00    3.50 3.76
3.50
   9 109 209 T 107 QPN ZG 0.00    3.50 3.76    3.50      9 109 209 T 108 QPN ZG 0.00    3.50 3.76
3.50
  10 110 210 T 109 QPN ZG 0.00    3.50 3.76    3.50     10 110 210 T 108 QPN ZG 0.00    3.50 3.76
3.50
  11 111  11 T 110 QPN ZG 0.00    2.00 2.16    2.00     11 111  11 T 109 QPN ZG 0.00    3.50 2.16
3.50
  11  11 -22 T 109 QPN ZG 0.00    3.50 0.70    3.50     11 -22 211 T 109 QPN ZG 0.00    3.50 0.90
3.50
  11 -22 211 T 210 QPN ZG 0.00    2.00 0.90    2.00     12 112  12 T 110 QPN ZG 0.00    2.00 2.16
2.00
  12 112  12 T 111 QPN ZG 0.00    4.00 2.16    4.00     12  12 -23 T 111 QPN ZG 0.00    4.00 0.70
4.00
  12 -23 212 T 111 QPN ZG 0.00    4.00 0.90    4.00     12 -23 212 T 210 QPN ZG 0.00    2.00 0.90
2.00
  13 113 213 T 111 QPN ZG 0.00    4.00 3.76    4.00     13 113 213 T 112 QPN ZG 0.00    4.00 3.76
4.00
  14 114 214 T 113 QPN ZG 0.00    4.00 3.76    4.00     14 114 214 T 112 QPN ZG 0.00    4.00 3.76
4.00
  15 115 215 T 113 QPN ZG 0.00    4.00 3.76    4.00     15 115 215 T 232 QPN ZG 0.00    3.62 3.76
3.62
  16 116 216 T 232 QPN ZG 0.00    3.62 3.76    3.62     16 116 216 T 133 QPN ZG 0.00    3.62 3.76
3.62
  18 118  18 T 133 QPN ZG 0.00    3.62 2.30    3.62     18 118  18 T 126 QPN ZG 0.00    2.68 2.30
2.68
  18  18 218 T 133 QPN ZG 0.00    3.62 1.46    3.62     18  18 218 T 233 QPN ZG 0.70    3.75 1.46
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3.75
  18  18 218 T 233 QPN ZG 0.49    1.28 0.70    3.75     18  18 218 T 233 QPN ZG 0.00    0.00 0.49
1.28
  19 119  19 T 128 QPN ZG 0.00    2.91 2.30    2.91     19 119  19 T 129 QPN ZG 0.00    2.67 2.30
2.67
  21  21 221 T 233 QPN ZG 0.00    3.75 0.76    3.75     21  21 221 T 134 QPN ZG 0.00    3.75 0.76
3.75
  23 123  23 T 135 QPN ZG 0.00    3.62 2.30    3.62     23 123  23 T 127 QPN ZG 0.00    3.06 2.30
3.06
  23  23 223 T 135 QPN ZG 0.00    3.62 1.46    3.62     23  23 223 T 134 QPN ZG 0.70    3.75 1.46
3.75
  23  23 223 T 134 QPN ZG 0.49    1.28 0.70    3.75     23  23 223 T 134 QPN ZG 0.00    0.00 0.49
1.28
  24 124 224 T 136 QPN ZG 0.00    3.62 3.76    3.62     24 124 224 T 135 QPN ZG 0.00    3.62 3.76
3.62
  26  26 226 T 314 QPN ZG 0.00    3.00 2.76    3.00     27 127  27 T 115 QPN ZG 0.00    2.00 0.50
2.00
  27  27 -17 T 115 QPN ZG 0.00    2.00 0.50    2.00     28 128  28 T 115 QPN ZG 0.00    2.00 1.00
2.00
  28  28 228 T 314 QPN ZG 0.00    3.00 2.76    3.00     29 129 -18 T 215 QPN ZG 0.00    2.00 1.70
2.00
  29 -18 229 T 315 QPN ZG 0.00    2.00 2.06    2.00     30 130  30 T 215 QPN ZG 0.00    2.00 1.70
2.00
  30  30 230 T 116 QPN ZG 0.00    3.10 2.06    3.10     30  30 230 T 315 QPN ZG 0.00    2.00 2.06
2.00
  31  31 231 T 117 QPN ZG 0.00    3.10 2.06    3.10     31  31 231 T 116 QPN ZG 0.00    3.10 2.06
3.10
  32  32 232 T 118 QPN ZG 0.00    3.10 2.06    3.10     32  32 232 T 117 QPN ZG 0.00    3.10 2.06
3.10
  33  33 233 T 119 QPN ZG 0.00    3.10 2.06    3.10     33  33 233 T 118 QPN ZG 0.00    3.10 2.06
3.10
  34  34 234 T 120 QPN ZG 0.00    3.10 2.06    3.10     34  34 234 T 119 QPN ZG 0.00    3.10 2.06
3.10
  36  36 236 T 120 QPN ZG 0.00    3.10 2.06    3.10     37  37 237 T 121 QPN ZG 0.00    3.10 2.06
3.10
  38  38 238 T 122 QPN ZG 0.00    3.10 2.06    3.10     38  38 238 T 121 QPN ZG 0.00    3.10 2.06
3.10
  39  39 239 T 123 QPN ZG 0.00    3.10 2.06    3.10     39  39 239 T 122 QPN ZG 0.00    3.10 2.06
3.10
  40  40 240 T 124 QPN ZG 0.00    3.10 2.06    3.10     40  40 240 T 123 QPN ZG 0.00    3.10 2.06
3.10
  41  41 241 T 125 QPN ZG 0.00    3.10 2.06    3.10     41  41 241 T 124 QPN ZG 0.00    3.10 2.06
3.10
  42 142 -19 T 136 QPN ZG 0.00    3.62 1.70    3.62     42 -19 242 T 125 QPN ZG 0.00    3.10 2.06
3.10
  42 -19 242 T 136 QPN ZG 0.00    3.62 2.06    3.62   1012 125 127 T 114 QPN ZG 0.00    2.50 2.20
2.50
1013 101  -1 T 130 QPN ZG 0.00    5.00 0.72    5.00   1013  -1 117 T 130 QPN ZG 0.00    5.00 0.72
5.00
1013 122 -11 T 132 QPN ZG 0.00    5.00 0.72    5.00   1013 -11 125 T 132 QPN ZG 0.00    5.00 0.72
5.00
2013 201 220 T 330 QPN ZG 0.00    0.00 2.20    3.50   2013 201 220 T 230 QPN ZG 1.45    7.30 2.20
7.30
2013 201 220 T 230 QPN ZG 0.00   13.80 1.45   13.80   2013 220 225 T 131 QPN ZG 0.00    7.30 0.75
7.30
2013 220 225 T 330 QPN ZG 0.00    3.50 2.20    0.00   2013 220 225 T 131 QPN ZG 0.75   13.80 2.20
13.80
2026 215 216 T 333 QPN ZG 0.00    0.00 0.72    1.15   2026 216 218 T 333 QPN ZG 0.00    1.15 0.72
2.31
2026 218 221 T 333 QPN ZG 0.00    2.31 0.75    3.50   2026 221 223 T 333 QPN ZG 0.00    3.50 0.75
2.31
2026 223 224 T 333 QPN ZG 0.00    2.31 0.72    1.15   2026 224 242 T 333 QPN ZG 0.00    1.15 0.72
0.00
3007 -72 -73 S 334 QPN ZG 0.00    2.89 0.75    2.89   3007 -73 -74 S 334 QPN ZG 0.00    2.89 0.75
2.89
3007 -74 -75 S 334 QPN ZG 0.00    2.89 0.75    2.89   3007 -75 -76 S 334 QPN ZG 0.00    2.89 0.75
2.89
3007 -81 -82 S 330 QPN ZG 0.00    2.89 0.70    2.89   3007 -82 -83 S 330 QPN ZG 0.00    2.89 0.70
2.89
3007 -83 -84 S 330 QPN ZG 0.00    2.89 0.70    2.89   3007 -84 -85 S 330 QPN ZG 0.00    2.89 1.40
2.89
3008 -68 -69 S 334 QPN ZG 0.00    2.89 3.00    2.89   3008 -68 -69 S 335 QPN ZG 0.00    2.89 3.00
2.89
3010 -51 -52 S 335 QPN ZG 0.00    2.89 3.00    2.89   3010 -53 -54 S 331 QPN ZG 0.00    2.89 3.50
2.89
3013 201 -38 T 330 QPN ZG 0.00    0.00 1.15    1.67   3013 -38 -55 S 301 QPN ZG 0.00    3.75 0.58
3.75
3013 -38 -55 T 330 QPN ZG 0.00    1.67 0.58    2.50   3013 -55 -72 S 319 QPN ZG 0.00    3.75 0.58
3.75
3013 -55 -72 T 330 QPN ZG 0.00    2.50 0.58    3.34   3014 -39 -56 S 300 QPN ZG 0.00    3.75 0.58
3.75
3014 -39 -56 S 301 QPN ZG 0.00    3.75 0.58    3.75   3014 -56 -73 S 318 QPN ZG 0.00    3.75 0.58
3.75
```

3014 -56 -73 S 319 QPN ZG 0.00 3.75 0.58 3.75 3015 -24 -27 S 316 QPN ZG 0.00 3.75 0.58
3.75
3015 -27 -40 S 333 QPN ZG 0.00 3.75 0.58 3.75 3015 -40 -57 S 300 QPN ZG 0.00 3.75 0.58
3.75
3015 -57 -74 S 318 QPN ZG 0.00 3.75 0.58 3.75 3015 -57 -74 S 321 QPN ZG 0.00 3.75 0.58
3.75
3016 204 -28 S 315 QPN ZG 0.00 3.75 0.58 3.75 3016 204 -28 S 316 QPN ZG 0.00 3.75 0.58
3.75
3016 -28 -41 S 332 QPN ZG 0.00 3.75 0.58 3.75 3016 -28 -41 S 333 QPN ZG 0.00 3.75 0.58
3.75
3017 205 -29 S 312 QPN ZG 0.00 3.50 0.58 3.50 3017 205 -29 S 315 QPN ZG 0.00 3.75 0.58
3.75
3017 -29 -42 S 313 QPN ZG 0.00 3.50 0.58 3.50 3017 -29 -42 S 332 QPN ZG 0.00 3.75 0.58
3.75
3017 -59 -76 S 320 QPN ZG 0.00 3.75 0.58 3.75 3017 -59 -76 S 322 QPN ZG 0.00 3.50 0.58
3.50
3018 206 -30 S 311 QPN ZG 0.00 3.50 0.58 3.50 3018 206 -30 S 312 QPN ZG 0.00 3.50 0.58
3.50
3018 -30 -43 S 310 QPN ZG 0.00 3.50 0.58 3.50 3018 -30 -43 S 313 QPN ZG 0.00 3.50 0.58
3.50
3019 207 -31 S 308 QPN ZG 0.00 3.50 0.58 3.50 3019 207 -31 S 311 QPN ZG 0.00 3.50 0.58
3.50
3019 -31 -44 S 309 QPN ZG 0.00 3.50 0.58 3.50 3019 -31 -44 S 310 QPN ZG 0.00 3.50 0.58
3.50
3020 208 -32 S 307 QPN ZG 0.00 3.50 0.58 3.50 3020 208 -32 S 308 QPN ZG 0.00 3.50 0.58
3.50
3020 -32 -45 S 306 QPN ZG 0.00 3.50 0.58 3.50 3020 -32 -45 S 309 QPN ZG 0.00 3.50 0.58
3.50
3021 209 -33 S 304 QPN ZG 0.00 3.50 0.58 3.50 3021 209 -33 S 307 QPN ZG 0.00 3.50 0.58
3.50
3021 -33 -46 S 305 QPN ZG 0.00 3.50 0.58 3.50 3021 -33 -46 S 306 QPN ZG 0.00 3.50 0.58
3.50
3022 210 -34 S 302 QPN ZG 0.00 3.50 0.58 3.50 3022 210 -34 S 304 QPN ZG 0.00 3.50 0.58
3.50
3022 -34 -47 S 303 QPN ZG 0.00 3.50 0.58 3.50 3022 -34 -47 S 305 QPN ZG 0.00 3.50 0.58
3.50
3022 -64 -81 S 325 QPN ZG 0.00 3.50 0.58 3.50 3022 -64 -81 S 327 QPN ZG 0.00 3.50 0.58
3.50
3023 211 -35 S 302 QPN ZG 0.00 3.50 0.58 3.50 3023 211 -35 S 317 QPN ZG 0.00 3.50 0.58
3.50
3023 -35 -48 S 303 QPN ZG 0.00 3.50 0.58 3.50 3024 -25 -36 S 314 QPN ZG 0.00 3.50 0.58
3.50
3024 -25 -36 S 317 QPN ZG 0.00 3.50 0.58 3.50 3025 -26 -37 S 314 QPN ZG 0.00 3.50 0.58
3.50
3025 -67 -84 S 328 QPN ZG 0.00 3.50 0.58 3.50 3026 215 -50 T 333 QPN ZG 0.00 0.00 1.15
1.67
3026 -50 -85 T 333 QPN ZG 0.00 1.67 1.15 3.34 3039 -70 -71 S 330 QPN ZG 0.00 2.89 3.50
2.89
3039 -70 -71 S 331 QPN ZG 0.00 2.89 3.50 2.89 3044 -72 -68 T 330 QPN ZG 0.00 3.34 0.58
2.50
3044 -68 -51 T 330 QPN ZG 0.00 2.50 0.58 1.67 3044 -51 225 T 330 QPN ZG 0.00 1.67 1.15
0.00
3047 -58 -75 S 320 QPN ZG 0.00 3.75 0.58 3.75 3047 -58 -75 S 321 QPN ZG 0.00 3.75 0.58
3.75
3049 -60 -77 S 322 QPN ZG 0.00 3.50 0.58 3.50 3049 -60 -77 S 323 QPN ZG 0.00 3.50 0.58
3.50
3050 -61 -78 S 323 QPN ZG 0.00 3.50 0.58 3.50 3050 -61 -78 S 324 QPN ZG 0.00 3.50 0.58
3.50
3051 -62 -79 S 324 QPN ZG 0.00 3.50 0.58 3.50 3051 -62 -79 S 326 QPN ZG 0.00 3.50 0.58
3.50
3052 -63 -80 S 325 QPN ZG 0.00 3.50 0.58 3.50 3052 -63 -80 S 326 QPN ZG 0.00 3.50 0.58
3.50
3054 -65 -82 S 327 QPN ZG 0.00 3.50 0.58 3.50 3054 -65 -82 S 329 QPN ZG 0.00 3.50 0.58
3.50
3055 -66 -83 S 328 QPN ZG 0.00 3.50 0.58 3.50 3055 -66 -83 S 329 QPN ZG 0.00 3.50 0.58
3.50
3057 -85 -71 T 333 QPN ZG 0.00 3.34 0.58 2.50 3057 -71 -54 T 333 QPN ZG 0.00 2.50 0.58
1.67
3057 -54 242 T 333 QPN ZG 0.00 1.67 1.15 0.00 5012 27 -14 T 214 QPN ZG 0.00 2.50 2.20
2.50
5012 27 -14 T 114 QPN ZG 0.00 2.50 2.20 2.50 5013 -15 17 T 230 QPN ZG 0.00 13.80 1.45
13.80
5013 -15 17 T 130 QPN ZG 0.00 5.00 1.45 5.00 5043 26 -16 T 214 QPN ZG 0.00 2.50 2.00
2.50
5043 -17 26 T 214 QPN ZG 0.00 2.50 0.20 2.50 5044 44 20 T 230 QPN ZG 0.00 7.30 0.75
7.30
5044 20 47 T 131 QPN ZG 0.00 7.30 0.75 7.30 5075 22 -16 T 131 QPN ZG 0.00 13.80 1.45
13.80
5075 22 -16 T 132 QPN ZG 0.00 5.00 1.45 5.00

CONDIZIONE DI CARICO 3: Esercizio cat.C

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
1001	101	102	S	103	QA	ZG	0.00	87.58	0.95	87.58	1001	102	103	S	103	QA	ZG	0.00	87.58	0.90	87.58
1001	103	104	S	103	QA	ZG	0.00	87.58	0.40	87.58	1001	104	105	S	103	QA	ZG	0.00	87.58	0.75	87.58
1001	105	106	S	102	QA	ZG	0.00	90.09	0.70	90.09	1001	106	107	S	102	QA	ZG	0.00	90.09	0.70	90.09
1001	107	108	S	102	QA	ZG	0.00	90.09	0.70	90.09	1001	108	109	S	102	QA	ZG	0.00	90.09	0.70	90.09
1001	109	110	S	102	QA	ZG	0.00	90.09	0.70	90.09	1001	110	111	S	117	QA	ZG	0.00	90.09	0.70	90.09
1001	111	112	S	117	QA	ZG	0.00	90.09	0.40	90.09	1001	112	113	S	117	QA	ZG	0.00	90.09	0.80	90.09
1001	113	114	S	117	QA	ZG	0.00	90.09	0.80	90.09	1001	114	115	S	117	QA	ZG	0.00	90.09	0.80	90.09
1003	-1	-2	S	103	QA	ZG	0.00	87.58	3.00	87.58	1003	-1	-2	S	104	QA	ZG	0.00	87.58	3.00	87.58
1003	-2	-3	S	101	QA	ZG	0.00	90.09	3.50	90.09	1003	-2	-3	S	102	QA	ZG	0.00	90.09	3.50	90.09
1003	-3	116	S	116	QA	ZG	0.00	90.09	3.50	90.09	1003	-3	116	S	117	QA	ZG	0.00	90.09	3.50	90.09
1005	117	-4	S	104	QA	ZG	0.00	87.58	3.00	87.58	1005	117	-4	S	105	QA	ZG	0.00	90.00	3.00	90.00
1005	-4	-5	S	100	QA	ZG	0.00	92.65	3.50	92.65	1005	-4	-5	S	101	QA	ZG	0.00	90.09	3.50	90.09
1005	-5	118	S	115	QA	ZG	0.00	92.65	3.50	92.65	1005	-5	118	S	116	QA	ZG	0.00	90.09	3.50	90.09
1007	-6	-7	S	105	QA	ZG	0.00	90.00	3.00	90.00	1007	-6	-7	S	106	QA	ZG	0.00	90.00	3.00	90.00
1007	-7	-8	S	100	QA	ZG	0.00	92.65	3.50	92.65	1007	-7	-8	S	109	QA	ZG	0.00	92.65	3.50	92.65
1007	-8	144	S	114	QA	ZG	0.00	92.65	3.50	92.65	1007	-8	144	S	115	QA	ZG	0.00	92.65	3.50	92.65
1009	122	-9	S	106	QA	ZG	0.00	90.00	3.00	90.00	1009	122	-9	S	107	QA	ZG	0.00	87.58	3.00	87.58
1009	-9	-10	S	109	QA	ZG	0.00	92.65	3.50	92.65	1009	-9	-10	S	110	QA	ZG	0.00	90.09	3.50	90.09
1009	-10	123	S	113	QA	ZG	0.00	90.09	3.50	90.09	1009	-10	123	S	114	QA	ZG	0.00	92.65	3.50	92.65
1011	-11	-12	S	107	QA	ZG	0.00	87.58	3.00	87.58	1011	-11	-12	S	108	QA	ZG	0.00	87.58	3.00	87.58
1011	-12	-13	S	110	QA	ZG	0.00	90.09	3.50	90.09	1011	-12	-13	S	111	QA	ZG	0.00	90.09	3.50	90.09
1011	-13	124	S	112	QA	ZG	0.00	90.09	3.50	90.09	1011	-13	124	S	113	QA	ZG	0.00	90.09	3.50	90.09
1012	125	127	S	108	QA	ZG	0.00	87.58	2.20	87.58	1012	127	128	S	108	QA	ZG	0.00	87.58	0.40	87.58
1012	128	129	S	108	QA	ZG	0.00	87.58	0.40	87.58	1012	129	130	S	111	QA	ZG	0.00	90.09	0.40	90.09
1012	130	135	S	111	QA	ZG	0.00	90.09	3.10	90.09	1012	135	142	S	112	QA	ZG	0.00	90.09	3.50	90.09
1013	101	-1	S	103	QA	ZG	0.00	87.58	0.72	87.58	1013	-1	117	S	104	QA	ZG	0.00	87.58	0.72	87.58
1013	117	-6	S	105	QA	ZG	0.00	90.00	0.75	90.00	1013	-6	122	S	106	QA	ZG	0.00	90.00	0.75	90.00
1013	122	-11	S	107	QA	ZG	0.00	87.58	0.72	87.58	1013	-11	125	S	108	QA	ZG	0.00	87.58	0.72	87.58
1017	105	-2	S	102	QA	ZG	0.00	90.09	0.72	90.09	1017	105	-2	S	103	QA	ZG	0.00	87.58	0.72	87.58
1017	-2	-4	S	101	QA	ZG	0.00	90.09	0.72	90.09	1017	-2	-4	S	104	QA	ZG	0.00	87.58	0.72	87.58
1017	-4	-7	S	100	QA	ZG	0.00	92.65	0.75	92.65	1017	-4	-7	S	105	QA	ZG	0.00	90.00	0.75	90.00
1017	-7	-9	S	106	QA	ZG	0.00	90.00	0.75	90.00	1017	-7	-9	S	109	QA	ZG	0.00	92.65	0.75	92.65
1017	-9	-12	S	107	QA	ZG	0.00	87.58	0.72	87.58	1017	-9	-12	S	110	QA	ZG	0.00	90.09	0.72	90.09
1017	-12	129	S	108	QA	ZG	0.00	87.58	0.72	87.58	1017	-12	129	S	111	QA	ZG	0.00	90.09	0.72	90.09
1022	110	-3	S	102	QA	ZG	0.00	90.09	0.72	90.09	1022	110	-3	S	117	QA	ZG	0.00	90.09	0.72	90.09
1022	-3	-5	S	101	QA	ZG	0.00	90.09	0.72	90.09	1022	-3	-5	S	116	QA	ZG	0.00	90.09	0.72	90.09
1022	-5	-8	S	100	QA	ZG	0.00	92.65	0.75	92.65	1022	-5	-8	S	115	QA	ZG	0.00	92.65	0.75	92.65

1022 -8 -10 S 109 QA ZG 0.00 92.65 0.75 92.65 1022 -8 -10 S 114 QA ZG 0.00 92.65 0.75 92.65
1022 -10 -13 S 110 QA ZG 0.00 90.09 0.72 90.09 1022 -10 -13 S 113 QA ZG 0.00 90.09 0.72 90.09
1022 -13 135 S 111 QA ZG 0.00 90.09 0.72 90.09 1022 -13 135 S 112 QA ZG 0.00 90.09 0.72 90.09
1026 115 116 S 117 QA ZG 0.00 90.09 0.72 90.09 1026 116 118 S 116 QA ZG 0.00 90.09 0.72 90.09
1026 118 144 S 115 QA ZG 0.00 92.65 0.75 92.65 1026 144 123 S 114 QA ZG 0.00 92.65 0.75 92.65
1026 123 124 S 113 QA ZG 0.00 90.09 0.72 90.09 1026 124 142 S 112 QA ZG 0.00 90.09 0.72 90.09

CONDIZIONE DI CARICO 4: Esercizio cat.H

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
3007	-72	-73	S	334	QA2	ZG	0.00	13.75	0.75	13.75	3007	-73	-74	S	334	QA2	ZG	0.00	13.75	0.75	13.75
3007	-74	-75	S	334	QA2	ZG	0.00	13.75	0.75	13.75	3007	-75	-76	S	334	QA2	ZG	0.00	13.75	0.75	13.75
3007	-81	-82	S	330	QA2	ZG	0.00	13.75	0.70	13.75	3007	-82	-83	S	330	QA2	ZG	0.00	13.75	0.70	13.75
3007	-83	-84	S	330	QA2	ZG	0.00	13.75	0.70	13.75	3007	-84	-85	S	330	QA2	ZG	0.00	13.75	1.40	13.75
3008	-68	-69	S	334	QA2	ZG	0.00	13.75	3.00	13.75	3008	-68	-69	S	335	QA2	ZG	0.00	13.75	3.00	13.75
3010	-51	-52	S	335	QA2	ZG	0.00	13.75	3.00	13.75	3010	-53	-54	S	331	QA2	ZG	0.00	13.75	3.50	13.75
3013	-38	-55	S	301	QA2	ZG	0.00	17.87	0.58	17.87	3013	-55	-72	S	319	QA2	ZG	0.00	17.87	0.58	17.87
3014	-39	-56	S	300	QA2	ZG	0.00	17.87	0.58	17.87	3014	-39	-56	S	301	QA2	ZG	0.00	17.87	0.58	17.87
3014	-56	-73	S	318	QA2	ZG	0.00	17.87	0.58	17.87	3014	-56	-73	S	319	QA2	ZG	0.00	17.87	0.58	17.87
3015	-24	-27	S	316	QA2	ZG	0.00	17.87	0.58	17.87	3015	-27	-40	S	333	QA2	ZG	0.00	17.87	0.58	17.87
3015	-40	-57	S	300	QA2	ZG	0.00	17.87	0.58	17.87	3015	-57	-74	S	318	QA2	ZG	0.00	17.87	0.58	17.87
3015	-57	-74	S	321	QA2	ZG	0.00	17.87	0.58	17.87	3016	204	-28	S	315	QA2	ZG	0.00	17.87	0.58	17.87
3016	204	-28	S	316	QA2	ZG	0.00	17.87	0.58	17.87	3016	-28	-41	S	332	QA2	ZG	0.00	17.87	0.58	17.87
3016	-28	-41	S	333	QA2	ZG	0.00	17.87	0.58	17.87	3017	205	-29	S	312	QA2	ZG	0.00	16.68	0.58	16.68
3017	205	-29	S	315	QA2	ZG	0.00	17.87	0.58	17.87	3017	-29	-42	S	313	QA2	ZG	0.00	16.68	0.58	16.68
3017	-29	-42	S	332	QA2	ZG	0.00	17.87	0.58	17.87	3017	-59	-76	S	320	QA2	ZG	0.00	17.87	0.58	17.87
3017	-59	-76	S	322	QA2	ZG	0.00	16.68	0.58	16.68	3018	206	-30	S	311	QA2	ZG	0.00	16.68	0.58	16.68
3018	206	-30	S	312	QA2	ZG	0.00	16.68	0.58	16.68	3018	-30	-43	S	310	QA2	ZG	0.00	16.68	0.58	16.68
3018	-30	-43	S	313	QA2	ZG	0.00	16.68	0.58	16.68	3019	207	-31	S	308	QA2	ZG	0.00	16.68	0.58	16.68
3019	207	-31	S	311	QA2	ZG	0.00	16.68	0.58	16.68	3019	-31	-44	S	309	QA2	ZG	0.00	16.68	0.58	16.68
3019	-31	-44	S	310	QA2	ZG	0.00	16.68	0.58	16.68	3020	208	-32	S	307	QA2	ZG	0.00	16.68	0.58	16.68
3020	208	-32	S	308	QA2	ZG	0.00	16.68	0.58	16.68	3020	-32	-45	S	306	QA2	ZG	0.00	16.68	0.58	16.68
3020	-32	-45	S	309	QA2	ZG	0.00	16.68	0.58	16.68	3021	209	-33	S	304	QA2	ZG	0.00	16.68	0.58	16.68
3021	209	-33	S	307	QA2	ZG	0.00	16.68	0.58	16.68	3021	-33	-46	S	305	QA2	ZG	0.00	16.68	0.58	16.68
3021	-33	-46	S	306	QA2	ZG	0.00	16.68	0.58	16.68	3022	210	-34	S	302	QA2	ZG	0.00	16.68	0.58	16.68
3022	210	-34	S	304	QA2	ZG	0.00	16.68	0.58	16.68	3022	-34	-47	S	303	QA2	ZG	0.00	16.68	0.58	16.68
3022	-34	-47	S	305	QA2	ZG	0.00	16.68	0.58	16.68	3022	-64	-81	S	325	QA2	ZG	0.00	16.68	0.58	16.68
3022	-64	-81	S	327	QA2	ZG	0.00	16.68	0.58	16.68	3023	211	-35	S	302	QA2	ZG	0.00	16.68	0.58	16.68
3023	211	-35	S	317	QA2	ZG	0.00	16.68	0.58	16.68	3023	-35	-48	S	303	QA2	ZG	0.00	16.68	0.58	16.68

16.68
3024 -25 -36 S 314 QA2 ZG 0.00 16.68 0.58 16.68 3024 -25 -36 S 317 QA2 ZG 0.00 16.68 0.58
16.68
3025 -26 -37 S 314 QA2 ZG 0.00 16.68 0.58 16.68 3025 -67 -84 S 328 QA2 ZG 0.00 16.68 0.58
16.68
3039 -70 -71 S 330 QA2 ZG 0.00 13.75 3.50 13.75 3039 -70 -71 S 331 QA2 ZG 0.00 13.75 3.50
13.75
3047 -58 -75 S 320 QA2 ZG 0.00 17.87 0.58 17.87 3047 -58 -75 S 321 QA2 ZG 0.00 17.87 0.58
17.87
3049 -60 -77 S 322 QA2 ZG 0.00 16.68 0.58 16.68 3049 -60 -77 S 323 QA2 ZG 0.00 16.68 0.58
16.68
3050 -61 -78 S 323 QA2 ZG 0.00 16.68 0.58 16.68 3050 -61 -78 S 324 QA2 ZG 0.00 16.68 0.58
16.68
3051 -62 -79 S 324 QA2 ZG 0.00 16.68 0.58 16.68 3051 -62 -79 S 326 QA2 ZG 0.00 16.68 0.58
16.68
3052 -63 -80 S 325 QA2 ZG 0.00 16.68 0.58 16.68 3052 -63 -80 S 326 QA2 ZG 0.00 16.68 0.58
16.68
3054 -65 -82 S 327 QA2 ZG 0.00 16.68 0.58 16.68 3054 -65 -82 S 329 QA2 ZG 0.00 16.68 0.58
16.68
3055 -66 -83 S 328 QA2 ZG 0.00 16.68 0.58 16.68 3055 -66 -83 S 329 QA2 ZG 0.00 16.68 0.58
16.68

CONDIZIONE DI CARICO 5: Neve

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
3007	-72	-73	S	334	QA3	ZG	0.00	13.20	0.75	13.20	3007	-73	-74	S	334	QA3	ZG	0.00	13.20	0.75	13.20
3007	-74	-75	S	334	QA3	ZG	0.00	13.20	0.75	13.20	3007	-75	-76	S	334	QA3	ZG	0.00	13.20	0.75	13.20
3007	-81	-82	S	330	QA3	ZG	0.00	13.20	0.70	13.20	3007	-82	-83	S	330	QA3	ZG	0.00	13.20	0.70	13.20
3007	-83	-84	S	330	QA3	ZG	0.00	13.20	0.70	13.20	3007	-84	-85	S	330	QA3	ZG	0.00	13.20	1.40	13.20
3008	-68	-69	S	334	QA3	ZG	0.00	13.20	3.00	13.20	3008	-68	-69	S	335	QA3	ZG	0.00	13.20	3.00	13.20
3010	-51	-52	S	335	QA3	ZG	0.00	13.20	3.00	13.20	3010	-53	-54	S	331	QA3	ZG	0.00	13.20	3.50	13.20
3013	-38	-55	S	301	QA3	ZG	0.00	17.15	0.58	17.15	3013	-55	-72	S	319	QA3	ZG	0.00	17.15	0.58	17.15
3014	-39	-56	S	300	QA3	ZG	0.00	17.15	0.58	17.15	3014	-39	-56	S	301	QA3	ZG	0.00	17.15	0.58	17.15
3014	-56	-73	S	318	QA3	ZG	0.00	17.15	0.58	17.15	3014	-56	-73	S	319	QA3	ZG	0.00	17.15	0.58	17.15
3015	-24	-27	S	316	QA3	ZG	0.00	17.15	0.58	17.15	3015	-27	-40	S	333	QA3	ZG	0.00	17.15	0.58	17.15
3015	-40	-57	S	300	QA3	ZG	0.00	17.15	0.58	17.15	3015	-57	-74	S	318	QA3	ZG	0.00	17.15	0.58	17.15
3015	-57	-74	S	321	QA3	ZG	0.00	17.15	0.58	17.15	3016	204	-28	S	315	QA3	ZG	0.00	17.15	0.58	17.15
3016	204	-28	S	316	QA3	ZG	0.00	17.15	0.58	17.15	3016	-28	-41	S	332	QA3	ZG	0.00	17.15	0.58	17.15
3016	-28	-41	S	333	QA3	ZG	0.00	17.15	0.58	17.15	3017	205	-29	S	312	QA3	ZG	0.00	16.01	0.58	16.01
3017	205	-29	S	315	QA3	ZG	0.00	17.15	0.58	17.15	3017	-29	-42	S	313	QA3	ZG	0.00	16.01	0.58	16.01
3017	-29	-42	S	332	QA3	ZG	0.00	17.15	0.58	17.15	3017	-59	-76	S	320	QA3	ZG	0.00	17.15	0.58	17.15
3017	-59	-76	S	322	QA3	ZG	0.00	16.01	0.58	16.01	3018	206	-30	S	311	QA3	ZG	0.00	16.01	0.58	16.01
3018	206	-30	S	312	QA3	ZG	0.00	16.01	0.58	16.01	3018	-30	-43	S	310	QA3	ZG	0.00	16.01	0.58	16.01
3018	-30	-43	S	313	QA3	ZG	0.00	16.01	0.58	16.01	3019	207	-31	S	308	QA3	ZG	0.00	16.01	0.58	16.01
3019	207	-31	S	311	QA3	ZG	0.00	16.01	0.58	16.01	3019	-31	-44	S	309	QA3	ZG	0.00	16.01	0.58	16.01
3019	-31	-44	S	310	QA3	ZG	0.00	16.01	0.58	16.01	3020	208	-32	S	307	QA3	ZG	0.00	16.01	0.58	16.01
3020	208	-32	S	308	QA3	ZG	0.00	16.01	0.58	16.01	3020	-32	-45	S	306	QA3	ZG	0.00	16.01	0.58	16.01
3020	-32	-45	S	309	QA3	ZG	0.00	16.01	0.58	16.01	3021	209	-33	S	304	QA3	ZG	0.00	16.01	0.58	16.01
3021	209	-33	S	307	QA3	ZG	0.00	16.01	0.58	16.01	3021	-33	-46	S	305	QA3	ZG	0.00	16.01	0.58	16.01
3021	-33	-46	S	306	QA3	ZG	0.00	16.01	0.58	16.01	3022	210	-34	S	302	QA3	ZG	0.00	16.01	0.58	16.01

3022 210 -34 S 304 QA3 ZG 0.00 16.01 0.58 16.01 3022 -34 -47 S 303 QA3 ZG 0.00 16.01 0.58 16.01
3022 -34 -47 S 305 QA3 ZG 0.00 16.01 0.58 16.01 3022 -64 -81 S 325 QA3 ZG 0.00 16.01 0.58 16.01
3022 -64 -81 S 327 QA3 ZG 0.00 16.01 0.58 16.01 3023 211 -35 S 302 QA3 ZG 0.00 16.01 0.58 16.01
3023 211 -35 S 317 QA3 ZG 0.00 16.01 0.58 16.01 3023 -35 -48 S 303 QA3 ZG 0.00 16.01 0.58 16.01
3024 -25 -36 S 314 QA3 ZG 0.00 16.01 0.58 16.01 3024 -25 -36 S 317 QA3 ZG 0.00 16.01 0.58 16.01
3025 -26 -37 S 314 QA3 ZG 0.00 16.01 0.58 16.01 3025 -67 -84 S 328 QA3 ZG 0.00 16.01 0.58 16.01
3039 -70 -71 S 330 QA3 ZG 0.00 13.20 3.50 13.20 3039 -70 -71 S 331 QA3 ZG 0.00 13.20 3.50 13.20
3047 -58 -75 S 320 QA3 ZG 0.00 17.15 0.58 17.15 3047 -58 -75 S 321 QA3 ZG 0.00 17.15 0.58 17.15
3049 -60 -77 S 322 QA3 ZG 0.00 16.01 0.58 16.01 3049 -60 -77 S 323 QA3 ZG 0.00 16.01 0.58 16.01
3050 -61 -78 S 323 QA3 ZG 0.00 16.01 0.58 16.01 3050 -61 -78 S 324 QA3 ZG 0.00 16.01 0.58 16.01
3051 -62 -79 S 324 QA3 ZG 0.00 16.01 0.58 16.01 3051 -62 -79 S 326 QA3 ZG 0.00 16.01 0.58 16.01
3052 -63 -80 S 325 QA3 ZG 0.00 16.01 0.58 16.01 3052 -63 -80 S 326 QA3 ZG 0.00 16.01 0.58 16.01
3054 -65 -82 S 327 QA3 ZG 0.00 16.01 0.58 16.01 3054 -65 -82 S 329 QA3 ZG 0.00 16.01 0.58 16.01
3055 -66 -83 S 328 QA3 ZG 0.00 16.01 0.58 16.01 3055 -66 -83 S 329 QA3 ZG 0.00 16.01 0.58 16.01

CONDIZIONE DI CARICO 6: Vento X+_1

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
0	143	45	T	126	VE	YL	0.00	12.38	2.30	12.38	0	143	45	T	126	VE	ZL	0.00	5.13	2.30	5.13
0	143	45	T	128	VE	YL	0.00	5.12	2.30	5.12	0	143	45	T	128	VE	ZL	0.00	13.62	2.30	13.62
0	145	46	T	129	VE	YL	0.00	-3.36	2.30	-3.36	0	145	46	T	129	VE	ZL	0.00	12.91	2.30	12.91
0	145	46	T	127	VE	YL	0.00	14.14	2.30	14.14	0	145	46	T	127	VE	ZL	0.00	-5.84	2.30	-5.84
0	18	48	T	233	VE	YL	0.00	0.00	0.56	5.67	0	48	21	T	233	VE	YL	0.00	2.44	0.54	7.18
0	49	21	T	134	VE	YL	0.00	-2.44	0.54	-7.18	0	23	49	T	134	VE	YL	0.00	0.00	0.56	-5.67
15	115	215	T	232	VE	YL	0.00	18.12	3.76	18.12	16	116	216	T	232	VE	ZL	0.00	18.12	3.76	18.12
16	116	216	T	133	VE	ZL	0.00	18.12	2.30	18.12	16	116	216	T	133	VE	ZL	2.30	18.12	3.76	18.12
18	118	18	T	133	VE	ZL	0.00	18.12	2.30	18.12	18	118	18	T	126	VE	YL	0.00	12.38	2.30	12.38
18	118	18	T	126	VE	ZL	0.00	5.13	2.30	5.13	18	18	218	T	133	VE	ZL	0.00	18.12	1.46	18.12
18	18	218	T	233	VE	ZL	0.00	0.00	0.49	6.38	18	18	218	T	233	VE	ZL	0.49	6.38	0.70	18.75
18	18	218	T	233	VE	ZL	0.70	18.75	1.46	18.75	19	119	19	T	128	VE	YL	0.00	5.12	2.30	5.12
19	119	19	T	128	VE	ZL	0.00	13.62	2.30	13.62	19	119	19	T	129	VE	YL	0.00	-3.36	2.30	-3.36
19	119	19	T	129	VE	ZL	0.00	12.91	2.30	12.91	21	21	221	T	233	VE	ZL	0.00	18.75	0.76	18.75
21	21	221	T	134	VE	ZL	0.00	18.75	0.76	18.75	23	123	23	T	135	VE	ZL	0.00	18.12	2.30	18.12
23	123	23	T	127	VE	YL	0.00	14.14	2.30	14.14	23	123	23	T	127	VE	ZL	0.00	-5.84	2.30	-5.84
23	23	223	T	135	VE	ZL	0.00	18.12	1.46	18.12	23	23	223	T	134	VE	ZL	0.00	0.00	0.49	6.38
23	23	223	T	134	VE	ZL	0.49	6.38	0.70	18.75	23	23	223	T	134	VE	ZL	0.70	18.75	1.46	18.75
24	124	224	T	136	VE	ZL	1.70	18.12	3.76	18.12	24	124	224	T	135	VE	ZL	0.00	18.12	2.30	18.12
24	124	224	T	135	VE	ZL	2.30	18.12	3.76	18.12	24	124	224	T	136	VE	ZL	0.00	18.12	1.70	18.12
42	142	-19	T	136	VE	YL	0.00	18.12	1.70	18.12	42	-19	242	T	136	VE	YL	0.00	18.12	2.06	18.12

```
1013 101  -1 T 130 VE YL 0.00   25.00 0.72   25.00   1013  -1 117 T 130 VE YL 0.00   25.00 0.72
25.00
1013 122 -11 T 132 VE YL 0.00   25.00 0.72   25.00   1013 -11 125 T 132 VE YL 0.00   25.00 0.72
25.00
2013 201 220 T 330 VE YL 0.00    0.00 1.10    8.75   2013 201 220 T 230 VE YL 1.45   36.50 2.20
36.50
2013 201 220 T 230 VE YL 0.00   69.00 1.45   69.00   2013 201 220 T 330 VE YL 1.65   13.12 2.20
17.50
2013 201 220 T 330 VE YL 1.10    8.75 1.65   13.12   2013 220 225 T 131 VE YL 0.00   36.50 0.75
36.50
2013 220 225 T 330 VE YL 1.10    8.75 2.20    0.00   2013 220 225 T 330 VE YL 0.55   13.12 1.10
8.75
2013 220 225 T 330 VE YL 0.00   17.50 0.55   13.12   2013 220 225 T 131 VE YL 0.75   69.00 2.20
69.00
2026 215 216 T 333 VE YL 0.00    0.00 0.72    5.77   2026 216 218 T 333 VE YL 0.00    5.77 0.38
8.75
2026 216 218 T 333 VE YL 0.38    8.75 0.72   11.53   2026 218 221 T 333 VE YL 0.00   11.53 0.75
17.50
2026 221 223 T 333 VE YL 0.00   17.50 0.55   13.12   2026 221 223 T 333 VE YL 0.55   13.12 0.75
11.53
2026 223 224 T 333 VE YL 0.00   11.53 0.35    8.75   2026 223 224 T 333 VE YL 0.35    8.75 0.72
5.77
2026 224 242 T 333 VE YL 0.00    5.77 0.72    0.00   3007 -72 -73 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -72 -73 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -73 -74 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -73 -74 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -74 -75 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -74 -75 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -75 -76 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -75 -76 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -81 -82 S 330 VE YL 0.00   -4.38 0.70   -
4.38
3007 -81 -82 S 330 VE ZL 0.00  -13.75 0.70  -13.75   3007 -82 -83 S 330 VE YL 0.00   -4.38 0.70   -
4.38
3007 -82 -83 S 330 VE ZL 0.00  -13.75 0.70  -13.75   3007 -83 -84 S 330 VE YL 0.00   -4.38 0.70   -
4.38
3007 -83 -84 S 330 VE ZL 0.00  -13.75 0.70  -13.75   3007 -84 -85 S 330 VE YL 0.00   -4.38 1.40   -
4.38
3007 -84 -85 S 330 VE ZL 0.00  -13.75 1.40  -13.75   3008 -68 -69 S 334 VE YL 0.00   -0.00 0.75   -
0.00
3008 -68 -69 S 334 VE ZL 0.00  -14.43 0.75  -14.43   3008 -68 -69 S 335 VE YL 0.00   -0.00 3.00   -
0.00
3008 -68 -69 S 335 VE ZL 0.00  -14.43 3.00  -14.43   3008 -68 -69 S 334 VE YL 2.25   -0.00 3.00   -
0.00
3008 -68 -69 S 334 VE ZL 2.25  -14.43 3.00  -14.43   3008 -68 -69 S 334 VE YL 1.50   -0.00 2.25   -
0.00
3008 -68 -69 S 334 VE ZL 1.50  -14.43 2.25  -14.43   3008 -68 -69 S 334 VE YL 0.75   -0.00 1.50   -
0.00
3008 -68 -69 S 334 VE ZL 0.75  -14.43 1.50  -14.43   3010 -51 -52 S 335 VE YL 0.00   -0.00 3.00   -
0.00
3010 -51 -52 S 335 VE ZL 0.00  -14.43 3.00  -14.43   3010 -53 -54 S 331 VE YL 0.00   -0.00 3.50   -
0.00
3010 -53 -54 S 331 VE ZL 0.00  -14.43 3.50  -14.43   3013 201 -38 T 330 VE YL 0.00    0.00 1.15
8.34
3013 -38 -55 S 301 VE ZL 0.00  -18.75 0.58  -18.75   3013 -38 -55 T 330 VE YL 0.00    8.34 0.58
12.51
3013 -55 -72 S 319 VE ZL 0.00  -18.75 0.58  -18.75   3013 -55 -72 T 330 VE YL 0.00   12.51 0.58
16.68
3014 -39 -56 S 300 VE ZL 0.00  -18.75 0.58  -18.75   3014 -39 -56 S 301 VE ZL 0.00  -18.75 0.58  -
18.75
3014 -56 -73 S 318 VE ZL 0.00  -18.75 0.58  -18.75   3014 -56 -73 S 319 VE ZL 0.00  -18.75 0.58  -
18.75
3015 -24 -27 S 316 VE ZL 0.00  -18.75 0.58  -18.75   3015 -27 -40 S 333 VE ZL 0.00  -18.75 0.58  -
18.75
3015 -40 -57 S 300 VE ZL 0.00  -18.75 0.58  -18.75   3015 -57 -74 S 318 VE ZL 0.00  -18.75 0.58  -
18.75
3015 -57 -74 S 321 VE ZL 0.00  -18.75 0.58  -18.75   3016 204 -28 S 315 VE ZL 0.00  -18.75 0.58  -
18.75
3016 204 -28 S 316 VE ZL 0.00  -18.75 0.58  -18.75   3016 -28 -41 S 332 VE ZL 0.00  -18.75 0.58  -
18.75
3016 -28 -41 S 333 VE ZL 0.00  -18.75 0.58  -18.75   3017 205 -29 S 312 VE ZL 0.00  -17.50 0.58  -
17.50
3017 205 -29 S 315 VE ZL 0.00  -18.75 0.58  -18.75   3017 -29 -42 S 313 VE ZL 0.00  -17.50 0.58  -
17.50
3017 -29 -42 S 332 VE ZL 0.00  -18.75 0.58  -18.75   3017 -59 -76 S 320 VE ZL 0.00  -18.75 0.58  -
18.75
3017 -59 -76 S 322 VE ZL 0.00  -17.50 0.58  -17.50   3018 206 -30 S 311 VE ZL 0.00  -17.50 0.58  -
17.50
3018 206 -30 S 312 VE ZL 0.00  -17.50 0.58  -17.50   3018 -30 -43 S 310 VE ZL 0.00  -17.50 0.58  -
17.50
3018 -30 -43 S 313 VE ZL 0.00  -17.50 0.58  -17.50   3019 207 -31 S 308 VE ZL 0.00  -17.50 0.58  -
17.50
3019 207 -31 S 311 VE ZL 0.00  -17.50 0.58  -17.50   3019 -31 -44 S 309 VE ZL 0.00  -17.50 0.58  -
```

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17.50
3019 -31 -44 S 310 VE ZL 0.00  -17.50 0.58  -17.50   3020 208 -32 S 307 VE ZL 0.00  -17.50 0.58  -
17.50
3020 208 -32 S 308 VE ZL 0.00  -17.50 0.58  -17.50   3020 -32 -45 S 306 VE ZL 0.00  -17.50 0.58  -
17.50
3020 -32 -45 S 309 VE ZL 0.00  -17.50 0.58  -17.50   3021 209 -33 S 304 VE ZL 0.00  -17.50 0.58  -
17.50
3021 209 -33 S 307 VE ZL 0.00  -17.50 0.58  -17.50   3021 -33 -46 S 305 VE ZL 0.00  -17.50 0.58  -
17.50
3021 -33 -46 S 306 VE ZL 0.00  -17.50 0.58  -17.50   3022 210 -34 S 302 VE ZL 0.00  -17.50 0.58  -
17.50
3022 210 -34 S 304 VE ZL 0.00  -17.50 0.58  -17.50   3022 -34 -47 S 303 VE ZL 0.00  -17.50 0.58  -
17.50
3022 -34 -47 S 305 VE ZL 0.00  -17.50 0.58  -17.50   3022 -64 -81 S 325 VE ZL 0.00  -17.50 0.58  -
17.50
3022 -64 -81 S 327 VE ZL 0.00  -17.50 0.58  -17.50   3023 211 -35 S 302 VE ZL 0.00  -17.50 0.58  -
17.50
3023 211 -35 S 317 VE ZL 0.00  -17.50 0.58  -17.50   3023 -35 -48 S 303 VE ZL 0.00  -17.50 0.58  -
17.50
3024 -25 -36 S 314 VE ZL 0.00  -17.50 0.58  -17.50   3024 -25 -36 S 317 VE ZL 0.00  -17.50 0.58  -
17.50
3025 -26 -37 S 314 VE ZL 0.00  -17.50 0.58  -17.50   3025 -67 -84 S 328 VE ZL 0.00  -17.50 0.58  -
17.50
3026 215 -50 T 333 VE YL 0.00    0.00 0.76    5.50   3026 215 -50 T 333 VE YL 0.76    5.50 1.15
8.34
3026 -50 -85 T 333 VE YL 0.00    8.34 0.37   10.99   3026 -50 -85 T 333 VE YL 0.37   10.99 1.15
16.68
3039 -70 -71 S 330 VE YL 0.00   -0.00 0.70   -0.00   3039 -70 -71 S 330 VE ZL 0.00  -14.43 0.70  -
14.43
3039 -70 -71 S 331 VE YL 0.00   -0.00 3.50   -0.00   3039 -70 -71 S 331 VE ZL 0.00  -14.43 3.50  -
14.43
3039 -70 -71 S 330 VE YL 2.10   -0.00 3.50   -0.00   3039 -70 -71 S 330 VE ZL 2.10  -14.43 3.50  -
14.43
3039 -70 -71 S 330 VE YL 1.40   -0.00 2.10   -0.00   3039 -70 -71 S 330 VE ZL 1.40  -14.43 2.10  -
14.43
3039 -70 -71 S 330 VE YL 0.70   -0.00 1.40   -0.00   3039 -70 -71 S 330 VE ZL 0.70  -14.43 1.40  -
14.43
3044 -72 -68 T 330 VE YL 0.00   16.68 0.58   12.51   3044 -68 -51 T 330 VE YL 0.00   12.51 0.58
8.34
3044 -51 225 T 330 VE YL 0.00    8.34 1.15    0.00   3047 -58 -75 S 320 VE ZL 0.00  -18.75 0.58  -
18.75
3047 -58 -75 S 321 VE ZL 0.00  -18.75 0.58  -18.75   3049 -60 -77 S 322 VE ZL 0.00  -17.50 0.58  -
17.50
3049 -60 -77 S 323 VE ZL 0.00  -17.50 0.58  -17.50   3050 -61 -78 S 323 VE ZL 0.00  -17.50 0.58  -
17.50
3050 -61 -78 S 324 VE ZL 0.00  -17.50 0.58  -17.50   3051 -62 -79 S 324 VE ZL 0.00  -17.50 0.58  -
17.50
3051 -62 -79 S 326 VE ZL 0.00  -17.50 0.58  -17.50   3052 -63 -80 S 325 VE ZL 0.00  -17.50 0.58  -
17.50
3052 -63 -80 S 326 VE ZL 0.00  -17.50 0.58  -17.50   3054 -65 -82 S 327 VE ZL 0.00  -17.50 0.58  -
17.50
3054 -65 -82 S 329 VE ZL 0.00  -17.50 0.58  -17.50   3055 -66 -83 S 328 VE ZL 0.00  -17.50 0.58  -
17.50
3055 -66 -83 S 329 VE ZL 0.00  -17.50 0.58  -17.50   3057 -85 -71 T 333 VE YL 0.00   16.68 0.58
12.51
3057 -71 -54 T 333 VE YL 0.00   12.51 0.21   10.99   3057 -71 -54 T 333 VE YL 0.21   10.99 0.58
8.34
3057 -54 242 T 333 VE YL 0.00    8.34 0.39    5.50   3057 -54 242 T 333 VE YL 0.39    5.50 1.15
0.00
5013 -15  17 T 230 VE ZL 0.00  -69.00 1.45  -69.00   5013 -15  17 T 130 VE ZL 0.72  -25.00 1.45  -
25.00
5013 -15  17 T 130 VE ZL 0.00  -25.00 0.72  -25.00   5044  44  20 T 230 VE ZL 0.00  -36.50 0.75  -
36.50
5044  20  47 T 131 VE ZL 0.00  -36.50 0.75  -36.50   5075  22 -16 T 131 VE ZL 0.00  -69.00 1.45  -
69.00
5075  22 -16 T 132 VE ZL 0.72  -25.00 1.45  -25.00   5075  22 -16 T 132 VE ZL 0.00  -25.00 0.72  -
25.00


CONDIZIONE DI CARICO 7: Vento Y+_1

CARICHI DISTRIBUITI

Asta  N1  N2 E  NE  T DC  Xi     Qi     Xf     Qf     Asta  N1  N2 E  NE  T DC  Xi     Qi     Xf     Qf
                          <m> <daN/m>  <m> <daN/m>                              <m> <daN/m>  <m>
<daN/m>
------------------------------------------------   ------------------------------------------------
--
   1 101 -15 T 101 VE ZL 0.00   23.75 1.00   23.75      1 -15 201 T 101 VE ZL 0.00   23.75 2.76
23.75
   2 102 202 T 102 VE ZL 2.86   22.50 3.76   22.50      2 102 202 T 101 VE ZL 0.00   23.75 1.00
```

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23.75
   2 102 202 T 101 VE ZL 1.00   23.75 3.76   23.75      2 102 202 T 102 VE ZL 0.00   22.50 2.16
22.50
   2 102 202 T 102 VE ZL 2.16   22.50 2.86   22.50      3 103   3 T 103 VE ZL 0.00   10.00 2.16
10.00
   3 103   3 T 102 VE ZL 0.00   22.50 2.16   22.50      3   3 -20 T 102 VE ZL 0.00   22.50 0.70
22.50
   3 -20 203 T 203 VE ZL 0.00   10.00 0.90   10.00      3 -20 203 T 102 VE ZL 0.00   22.50 0.90
22.50
   4 104   4 T 104 VE ZL 1.60   18.75 2.16   18.75      4 104   4 T 103 VE ZL 0.00   10.00 2.16
10.00
   4 104   4 T 104 VE ZL 0.00   18.75 1.60   18.75      4   4 -21 T 104 VE ZL 0.00   18.75 0.70
18.75
   4 -21 204 T 104 VE ZL 0.00   18.75 0.90   18.75      4 -21 204 T 203 VE ZL 0.00   10.00 0.90
10.00
   5 105  43 T 104 VE ZL 0.00   18.75 1.60   18.75      5  43 205 T 204 VE ZL 0.00   17.50 2.16
17.50
   5  43 205 T 104 VE ZL 0.00   18.75 0.56   18.75      5  43 205 T 104 VE ZL 0.56   18.75 1.26
18.75
   5  43 205 T 104 VE ZL 1.26   18.75 2.16   18.75      6 106   6 T 105 VE ZL 0.00   17.50 1.60
17.50
   6   6 206 T 105 VE ZL 0.00   17.50 2.16   17.50      6   6 206 T 204 VE ZL 0.00   17.50 2.16
17.50
   7 107 207 T 106 VE ZL 0.00   17.50 3.76   17.50      7 107 207 T 105 VE ZL 0.00   17.50 1.60
17.50
   7 107 207 T 105 VE ZL 1.60   17.50 3.76   17.50      8 108 208 T 107 VE ZL 0.00   17.50 3.76
17.50
   8 108 208 T 106 VE ZL 0.00   17.50 3.76   17.50      9 109 209 T 107 VE ZL 0.00   17.50 3.76
17.50
   9 109 209 T 108 VE ZL 0.00   17.50 3.76   17.50     10 110 210 T 109 VE ZL 2.86   17.50 3.76
17.50
  10 110 210 T 108 VE ZL 0.00   17.50 3.76   17.50     10 110 210 T 109 VE ZL 0.00   17.50 2.16
17.50
  10 110 210 T 109 VE ZL 2.16   17.50 2.86   17.50     11 111  11 T 110 VE ZL 0.00   10.00 2.16
10.00
  11 111  11 T 109 VE ZL 0.00   17.50 2.16   17.50     11  11 -22 T 109 VE ZL 0.00   17.50 0.70
17.50
  11 -22 211 T 109 VE ZL 0.00   17.50 0.90   17.50     11 -22 211 T 210 VE ZL 0.00   10.00 0.90
10.00
  12 112  12 T 110 VE ZL 0.00   10.00 2.16   10.00     12 112  12 T 111 VE ZL 0.00   20.00 2.16
20.00
  12  12 -23 T 111 VE ZL 0.00   20.00 0.70   20.00     12 -23 212 T 111 VE ZL 0.00   20.00 0.90
20.00
  12 -23 212 T 210 VE ZL 0.00   10.00 0.90   10.00     13 113 213 T 111 VE ZL 2.86   20.00 3.76
20.00
  13 113 213 T 112 VE ZL 0.00   20.00 3.76   20.00     13 113 213 T 111 VE ZL 0.00   20.00 2.16
20.00
  13 113 213 T 111 VE ZL 2.16   20.00 2.86   20.00     14 114 214 T 113 VE ZL 0.00   20.00 3.76
20.00
  14 114 214 T 112 VE ZL 0.00   20.00 3.76   20.00     15 115 215 T 113 VE ZL 0.00   20.00 3.76
20.00
  26  26 226 T 314 VE ZL 0.00   15.00 2.76   15.00     27 127  27 T 115 VE ZL 0.00   10.00 0.50
10.00
  27  27 -17 T 115 VE ZL 0.00   10.00 0.50   10.00     28 128  28 T 115 VE ZL 0.50   10.00 1.00
10.00
  28 128  28 T 115 VE ZL 0.00   10.00 0.50   10.00     28  28 228 T 314 VE ZL 0.00   15.00 2.76
15.00
  29 129 -18 T 215 VE ZL 0.00   10.00 1.70   10.00     29 -18 229 T 315 VE ZL 0.00   10.00 2.06
10.00
  30 130  30 T 215 VE ZL 0.00   10.00 1.70   10.00     30  30 230 T 116 VE ZL 0.00   15.50 2.06
15.50
  30  30 230 T 315 VE ZL 0.00   10.00 2.06   10.00     31  31 231 T 117 VE ZL 0.00   15.50 2.06
15.50
  31  31 231 T 116 VE ZL 0.00   15.50 2.06   15.50     32  32 232 T 118 VE ZL 0.00   15.50 2.06
15.50
  32  32 232 T 117 VE ZL 0.00   15.50 2.06   15.50     33  33 233 T 119 VE ZL 0.00   15.50 2.06
15.50
  33  33 233 T 118 VE ZL 0.00   15.50 2.06   15.50     34  34 234 T 120 VE ZL 0.00   15.50 2.06
15.50
  34  34 234 T 119 VE ZL 0.00   15.50 2.06   15.50     36  36 236 T 120 VE ZL 0.00   15.50 2.06
15.50
  37  37 237 T 121 VE ZL 0.00   15.50 2.06   15.50     38  38 238 T 122 VE ZL 0.00   15.50 2.06
15.50
  38  38 238 T 121 VE ZL 0.00   15.50 2.06   15.50     39  39 239 T 123 VE ZL 0.00   15.50 2.06
15.50
  39  39 239 T 122 VE ZL 0.00   15.50 2.06   15.50     40  40 240 T 124 VE ZL 0.00   15.50 2.06
15.50
  40  40 240 T 123 VE ZL 0.00   15.50 2.06   15.50     41  41 241 T 125 VE ZL 0.00   15.50 2.06
15.50
  41  41 241 T 124 VE ZL 0.00   15.50 2.06   15.50     42 -19 242 T 125 VE ZL 0.00   15.50 2.06
15.50
1012 125 127 T 114 VE YL 0.00  -12.50 2.20  -12.50   3007 -72 -73 S 334 VE YL 0.00   -4.38 0.75   -
4.38
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3007 -73 -74 S 334 VE ZL 0.00 -13.75 0.75 -13.75 3007 -74 -75 S 334 VE YL 0.00 -4.38 0.75 -4.38
3007 -74 -75 S 334 VE ZL 0.00 -13.75 0.75 -13.75 3007 -75 -76 S 334 VE YL 0.00 -4.38 0.75 -4.38
3007 -75 -76 S 334 VE ZL 0.00 -13.75 0.75 -13.75 3007 -81 -82 S 330 VE YL 0.00 -4.38 0.70 -4.38
3007 -81 -82 S 330 VE ZL 0.00 -13.75 0.70 -13.75 3007 -82 -83 S 330 VE YL 0.00 -4.38 0.70 -4.38
3007 -82 -83 S 330 VE ZL 0.00 -13.75 0.70 -13.75 3007 -83 -84 S 330 VE YL 0.00 -4.38 0.70 -4.38
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3007 -84 -85 S 330 VE ZL 0.00 -13.75 1.40 -13.75 3008 -68 -69 S 334 VE YL 0.00 -0.00 0.75 -0.00
3008 -68 -69 S 334 VE ZL 0.00 -14.43 0.75 -14.43 3008 -68 -69 S 335 VE YL 0.00 -0.00 3.00 -0.00
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3008 -68 -69 S 334 VE ZL 1.50 -14.43 2.25 -14.43 3008 -68 -69 S 334 VE YL 0.75 -0.00 1.50 -0.00
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3010 -51 -52 S 335 VE ZL 0.00 -14.43 3.00 -14.43 3010 -53 -54 S 331 VE YL 0.00 -0.00 3.50 -0.00
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3013 -55 -72 S 319 VE ZL 0.00 -18.75 0.58 -18.75 3014 -39 -56 S 300 VE ZL 0.00 -18.75 0.58 -18.75
3014 -39 -56 S 301 VE ZL 0.00 -18.75 0.58 -18.75 3014 -56 -73 S 318 VE ZL 0.00 -18.75 0.58 -18.75
3014 -56 -73 S 319 VE ZL 0.00 -18.75 0.58 -18.75 3015 -24 -27 S 316 VE ZL 0.00 -18.75 0.58 -18.75
3015 -27 -40 S 333 VE ZL 0.00 -18.75 0.58 -18.75 3015 -40 -57 S 300 VE ZL 0.00 -18.75 0.58 -18.75
3015 -57 -74 S 318 VE ZL 0.00 -18.75 0.58 -18.75 3015 -57 -74 S 321 VE ZL 0.00 -18.75 0.58 -18.75
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3017 -29 -42 S 313 VE ZL 0.00 -17.50 0.58 -17.50 3017 -29 -42 S 332 VE ZL 0.00 -18.75 0.58 -18.75
3017 -59 -76 S 320 VE ZL 0.00 -18.75 0.58 -18.75 3017 -59 -76 S 322 VE ZL 0.00 -17.50 0.58 -17.50
3018 206 -30 S 311 VE ZL 0.00 -17.50 0.58 -17.50 3018 206 -30 S 312 VE ZL 0.00 -17.50 0.58 -17.50
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3019 -31 -44 S 309 VE ZL 0.00 -17.50 0.58 -17.50 3019 -31 -44 S 310 VE ZL 0.00 -17.50 0.58 -17.50
3020 208 -32 S 307 VE ZL 0.00 -17.50 0.58 -17.50 3020 208 -32 S 308 VE ZL 0.00 -17.50 0.58 -17.50
3020 -32 -45 S 306 VE ZL 0.00 -17.50 0.58 -17.50 3020 -32 -45 S 309 VE ZL 0.00 -17.50 0.58 -17.50
3021 209 -33 S 304 VE ZL 0.00 -17.50 0.58 -17.50 3021 209 -33 S 307 VE ZL 0.00 -17.50 0.58 -17.50
3021 -33 -46 S 305 VE ZL 0.00 -17.50 0.58 -17.50 3021 -33 -46 S 306 VE ZL 0.00 -17.50 0.58 -17.50
3022 210 -34 S 302 VE ZL 0.00 -17.50 0.58 -17.50 3022 210 -34 S 304 VE ZL 0.00 -17.50 0.58 -17.50
3022 -34 -47 S 303 VE ZL 0.00 -17.50 0.58 -17.50 3022 -34 -47 S 305 VE ZL 0.00 -17.50 0.58 -17.50
3022 -64 -81 S 325 VE ZL 0.00 -17.50 0.58 -17.50 3022 -64 -81 S 327 VE ZL 0.00 -17.50 0.58 -17.50
3023 211 -35 S 302 VE ZL 0.00 -17.50 0.58 -17.50 3023 211 -35 S 317 VE ZL 0.00 -17.50 0.58 -17.50
3023 -35 -48 S 303 VE ZL 0.00 -17.50 0.58 -17.50 3024 -25 -36 S 314 VE ZL 0.00 -17.50 0.58 -17.50
3024 -25 -36 S 317 VE ZL 0.00 -17.50 0.58 -17.50 3025 -26 -37 S 314 VE ZL 0.00 -17.50 0.58 -17.50
3025 -67 -84 S 328 VE ZL 0.00 -17.50 0.58 -17.50 3039 -70 -71 S 330 VE YL 0.00 -0.00 0.70 -0.00
3039 -70 -71 S 330 VE ZL 0.00 -14.43 0.70 -14.43 3039 -70 -71 S 331 VE YL 0.00 -0.00 3.50 -

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0.00
3039 -70 -71 S 331 VE ZL 0.00  -14.43 3.50  -14.43   3039 -70 -71 S 330 VE YL 2.10   -0.00 3.50   -
0.00
3039 -70 -71 S 330 VE ZL 2.10  -14.43 3.50  -14.43   3039 -70 -71 S 330 VE YL 1.40   -0.00 2.10   -
0.00
3039 -70 -71 S 330 VE ZL 1.40  -14.43 2.10  -14.43   3039 -70 -71 S 330 VE YL 0.70   -0.00 1.40   -
0.00
3039 -70 -71 S 330 VE ZL 0.70  -14.43 1.40  -14.43   3047 -58 -75 S 320 VE ZL 0.00  -18.75 0.58  -
18.75
3047 -58 -75 S 321 VE ZL 0.00  -18.75 0.58  -18.75   3049 -60 -77 S 322 VE ZL 0.00  -17.50 0.58  -
17.50
3049 -60 -77 S 323 VE ZL 0.00  -17.50 0.58  -17.50   3050 -61 -78 S 323 VE ZL 0.00  -17.50 0.58  -
17.50
3050 -61 -78 S 324 VE ZL 0.00  -17.50 0.58  -17.50   3051 -62 -79 S 324 VE ZL 0.00  -17.50 0.58  -
17.50
3051 -62 -79 S 326 VE ZL 0.00  -17.50 0.58  -17.50   3052 -63 -80 S 325 VE ZL 0.00  -17.50 0.58  -
17.50
3052 -63 -80 S 326 VE ZL 0.00  -17.50 0.58  -17.50   3054 -65 -82 S 327 VE ZL 0.00  -17.50 0.58  -
17.50
3054 -65 -82 S 329 VE ZL 0.00  -17.50 0.58  -17.50   3055 -66 -83 S 328 VE ZL 0.00  -17.50 0.58  -
17.50
3055 -66 -83 S 329 VE ZL 0.00  -17.50 0.58  -17.50   5012  27 -14 T 214 VE ZL 0.20  -12.50 2.20  -
12.50
5012  27 -14 T 114 VE ZL 0.00  -12.50 2.20  -12.50   5012  27 -14 T 214 VE ZL 0.00  -12.50 0.20  -
12.50
5043  26 -16 T 214 VE ZL 0.00  -12.50 2.00  -12.50   5043 -17  26 T 214 VE ZL 0.00  -12.50 0.20  -
12.50
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CONDIZIONE DI CARICO 8: Vento X-_1

CARICHI DISTRIBUITI

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Asta  N1  N2 E  NE  T DC  Xi     Qi     Xf     Qf     Asta  N1  N2 E  NE  T DC  Xi     Qi     Xf     Qf
                        <m> <daN/m>  <m> <daN/m>                        <m> <daN/m>  <m>
<daN/m>
-------------------------------------------------  -------------------------------------------------
--
   0 143  45 T 126 VE YL 0.00  -12.38 2.30  -12.38      0 143  45 T 126 VE ZL 0.00   -5.13 2.30   -
5.13
   0 143  45 T 128 VE YL 0.00   -5.12 2.30   -5.12      0 143  45 T 128 VE ZL 0.00  -13.62 2.30  -
13.62
   0 145  46 T 129 VE YL 0.00    3.36 2.30    3.36      0 145  46 T 129 VE ZL 0.00  -12.91 2.30  -
12.91
   0 145  46 T 127 VE YL 0.00  -14.14 2.30  -14.14      0 145  46 T 127 VE ZL 0.00    5.84 2.30
5.84
   0  18  48 T 233 VE YL 0.00    0.00 0.56   -5.67      0  48  21 T 233 VE YL 0.00   -2.44 0.54   -
7.18
   0  49  21 T 134 VE YL 0.00    2.44 0.54    7.18      0  23  49 T 134 VE YL 0.00    0.00 0.56
5.67
  15 115 215 T 232 VE YL 0.00  -18.12 3.76  -18.12     16 116 216 T 232 VE ZL 0.00  -18.12 3.76  -
18.12
  16 116 216 T 133 VE ZL 0.00  -18.12 2.30  -18.12     16 116 216 T 133 VE ZL 2.30  -18.12 3.76  -
18.12
  18 118  18 T 133 VE ZL 0.00  -18.12 2.30  -18.12     18 118  18 T 126 VE YL 0.00  -12.38 2.30  -
12.38
  18 118  18 T 126 VE ZL 0.00   -5.13 2.30   -5.13     18  18 218 T 133 VE ZL 0.00  -18.12 1.46  -
18.12
  18  18 218 T 233 VE ZL 0.00    0.00 0.49   -6.38     18  18 218 T 233 VE ZL 0.49   -6.38 0.70  -
18.75
  18  18 218 T 233 VE ZL 0.70  -18.75 1.46  -18.75     19 119  19 T 128 VE YL 0.00   -5.12 2.30   -
5.12
  19 119  19 T 128 VE ZL 0.00  -13.62 2.30  -13.62     19 119  19 T 129 VE YL 0.00    3.36 2.30
3.36
  19 119  19 T 129 VE ZL 0.00  -12.91 2.30  -12.91     21  21 221 T 233 VE ZL 0.00  -18.75 0.76  -
18.75
  21  21 221 T 134 VE ZL 0.00  -18.75 0.76  -18.75     23 123  23 T 135 VE ZL 0.00  -18.12 2.30  -
18.12
  23 123  23 T 127 VE YL 0.00  -14.14 2.30  -14.14     23 123  23 T 127 VE ZL 0.00    5.84 2.30
5.84
  23  23 223 T 135 VE ZL 0.00  -18.12 1.46  -18.12     23  23 223 T 134 VE ZL 0.00    0.00 0.49   -
6.38
  23  23 223 T 134 VE ZL 0.49   -6.38 0.70  -18.75     23  23 223 T 134 VE ZL 0.70  -18.75 1.46  -
18.75
  24 124 224 T 136 VE ZL 1.70  -18.12 3.76  -18.12     24 124 224 T 135 VE ZL 0.00  -18.12 2.30  -
18.12
  24 124 224 T 135 VE ZL 2.30  -18.12 3.76  -18.12     24 124 224 T 136 VE ZL 0.00  -18.12 1.70  -
18.12
  42 142 -19 T 136 VE YL 0.00  -18.12 1.70  -18.12     42 -19 242 T 136 VE YL 0.00  -18.12 2.06  -
18.12
1013 101  -1 T 130 VE YL 0.00  -25.00 0.72  -25.00   1013  -1 117 T 130 VE YL 0.00  -25.00 0.72  -
25.00
1013 122 -11 T 132 VE YL 0.00  -25.00 0.72  -25.00   1013 -11 125 T 132 VE YL 0.00  -25.00 0.72  -
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25.00
2013 201 220 T 330 VE YL 0.00    0.00 1.10   -8.75   2013 201 220 T 230 VE YL 1.45  -36.50 2.20  -
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2013 201 220 T 230 VE YL 0.00  -69.00 1.45  -69.00   2013 201 220 T 330 VE YL 1.65  -13.12 2.20  -
17.50
2013 201 220 T 330 VE YL 1.10   -8.75 1.65  -13.12   2013 220 225 T 131 VE YL 0.00  -36.50 0.75  -
36.50
2013 220 225 T 330 VE YL 1.10   -8.75 2.20    0.00   2013 220 225 T 330 VE YL 0.55  -13.12 1.10   -
8.75
2013 220 225 T 330 VE YL 0.00  -17.50 0.55  -13.12   2013 220 225 T 131 VE YL 0.75  -69.00 2.20  -
69.00
2026 215 216 T 333 VE YL 0.00    0.00 0.72   -5.77   2026 216 218 T 333 VE YL 0.00   -5.77 0.38   -
8.75
2026 216 218 T 333 VE YL 0.38   -8.75 0.72  -11.53   2026 218 221 T 333 VE YL 0.00  -11.53 0.75  -
17.50
2026 221 223 T 333 VE YL 0.00  -17.50 0.55  -13.12   2026 221 223 T 333 VE YL 0.55  -13.12 0.75  -
11.53
2026 223 224 T 333 VE YL 0.00  -11.53 0.35   -8.75   2026 223 224 T 333 VE YL 0.35   -8.75 0.72   -
5.77
2026 224 242 T 333 VE YL 0.00   -5.77 0.72    0.00   3007 -72 -73 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -72 -73 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -73 -74 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -73 -74 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -74 -75 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -74 -75 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -75 -76 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -75 -76 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -81 -82 S 330 VE YL 0.00   -4.38 0.70   -
4.38
3007 -81 -82 S 330 VE ZL 0.00  -13.75 0.70  -13.75   3007 -82 -83 S 330 VE YL 0.00   -4.38 0.70   -
4.38
3007 -82 -83 S 330 VE ZL 0.00  -13.75 0.70  -13.75   3007 -83 -84 S 330 VE YL 0.00   -4.38 0.70   -
4.38
3007 -83 -84 S 330 VE ZL 0.00  -13.75 0.70  -13.75   3007 -84 -85 S 330 VE YL 0.00   -4.38 1.40   -
4.38
3007 -84 -85 S 330 VE ZL 0.00  -13.75 1.40  -13.75   3008 -68 -69 S 334 VE YL 0.00   -0.00 0.75   -
0.00
3008 -68 -69 S 334 VE ZL 0.00  -14.43 0.75  -14.43   3008 -68 -69 S 335 VE YL 0.00   -0.00 3.00   -
0.00
3008 -68 -69 S 335 VE ZL 0.00  -14.43 3.00  -14.43   3008 -68 -69 S 334 VE YL 2.25   -0.00 3.00   -
0.00
3008 -68 -69 S 334 VE ZL 2.25  -14.43 3.00  -14.43   3008 -68 -69 S 334 VE YL 1.50   -0.00 2.25   -
0.00
3008 -68 -69 S 334 VE ZL 1.50  -14.43 2.25  -14.43   3008 -68 -69 S 334 VE YL 0.75   -0.00 1.50   -
0.00
3008 -68 -69 S 334 VE ZL 0.75  -14.43 1.50  -14.43   3010 -51 -52 S 335 VE YL 0.00   -0.00 3.00   -
0.00
3010 -51 -52 S 335 VE ZL 0.00  -14.43 3.00  -14.43   3010 -53 -54 S 331 VE YL 0.00   -0.00 3.50   -
0.00
3010 -53 -54 S 331 VE ZL 0.00  -14.43 3.50  -14.43   3013 201 -38 T 330 VE YL 0.00    0.00 1.15   -
8.34
3013 -38 -55 S 301 VE ZL 0.00  -18.75 0.58  -18.75   3013 -38 -55 T 330 VE YL 0.00   -8.34 0.58  -
12.51
3013 -55 -72 S 319 VE ZL 0.00  -18.75 0.58  -18.75   3013 -55 -72 T 330 VE YL 0.00  -12.51 0.58  -
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3014 -39 -56 S 300 VE ZL 0.00  -18.75 0.58  -18.75   3014 -39 -56 S 301 VE ZL 0.00  -18.75 0.58  -
18.75
3014 -56 -73 S 318 VE ZL 0.00  -18.75 0.58  -18.75   3014 -56 -73 S 319 VE ZL 0.00  -18.75 0.58  -
18.75
3015 -24 -27 S 316 VE ZL 0.00  -18.75 0.58  -18.75   3015 -27 -40 S 333 VE ZL 0.00  -18.75 0.58  -
18.75
3015 -40 -57 S 300 VE ZL 0.00  -18.75 0.58  -18.75   3015 -57 -74 S 318 VE ZL 0.00  -18.75 0.58  -
18.75
3015 -57 -74 S 321 VE ZL 0.00  -18.75 0.58  -18.75   3016 204 -28 S 315 VE ZL 0.00  -18.75 0.58  -
18.75
3016 204 -28 S 316 VE ZL 0.00  -18.75 0.58  -18.75   3016 -28 -41 S 332 VE ZL 0.00  -18.75 0.58  -
18.75
3016 -28 -41 S 333 VE ZL 0.00  -18.75 0.58  -18.75   3017 205 -29 S 312 VE ZL 0.00  -17.50 0.58  -
17.50
3017 205 -29 S 315 VE ZL 0.00  -18.75 0.58  -18.75   3017 -29 -42 S 313 VE ZL 0.00  -17.50 0.58  -
17.50
3017 -29 -42 S 332 VE ZL 0.00  -18.75 0.58  -18.75   3017 -59 -76 S 320 VE ZL 0.00  -18.75 0.58  -
18.75
3017 -59 -76 S 322 VE ZL 0.00  -17.50 0.58  -17.50   3018 206 -30 S 311 VE ZL 0.00  -17.50 0.58  -
17.50
3018 206 -30 S 312 VE ZL 0.00  -17.50 0.58  -17.50   3018 -30 -43 S 310 VE ZL 0.00  -17.50 0.58  -
17.50
3018 -30 -43 S 313 VE ZL 0.00  -17.50 0.58  -17.50   3019 207 -31 S 308 VE ZL 0.00  -17.50 0.58  -
17.50
3019 207 -31 S 311 VE ZL 0.00  -17.50 0.58  -17.50   3019 -31 -44 S 309 VE ZL 0.00  -17.50 0.58  -
17.50
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3019 -31 -44 S 310 VE ZL 0.00 -17.50 0.58 -17.50 3020 208 -32 S 307 VE ZL 0.00 -17.50 0.58 -17.50
3020 208 -32 S 308 VE ZL 0.00 -17.50 0.58 -17.50 3020 -32 -45 S 306 VE ZL 0.00 -17.50 0.58 -17.50
3020 -32 -45 S 309 VE ZL 0.00 -17.50 0.58 -17.50 3021 209 -33 S 304 VE ZL 0.00 -17.50 0.58 -17.50
3021 209 -33 S 307 VE ZL 0.00 -17.50 0.58 -17.50 3021 -33 -46 S 305 VE ZL 0.00 -17.50 0.58 -17.50
3021 -33 -46 S 306 VE ZL 0.00 -17.50 0.58 -17.50 3022 210 -34 S 302 VE ZL 0.00 -17.50 0.58 -17.50
3022 210 -34 S 304 VE ZL 0.00 -17.50 0.58 -17.50 3022 -34 -47 S 303 VE ZL 0.00 -17.50 0.58 -17.50
3022 -34 -47 S 305 VE ZL 0.00 -17.50 0.58 -17.50 3022 -64 -81 S 325 VE ZL 0.00 -17.50 0.58 -17.50
3022 -64 -81 S 327 VE ZL 0.00 -17.50 0.58 -17.50 3023 211 -35 S 302 VE ZL 0.00 -17.50 0.58 -17.50
3023 211 -35 S 317 VE ZL 0.00 -17.50 0.58 -17.50 3023 -35 -48 S 303 VE ZL 0.00 -17.50 0.58 -17.50
3024 -25 -36 S 314 VE ZL 0.00 -17.50 0.58 -17.50 3024 -25 -36 S 317 VE ZL 0.00 -17.50 0.58 -17.50
3025 -26 -37 S 314 VE ZL 0.00 -17.50 0.58 -17.50 3025 -67 -84 S 328 VE ZL 0.00 -17.50 0.58 -17.50
3026 215 -50 T 333 VE YL 0.00 0.00 0.76 -5.50 3026 215 -50 T 333 VE YL 0.76 -5.50 1.15 -8.34
3026 -50 -85 T 333 VE YL 0.00 -8.34 0.37 -10.99 3026 -50 -85 T 333 VE YL 0.37 -10.99 1.15 -16.68
3039 -70 -71 S 330 VE YL 0.00 -0.00 0.70 -0.00 3039 -70 -71 S 330 VE ZL 0.00 -14.43 0.70 -14.43
3039 -70 -71 S 331 VE YL 0.00 -0.00 3.50 -0.00 3039 -70 -71 S 331 VE ZL 0.00 -14.43 3.50 -14.43
3039 -70 -71 S 330 VE YL 2.10 -0.00 3.50 -0.00 3039 -70 -71 S 330 VE ZL 2.10 -14.43 3.50 -14.43
3039 -70 -71 S 330 VE YL 1.40 -0.00 2.10 -0.00 3039 -70 -71 S 330 VE ZL 1.40 -14.43 2.10 -14.43
3039 -70 -71 S 330 VE YL 0.70 -0.00 1.40 -0.00 3039 -70 -71 S 330 VE ZL 0.70 -14.43 1.40 -14.43
3044 -72 -68 T 330 VE YL 0.00 -16.68 0.58 -12.51 3044 -68 -51 T 330 VE YL 0.00 -12.51 0.58 -8.34
3044 -51 225 T 330 VE YL 0.00 -8.34 1.15 0.00 3047 -58 -75 S 320 VE ZL 0.00 -18.75 0.58 -18.75
3047 -58 -75 S 321 VE ZL 0.00 -18.75 0.58 -18.75 3049 -60 -77 S 322 VE ZL 0.00 -17.50 0.58 -17.50
3049 -60 -77 S 323 VE ZL 0.00 -17.50 0.58 -17.50 3050 -61 -78 S 323 VE ZL 0.00 -17.50 0.58 -17.50
3050 -61 -78 S 324 VE ZL 0.00 -17.50 0.58 -17.50 3051 -62 -79 S 324 VE ZL 0.00 -17.50 0.58 -17.50
3051 -62 -79 S 326 VE ZL 0.00 -17.50 0.58 -17.50 3052 -63 -80 S 325 VE ZL 0.00 -17.50 0.58 -17.50
3052 -63 -80 S 326 VE ZL 0.00 -17.50 0.58 -17.50 3054 -65 -82 S 327 VE ZL 0.00 -17.50 0.58 -17.50
3054 -65 -82 S 329 VE ZL 0.00 -17.50 0.58 -17.50 3055 -66 -83 S 328 VE ZL 0.00 -17.50 0.58 -17.50
3055 -66 -83 S 329 VE ZL 0.00 -17.50 0.58 -17.50 3057 -85 -71 T 333 VE YL 0.00 -16.68 0.58 -12.51
3057 -71 -54 T 333 VE YL 0.00 -12.51 0.21 -10.99 3057 -71 -54 T 333 VE YL 0.21 -10.99 0.58 -8.34
3057 -54 242 T 333 VE YL 0.00 -8.34 0.39 -5.50 3057 -54 242 T 333 VE YL 0.39 -5.50 1.15 0.00
5013 -15 17 T 230 VE ZL 0.00 69.00 1.45 69.00 5013 -15 17 T 130 VE ZL 0.72 25.00 1.45 25.00
5013 -15 17 T 130 VE ZL 0.00 25.00 0.72 25.00 5044 44 20 T 230 VE ZL 0.00 36.50 0.75 36.50
5044 20 47 T 131 VE ZL 0.00 36.50 0.75 36.50 5075 22 -16 T 131 VE ZL 0.00 69.00 1.45 69.00
5075 22 -16 T 132 VE ZL 0.72 25.00 1.45 25.00 5075 22 -16 T 132 VE ZL 0.00 25.00 0.72 25.00

CONDIZIONE DI CARICO 9: Vento Y-_1

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
1	101	-15	T	101	VE	ZL	0.00	-23.75	1.00	-23.75	1	-15	201	T	101	VE	ZL	0.00	-23.75	2.76	-23.75
2	102	202	T	102	VE	ZL	2.86	-22.50	3.76	-22.50	2	102	202	T	101	VE	ZL	0.00	-23.75	1.00	-23.75
2	102	202	T	101	VE	ZL	1.00	-23.75	3.76	-23.75	2	102	202	T	102	VE	ZL	0.00	-22.50	2.16	-22.50

```
   2 102 202 T 102 VE ZL 2.16  -22.50 2.86  -22.50      3 103   3 T 103 VE ZL 0.00  -10.00 2.16  -
10.00
   3 103   3 T 102 VE ZL 0.00  -22.50 2.16  -22.50      3   3 -20 T 102 VE ZL 0.00  -22.50 0.70  -
22.50
   3 -20 203 T 203 VE ZL 0.00  -10.00 0.90  -10.00      3 -20 203 T 102 VE ZL 0.00  -22.50 0.90  -
22.50
   4 104   4 T 104 VE ZL 1.60  -18.75 2.16  -18.75      4 104   4 T 103 VE ZL 0.00  -10.00 2.16  -
10.00
   4 104   4 T 104 VE ZL 0.00  -18.75 1.60  -18.75      4   4 -21 T 104 VE ZL 0.00  -18.75 0.70  -
18.75
   4 -21 204 T 104 VE ZL 0.00  -18.75 0.90  -18.75      4 -21 204 T 203 VE ZL 0.00  -10.00 0.90  -
10.00
   5 105  43 T 104 VE ZL 0.00  -18.75 1.60  -18.75      5  43 205 T 204 VE ZL 0.00  -17.50 2.16  -
17.50
   5  43 205 T 104 VE ZL 0.00  -18.75 0.56  -18.75      5  43 205 T 104 VE ZL 0.56  -18.75 1.26  -
18.75
   5  43 205 T 104 VE ZL 1.26  -18.75 2.16  -18.75      6 106   6 T 105 VE ZL 0.00  -17.50 1.60  -
17.50
   6   6 206 T 105 VE ZL 0.00  -17.50 2.16  -17.50      6   6 206 T 204 VE ZL 0.00  -17.50 2.16  -
17.50
   7 107 207 T 106 VE ZL 0.00  -17.50 3.76  -17.50      7 107 207 T 105 VE ZL 0.00  -17.50 1.60  -
17.50
   7 107 207 T 105 VE ZL 1.60  -17.50 3.76  -17.50      8 108 208 T 107 VE ZL 0.00  -17.50 3.76  -
17.50
   8 108 208 T 106 VE ZL 0.00  -17.50 3.76  -17.50      9 109 209 T 107 VE ZL 0.00  -17.50 3.76  -
17.50
   9 109 209 T 108 VE ZL 0.00  -17.50 3.76  -17.50     10 110 210 T 109 VE ZL 2.86  -17.50 3.76  -
17.50
  10 110 210 T 108 VE ZL 0.00  -17.50 3.76  -17.50     10 110 210 T 109 VE ZL 0.00  -17.50 2.16  -
17.50
  10 110 210 T 109 VE ZL 2.16  -17.50 2.86  -17.50     11 111  11 T 110 VE ZL 0.00  -10.00 2.16  -
10.00
  11 111  11 T 109 VE ZL 0.00  -17.50 2.16  -17.50     11  11 -22 T 109 VE ZL 0.00  -17.50 0.70  -
17.50
  11 -22 211 T 109 VE ZL 0.00  -17.50 0.90  -17.50     11 -22 211 T 210 VE ZL 0.00  -10.00 0.90  -
10.00
  12 112  12 T 110 VE ZL 0.00  -10.00 2.16  -10.00     12 112  12 T 111 VE ZL 0.00  -20.00 2.16  -
20.00
  12  12 -23 T 111 VE ZL 0.00  -20.00 0.70  -20.00     12 -23 212 T 111 VE ZL 0.00  -20.00 0.90  -
20.00
  12 -23 212 T 210 VE ZL 0.00  -10.00 0.90  -10.00     13 113 213 T 111 VE ZL 2.86  -20.00 3.76  -
20.00
  13 113 213 T 112 VE ZL 0.00  -20.00 3.76  -20.00     13 113 213 T 111 VE ZL 0.00  -20.00 2.16  -
20.00
  13 113 213 T 111 VE ZL 2.16  -20.00 2.86  -20.00     14 114 214 T 113 VE ZL 0.00  -20.00 3.76  -
20.00
  14 114 214 T 112 VE ZL 0.00  -20.00 3.76  -20.00     15 115 215 T 113 VE ZL 0.00  -20.00 3.76  -
20.00
  26  26 226 T 314 VE ZL 0.00  -15.00 2.76  -15.00     27 127  27 T 115 VE ZL 0.00  -10.00 0.50  -
10.00
  27  27 -17 T 115 VE ZL 0.00  -10.00 0.50  -10.00     28 128  28 T 115 VE ZL 0.50  -10.00 1.00  -
10.00
  28 128  28 T 115 VE ZL 0.00  -10.00 0.50  -10.00     28  28 228 T 314 VE ZL 0.00  -15.00 2.76  -
15.00
  29 129 -18 T 215 VE ZL 0.00  -10.00 1.70  -10.00     29 -18 229 T 315 VE ZL 0.00  -10.00 2.06  -
10.00
  30 130  30 T 215 VE ZL 0.00  -10.00 1.70  -10.00     30  30 230 T 116 VE ZL 0.00  -15.50 2.06  -
15.50
  30  30 230 T 315 VE ZL 0.00  -10.00 2.06  -10.00     31  31 231 T 117 VE ZL 0.00  -15.50 2.06  -
15.50
  31  31 231 T 116 VE ZL 0.00  -15.50 2.06  -15.50     32  32 232 T 118 VE ZL 0.00  -15.50 2.06  -
15.50
  32  32 232 T 117 VE ZL 0.00  -15.50 2.06  -15.50     33  33 233 T 119 VE ZL 0.00  -15.50 2.06  -
15.50
  33  33 233 T 118 VE ZL 0.00  -15.50 2.06  -15.50     34  34 234 T 120 VE ZL 0.00  -15.50 2.06  -
15.50
  34  34 234 T 119 VE ZL 0.00  -15.50 2.06  -15.50     36  36 236 T 120 VE ZL 0.00  -15.50 2.06  -
15.50
  37  37 237 T 121 VE ZL 0.00  -15.50 2.06  -15.50     38  38 238 T 122 VE ZL 0.00  -15.50 2.06  -
15.50
  38  38 238 T 121 VE ZL 0.00  -15.50 2.06  -15.50     39  39 239 T 123 VE ZL 0.00  -15.50 2.06  -
15.50
  39  39 239 T 122 VE ZL 0.00  -15.50 2.06  -15.50     40  40 240 T 124 VE ZL 0.00  -15.50 2.06  -
15.50
  40  40 240 T 123 VE ZL 0.00  -15.50 2.06  -15.50     41  41 241 T 125 VE ZL 0.00  -15.50 2.06  -
15.50
  41  41 241 T 124 VE ZL 0.00  -15.50 2.06  -15.50     42 -19 242 T 125 VE ZL 0.00  -15.50 2.06  -
15.50
1012 125 127 T 114 VE YL 0.00   12.50 2.20   12.50   3007 -72 -73 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -72 -73 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -73 -74 S 334 VE YL 0.00   -4.38 0.75   -
```

```
4.38
3007 -73 -74 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -74 -75 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -74 -75 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -75 -76 S 334 VE YL 0.00   -4.38 0.75   -
4.38
3007 -75 -76 S 334 VE ZL 0.00  -13.75 0.75  -13.75   3007 -81 -82 S 330 VE YL 0.00   -4.38 0.70   -
4.38
3007 -81 -82 S 330 VE ZL 0.00  -13.75 0.70  -13.75   3007 -82 -83 S 330 VE YL 0.00   -4.38 0.70   -
4.38
3007 -82 -83 S 330 VE ZL 0.00  -13.75 0.70  -13.75   3007 -83 -84 S 330 VE YL 0.00   -4.38 0.70   -
4.38
3007 -83 -84 S 330 VE ZL 0.00  -13.75 0.70  -13.75   3007 -84 -85 S 330 VE YL 0.00   -4.38 1.40   -
4.38
3007 -84 -85 S 330 VE ZL 0.00  -13.75 1.40  -13.75   3008 -68 -69 S 334 VE YL 0.00   -0.00 0.75   -
0.00
3008 -68 -69 S 334 VE ZL 0.00  -14.43 0.75  -14.43   3008 -68 -69 S 335 VE YL 0.00   -0.00 3.00   -
0.00
3008 -68 -69 S 335 VE ZL 0.00  -14.43 3.00  -14.43   3008 -68 -69 S 334 VE YL 2.25   -0.00 3.00   -
0.00
3008 -68 -69 S 334 VE ZL 2.25  -14.43 3.00  -14.43   3008 -68 -69 S 334 VE YL 1.50   -0.00 2.25   -
0.00
3008 -68 -69 S 334 VE ZL 1.50  -14.43 2.25  -14.43   3008 -68 -69 S 334 VE YL 0.75   -0.00 1.50   -
0.00
3008 -68 -69 S 334 VE ZL 0.75  -14.43 1.50  -14.43   3010 -51 -52 S 335 VE YL 0.00   -0.00 3.00   -
0.00
3010 -51 -52 S 335 VE ZL 0.00  -14.43 3.00  -14.43   3010 -53 -54 S 331 VE YL 0.00   -0.00 3.50   -
0.00
3010 -53 -54 S 331 VE ZL 0.00  -14.43 3.50  -14.43   3013 -38 -55 S 301 VE ZL 0.00  -18.75 0.58  -
18.75
3013 -55 -72 S 319 VE ZL 0.00  -18.75 0.58  -18.75   3014 -39 -56 S 300 VE ZL 0.00  -18.75 0.58  -
18.75
3014 -39 -56 S 301 VE ZL 0.00  -18.75 0.58  -18.75   3014 -56 -73 S 318 VE ZL 0.00  -18.75 0.58  -
18.75
3014 -56 -73 S 319 VE ZL 0.00  -18.75 0.58  -18.75   3015 -24 -27 S 316 VE ZL 0.00  -18.75 0.58  -
18.75
3015 -27 -40 S 333 VE ZL 0.00  -18.75 0.58  -18.75   3015 -40 -57 S 300 VE ZL 0.00  -18.75 0.58  -
18.75
3015 -57 -74 S 318 VE ZL 0.00  -18.75 0.58  -18.75   3015 -57 -74 S 321 VE ZL 0.00  -18.75 0.58  -
18.75
3016 204 -28 S 315 VE ZL 0.00  -18.75 0.58  -18.75   3016 204 -28 S 316 VE ZL 0.00  -18.75 0.58  -
18.75
3016 -28 -41 S 332 VE ZL 0.00  -18.75 0.58  -18.75   3016 -28 -41 S 333 VE ZL 0.00  -18.75 0.58  -
18.75
3017 205 -29 S 312 VE ZL 0.00  -17.50 0.58  -17.50   3017 205 -29 S 315 VE ZL 0.00  -18.75 0.58  -
18.75
3017 -29 -42 S 313 VE ZL 0.00  -17.50 0.58  -17.50   3017 -29 -42 S 332 VE ZL 0.00  -18.75 0.58  -
18.75
3017 -59 -76 S 320 VE ZL 0.00  -18.75 0.58  -18.75   3017 -59 -76 S 322 VE ZL 0.00  -17.50 0.58  -
17.50
3018 206 -30 S 311 VE ZL 0.00  -17.50 0.58  -17.50   3018 206 -30 S 312 VE ZL 0.00  -17.50 0.58  -
17.50
3018 -30 -43 S 310 VE ZL 0.00  -17.50 0.58  -17.50   3018 -30 -43 S 313 VE ZL 0.00  -17.50 0.58  -
17.50
3019 207 -31 S 308 VE ZL 0.00  -17.50 0.58  -17.50   3019 207 -31 S 311 VE ZL 0.00  -17.50 0.58  -
17.50
3019 -31 -44 S 309 VE ZL 0.00  -17.50 0.58  -17.50   3019 -31 -44 S 310 VE ZL 0.00  -17.50 0.58  -
17.50
3020 208 -32 S 307 VE ZL 0.00  -17.50 0.58  -17.50   3020 208 -32 S 308 VE ZL 0.00  -17.50 0.58  -
17.50
3020 -32 -45 S 306 VE ZL 0.00  -17.50 0.58  -17.50   3020 -32 -45 S 309 VE ZL 0.00  -17.50 0.58  -
17.50
3021 209 -33 S 304 VE ZL 0.00  -17.50 0.58  -17.50   3021 209 -33 S 307 VE ZL 0.00  -17.50 0.58  -
17.50
3021 -33 -46 S 305 VE ZL 0.00  -17.50 0.58  -17.50   3021 -33 -46 S 306 VE ZL 0.00  -17.50 0.58  -
17.50
3022 210 -34 S 302 VE ZL 0.00  -17.50 0.58  -17.50   3022 210 -34 S 304 VE ZL 0.00  -17.50 0.58  -
17.50
3022 -34 -47 S 303 VE ZL 0.00  -17.50 0.58  -17.50   3022 -34 -47 S 305 VE ZL 0.00  -17.50 0.58  -
17.50
3022 -64 -81 S 325 VE ZL 0.00  -17.50 0.58  -17.50   3022 -64 -81 S 327 VE ZL 0.00  -17.50 0.58  -
17.50
3023 211 -35 S 302 VE ZL 0.00  -17.50 0.58  -17.50   3023 211 -35 S 317 VE ZL 0.00  -17.50 0.58  -
17.50
3023 -35 -48 S 303 VE ZL 0.00  -17.50 0.58  -17.50   3024 -25 -36 S 314 VE ZL 0.00  -17.50 0.58  -
17.50
3024 -25 -36 S 317 VE ZL 0.00  -17.50 0.58  -17.50   3025 -26 -37 S 314 VE ZL 0.00  -17.50 0.58  -
17.50
3025 -67 -84 S 328 VE ZL 0.00  -17.50 0.58  -17.50   3039 -70 -71 S 330 VE YL 0.00   -0.00 0.70   -
0.00
3039 -70 -71 S 330 VE ZL 0.00  -14.43 0.70  -14.43   3039 -70 -71 S 331 VE YL 0.00   -0.00 3.50   -
0.00
3039 -70 -71 S 331 VE ZL 0.00  -14.43 3.50  -14.43   3039 -70 -71 S 330 VE YL 2.10   -0.00 3.50   -
0.00
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3039 -70 -71 S 330 VE ZL 2.10 -14.43 3.50 -14.43 3039 -70 -71 S 330 VE YL 1.40 -0.00 2.10 -0.00
3039 -70 -71 S 330 VE ZL 1.40 -14.43 2.10 -14.43 3039 -70 -71 S 330 VE YL 0.70 -0.00 1.40 -0.00
3039 -70 -71 S 330 VE ZL 0.70 -14.43 1.40 -14.43 3047 -58 -75 S 320 VE ZL 0.00 -18.75 0.58 -18.75
3047 -58 -75 S 321 VE ZL 0.00 -18.75 0.58 -18.75 3049 -60 -77 S 322 VE ZL 0.00 -17.50 0.58 -17.50
3049 -60 -77 S 323 VE ZL 0.00 -17.50 0.58 -17.50 3050 -61 -78 S 323 VE ZL 0.00 -17.50 0.58 -17.50
3050 -61 -78 S 324 VE ZL 0.00 -17.50 0.58 -17.50 3051 -62 -79 S 324 VE ZL 0.00 -17.50 0.58 -17.50
3051 -62 -79 S 326 VE ZL 0.00 -17.50 0.58 -17.50 3052 -63 -80 S 325 VE ZL 0.00 -17.50 0.58 -17.50
3052 -63 -80 S 326 VE ZL 0.00 -17.50 0.58 -17.50 3054 -65 -82 S 327 VE ZL 0.00 -17.50 0.58 -17.50
3054 -65 -82 S 329 VE ZL 0.00 -17.50 0.58 -17.50 3055 -66 -83 S 328 VE ZL 0.00 -17.50 0.58 -17.50
3055 -66 -83 S 329 VE ZL 0.00 -17.50 0.58 -17.50 5012 27 -14 T 214 VE ZL 0.20 12.50 2.20 12.50
5012 27 -14 T 114 VE ZL 0.00 12.50 2.20 12.50 5012 27 -14 T 214 VE ZL 0.00 12.50 0.20 12.50
5043 26 -16 T 214 VE ZL 0.00 12.50 2.00 12.50 5043 -17 26 T 214 VE ZL 0.00 12.50 0.20 12.50

CONDIZIONE DI CARICO 10: Vento X+_2

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
0	143	45	T	126	VE	YL	0.00	12.38	2.30	12.38	0	143	45	T	126	VE	ZL	0.00	5.13	2.30	5.13
0	143	45	T	128	VE	YL	0.00	5.12	2.30	5.12	0	143	45	T	128	VE	ZL	0.00	13.62	2.30	13.62
0	145	46	T	129	VE	YL	0.00	-3.36	2.30	-3.36	0	145	46	T	129	VE	ZL	0.00	12.91	2.30	12.91
0	145	46	T	127	VE	YL	0.00	14.14	2.30	14.14	0	145	46	T	127	VE	ZL	0.00	-5.84	2.30	-5.84
0	18	48	T	233	VE	YL	0.00	0.00	0.56	5.67	0	48	21	T	233	VE	YL	0.00	2.44	0.54	7.18
0	49	21	T	134	VE	YL	0.00	-2.44	0.54	-7.18	0	23	49	T	134	VE	YL	0.00	0.00	0.56	-5.67
15	115	215	T	232	VE	YL	0.00	18.12	3.76	18.12	16	116	216	T	232	VE	ZL	0.00	18.12	3.76	18.12
16	116	216	T	133	VE	ZL	0.00	18.12	2.30	18.12	16	116	216	T	133	VE	ZL	2.30	18.12	3.76	18.12
18	118	18	T	133	VE	ZL	0.00	18.12	2.30	18.12	18	118	18	T	126	VE	YL	0.00	12.38	2.30	12.38
18	118	18	T	126	VE	ZL	0.00	5.13	2.30	5.13	18	18	218	T	133	VE	ZL	0.00	18.12	1.46	18.12
18	18	218	T	233	VE	ZL	0.00	0.00	0.49	6.38	18	18	218	T	233	VE	ZL	0.49	6.38	0.70	18.75
18	18	218	T	233	VE	ZL	0.70	18.75	1.46	18.75	19	119	19	T	128	VE	YL	0.00	5.12	2.30	5.12
19	119	19	T	128	VE	ZL	0.00	13.62	2.30	13.62	19	119	19	T	129	VE	YL	0.00	-3.36	2.30	-3.36
19	119	19	T	129	VE	ZL	0.00	12.91	2.30	12.91	21	21	221	T	233	VE	ZL	0.00	18.75	0.76	18.75
21	21	221	T	134	VE	ZL	0.00	18.75	0.76	18.75	23	123	23	T	135	VE	ZL	0.00	18.12	2.30	18.12
23	123	23	T	127	VE	YL	0.00	14.14	2.30	14.14	23	123	23	T	127	VE	ZL	0.00	-5.84	2.30	-5.84
23	23	223	T	135	VE	ZL	0.00	18.12	1.46	18.12	23	23	223	T	134	VE	ZL	0.00	0.00	0.49	6.38
23	23	223	T	134	VE	ZL	0.49	6.38	0.70	18.75	23	23	223	T	134	VE	ZL	0.70	18.75	1.46	18.75
24	124	224	T	136	VE	ZL	1.70	18.12	3.76	18.12	24	124	224	T	135	VE	ZL	0.00	18.12	2.30	18.12
24	124	224	T	135	VE	ZL	2.30	18.12	3.76	18.12	24	124	224	T	136	VE	ZL	0.00	18.12	1.70	18.12
42	142	-19	T	136	VE	YL	0.00	18.12	1.70	18.12	42	-19	242	T	136	VE	YL	0.00	18.12	2.06	18.12
1013	101	-1	T	130	VE	YL	0.00	25.00	0.72	25.00	1013	-1	117	T	130	VE	YL	0.00	25.00	0.72	25.00
1013	122	-11	T	132	VE	YL	0.00	25.00	0.72	25.00	1013	-11	125	T	132	VE	YL	0.00	25.00	0.72	25.00

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2013 201 220 T 330 VE YL 0.00     0.00 1.10     8.75   2013 201 220 T 230 VE YL 1.45    36.50 2.20
36.50
2013 201 220 T 230 VE YL 0.00    69.00 1.45    69.00   2013 201 220 T 330 VE YL 1.65    13.12 2.20
17.50
2013 201 220 T 330 VE YL 1.10     8.75 1.65    13.12   2013 220 225 T 131 VE YL 0.00    36.50 0.75
36.50
2013 220 225 T 330 VE YL 1.10     8.75 2.20     0.00   2013 220 225 T 330 VE YL 0.55    13.12 1.10
8.75
2013 220 225 T 330 VE YL 0.00    17.50 0.55    13.12   2013 220 225 T 131 VE YL 0.75    69.00 2.20
69.00
2026 215 216 T 333 VE YL 0.00     0.00 0.72     5.77   2026 216 218 T 333 VE YL 0.00     5.77 0.38
8.75
2026 216 218 T 333 VE YL 0.38     8.75 0.72    11.53   2026 218 221 T 333 VE YL 0.00    11.53 0.75
17.50
2026 221 223 T 333 VE YL 0.00    17.50 0.55    13.12   2026 221 223 T 333 VE YL 0.55    13.12 0.75
11.53
2026 223 224 T 333 VE YL 0.00    11.53 0.35     8.75   2026 223 224 T 333 VE YL 0.35     8.75 0.72
5.77
2026 224 242 T 333 VE YL 0.00     5.77 0.72     0.00   3007 -72 -73 S 334 VE YL 0.00     4.38 0.75
4.38
3007 -72 -73 S 334 VE ZL 0.00    13.75 0.75    13.75   3007 -73 -74 S 334 VE YL 0.00     4.38 0.75
4.38
3007 -73 -74 S 334 VE ZL 0.00    13.75 0.75    13.75   3007 -74 -75 S 334 VE YL 0.00     4.38 0.75
4.38
3007 -74 -75 S 334 VE ZL 0.00    13.75 0.75    13.75   3007 -75 -76 S 334 VE YL 0.00     4.38 0.75
4.38
3007 -75 -76 S 334 VE ZL 0.00    13.75 0.75    13.75   3007 -81 -82 S 330 VE YL 0.00     4.38 0.70
4.38
3007 -81 -82 S 330 VE ZL 0.00    13.75 0.70    13.75   3007 -82 -83 S 330 VE YL 0.00     4.38 0.70
4.38
3007 -82 -83 S 330 VE ZL 0.00    13.75 0.70    13.75   3007 -83 -84 S 330 VE YL 0.00     4.38 0.70
4.38
3007 -83 -84 S 330 VE ZL 0.00    13.75 0.70    13.75   3007 -84 -85 S 330 VE YL 0.00     4.38 1.40
4.38
3007 -84 -85 S 330 VE ZL 0.00    13.75 1.40    13.75   3008 -68 -69 S 334 VE YL 0.00     0.00 0.75
0.00
3008 -68 -69 S 334 VE ZL 0.00    14.43 0.75    14.43   3008 -68 -69 S 335 VE YL 0.00     0.00 3.00
0.00
3008 -68 -69 S 335 VE ZL 0.00    14.43 3.00    14.43   3008 -68 -69 S 334 VE YL 2.25     0.00 3.00
0.00
3008 -68 -69 S 334 VE ZL 2.25    14.43 3.00    14.43   3008 -68 -69 S 334 VE YL 1.50     0.00 2.25
0.00
3008 -68 -69 S 334 VE ZL 1.50    14.43 2.25    14.43   3008 -68 -69 S 334 VE YL 0.75     0.00 1.50
0.00
3008 -68 -69 S 334 VE ZL 0.75    14.43 1.50    14.43   3010 -51 -52 S 335 VE YL 0.00     0.00 3.00
0.00
3010 -51 -52 S 335 VE ZL 0.00    14.43 3.00    14.43   3010 -53 -54 S 331 VE YL 0.00     0.00 3.50
0.00
3010 -53 -54 S 331 VE ZL 0.00    14.43 3.50    14.43   3013 201 -38 T 330 VE YL 0.00     0.00 1.15
8.34
3013 -38 -55 S 301 VE ZL 0.00    18.75 0.58    18.75   3013 -38 -55 T 330 VE YL 0.00     8.34 0.58
12.51
3013 -55 -72 S 319 VE ZL 0.00    18.75 0.58    18.75   3013 -55 -72 T 330 VE YL 0.00    12.51 0.58
16.68
3014 -39 -56 S 300 VE ZL 0.00    18.75 0.58    18.75   3014 -39 -56 S 301 VE ZL 0.00    18.75 0.58
18.75
3014 -56 -73 S 318 VE ZL 0.00    18.75 0.58    18.75   3014 -56 -73 S 319 VE ZL 0.00    18.75 0.58
18.75
3015 -24 -27 S 316 VE ZL 0.00    18.75 0.58    18.75   3015 -27 -40 S 333 VE ZL 0.00    18.75 0.58
18.75
3015 -40 -57 S 300 VE ZL 0.00    18.75 0.58    18.75   3015 -57 -74 S 318 VE ZL 0.00    18.75 0.58
18.75
3015 -57 -74 S 321 VE ZL 0.00    18.75 0.58    18.75   3016 204 -28 S 315 VE ZL 0.00    18.75 0.58
18.75
3016 204 -28 S 316 VE ZL 0.00    18.75 0.58    18.75   3016 -28 -41 S 332 VE ZL 0.00    18.75 0.58
18.75
3016 -28 -41 S 333 VE ZL 0.00    18.75 0.58    18.75   3017 205 -29 S 312 VE ZL 0.00    17.50 0.58
17.50
3017 205 -29 S 315 VE ZL 0.00    18.75 0.58    18.75   3017 -29 -42 S 313 VE ZL 0.00    17.50 0.58
17.50
3017 -29 -42 S 332 VE ZL 0.00    18.75 0.58    18.75   3017 -59 -76 S 320 VE ZL 0.00    18.75 0.58
18.75
3017 -59 -76 S 322 VE ZL 0.00    17.50 0.58    17.50   3018 206 -30 S 311 VE ZL 0.00    17.50 0.58
17.50
3018 206 -30 S 312 VE ZL 0.00    17.50 0.58    17.50   3018 -30 -43 S 310 VE ZL 0.00    17.50 0.58
17.50
3018 -30 -43 S 313 VE ZL 0.00    17.50 0.58    17.50   3019 207 -31 S 308 VE ZL 0.00    17.50 0.58
17.50
3019 207 -31 S 311 VE ZL 0.00    17.50 0.58    17.50   3019 -31 -44 S 309 VE ZL 0.00    17.50 0.58
17.50
3019 -31 -44 S 310 VE ZL 0.00    17.50 0.58    17.50   3020 208 -32 S 307 VE ZL 0.00    17.50 0.58
17.50
3020 208 -32 S 308 VE ZL 0.00    17.50 0.58    17.50   3020 -32 -45 S 306 VE ZL 0.00    17.50 0.58
```

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17.50
3020 -32 -45 S 309 VE ZL 0.00   17.50 0.58   17.50   3021 209 -33 S 304 VE ZL 0.00   17.50 0.58
17.50
3021 209 -33 S 307 VE ZL 0.00   17.50 0.58   17.50   3021 -33 -46 S 305 VE ZL 0.00   17.50 0.58
17.50
3021 -33 -46 S 306 VE ZL 0.00   17.50 0.58   17.50   3022 210 -34 S 302 VE ZL 0.00   17.50 0.58
17.50
3022 210 -34 S 304 VE ZL 0.00   17.50 0.58   17.50   3022 -34 -47 S 303 VE ZL 0.00   17.50 0.58
17.50
3022 -34 -47 S 305 VE ZL 0.00   17.50 0.58   17.50   3022 -64 -81 S 325 VE ZL 0.00   17.50 0.58
17.50
3022 -64 -81 S 327 VE ZL 0.00   17.50 0.58   17.50   3023 211 -35 S 302 VE ZL 0.00   17.50 0.58
17.50
3023 211 -35 S 317 VE ZL 0.00   17.50 0.58   17.50   3023 -35 -48 S 303 VE ZL 0.00   17.50 0.58
17.50
3024 -25 -36 S 314 VE ZL 0.00   17.50 0.58   17.50   3024 -25 -36 S 317 VE ZL 0.00   17.50 0.58
17.50
3025 -26 -37 S 314 VE ZL 0.00   17.50 0.58   17.50   3025 -67 -84 S 328 VE ZL 0.00   17.50 0.58
17.50
3026 215 -50 T 333 VE YL 0.00    0.00 0.76    5.50   3026 215 -50 T 333 VE YL 0.76    5.50 1.15
8.34
3026 -50 -85 T 333 VE YL 0.00    8.34 0.37   10.99   3026 -50 -85 T 333 VE YL 0.37   10.99 1.15
16.68
3039 -70 -71 S 330 VE YL 0.00    0.00 0.70    0.00   3039 -70 -71 S 330 VE ZL 0.00   14.43 0.70
14.43
3039 -70 -71 S 331 VE YL 0.00    0.00 3.50    0.00   3039 -70 -71 S 331 VE ZL 0.00   14.43 3.50
14.43
3039 -70 -71 S 330 VE YL 2.10    0.00 3.50    0.00   3039 -70 -71 S 330 VE ZL 2.10   14.43 3.50
14.43
3039 -70 -71 S 330 VE YL 1.40    0.00 2.10    0.00   3039 -70 -71 S 330 VE ZL 1.40   14.43 2.10
14.43
3039 -70 -71 S 330 VE YL 0.70    0.00 1.40    0.00   3039 -70 -71 S 330 VE ZL 0.70   14.43 1.40
14.43
3044 -72 -68 T 330 VE YL 0.00   16.68 0.58   12.51   3044 -68 -51 T 330 VE YL 0.00   12.51 0.58
8.34
3044 -51 225 T 330 VE YL 0.00    8.34 1.15    0.00   3047 -58 -75 S 320 VE ZL 0.00   18.75 0.58
18.75
3047 -58 -75 S 321 VE ZL 0.00   18.75 0.58   18.75   3049 -60 -77 S 322 VE ZL 0.00   17.50 0.58
17.50
3049 -60 -77 S 323 VE ZL 0.00   17.50 0.58   17.50   3050 -61 -78 S 323 VE ZL 0.00   17.50 0.58
17.50
3050 -61 -78 S 324 VE ZL 0.00   17.50 0.58   17.50   3051 -62 -79 S 324 VE ZL 0.00   17.50 0.58
17.50
3051 -62 -79 S 326 VE ZL 0.00   17.50 0.58   17.50   3052 -63 -80 S 325 VE ZL 0.00   17.50 0.58
17.50
3052 -63 -80 S 326 VE ZL 0.00   17.50 0.58   17.50   3054 -65 -82 S 327 VE ZL 0.00   17.50 0.58
17.50
3054 -65 -82 S 329 VE ZL 0.00   17.50 0.58   17.50   3055 -66 -83 S 328 VE ZL 0.00   17.50 0.58
17.50
3055 -66 -83 S 329 VE ZL 0.00   17.50 0.58   17.50   3057 -85 -71 T 333 VE YL 0.00   16.68 0.58
12.51
3057 -71 -54 T 333 VE YL 0.00   12.51 0.21   10.99   3057 -71 -54 T 333 VE YL 0.21   10.99 0.58
8.34
3057 -54 242 T 333 VE YL 0.00    8.34 0.39    5.50   3057 -54 242 T 333 VE YL 0.39    5.50 1.15
0.00
5013 -15  17 T 230 VE ZL 0.00  -69.00 1.45  -69.00   5013 -15  17 T 130 VE ZL 0.72  -25.00 1.45  -
25.00
5013 -15  17 T 130 VE ZL 0.00  -25.00 0.72  -25.00   5044  44  20 T 230 VE ZL 0.00  -36.50 0.75  -
36.50
5044  20  47 T 131 VE ZL 0.00  -36.50 0.75  -36.50   5075  22 -16 T 131 VE ZL 0.00  -69.00 1.45  -
69.00
5075  22 -16 T 132 VE ZL 0.72  -25.00 1.45  -25.00   5075  22 -16 T 132 VE ZL 0.00  -25.00 0.72  -
25.00


CONDIZIONE DI CARICO 11: Vento Y+_2

CARICHI DISTRIBUITI

Asta  N1  N2 E  NE  T DC  Xi     Qi     Xf     Qf     Asta  N1  N2 E  NE  T DC  Xi     Qi     Xf     Qf
                          <m> <daN/m>  <m> <daN/m>                          <m> <daN/m>  <m> <daN/m>
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--
   1 101 -15 T 101 VE ZL 0.00   23.75 1.00   23.75      1 -15 201 T 101 VE ZL 0.00   23.75 2.76
23.75
   2 102 202 T 102 VE ZL 2.86   22.50 3.76   22.50      2 102 202 T 101 VE ZL 0.00   23.75 1.00
23.75
   2 102 202 T 101 VE ZL 1.00   23.75 3.76   23.75      2 102 202 T 102 VE ZL 0.00   22.50 2.16
22.50
   2 102 202 T 102 VE ZL 2.16   22.50 2.86   22.50      3 103   3 T 103 VE ZL 0.00   10.00 2.16
```

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10.00
   3 103   3 T 102 VE ZL 0.00   22.50 2.16   22.50      3   3 -20 T 102 VE ZL 0.00   22.50 0.70
22.50
   3 -20 203 T 203 VE ZL 0.00   10.00 0.90   10.00      3 -20 203 T 102 VE ZL 0.00   22.50 0.90
22.50
   4 104   4 T 104 VE ZL 1.60   18.75 2.16   18.75      4 104   4 T 103 VE ZL 0.00   10.00 2.16
10.00
   4 104   4 T 104 VE ZL 0.00   18.75 1.60   18.75      4   4 -21 T 104 VE ZL 0.00   18.75 0.70
18.75
   4 -21 204 T 104 VE ZL 0.00   18.75 0.90   18.75      4 -21 204 T 203 VE ZL 0.00   10.00 0.90
10.00
   5 105  43 T 104 VE ZL 0.00   18.75 1.60   18.75      5  43 205 T 204 VE ZL 0.00   17.50 2.16
17.50
   5  43 205 T 104 VE ZL 0.00   18.75 0.56   18.75      5  43 205 T 104 VE ZL 0.56   18.75 1.26
18.75
   5  43 205 T 104 VE ZL 1.26   18.75 2.16   18.75      6 106   6 T 105 VE ZL 0.00   17.50 1.60
17.50
   6   6 206 T 105 VE ZL 0.00   17.50 2.16   17.50      6   6 206 T 204 VE ZL 0.00   17.50 2.16
17.50
   7 107 207 T 106 VE ZL 0.00   17.50 3.76   17.50      7 107 207 T 105 VE ZL 0.00   17.50 1.60
17.50
   7 107 207 T 105 VE ZL 1.60   17.50 3.76   17.50      8 108 208 T 107 VE ZL 0.00   17.50 3.76
17.50
   8 108 208 T 106 VE ZL 0.00   17.50 3.76   17.50      9 109 209 T 107 VE ZL 0.00   17.50 3.76
17.50
   9 109 209 T 108 VE ZL 0.00   17.50 3.76   17.50     10 110 210 T 109 VE ZL 2.86   17.50 3.76
17.50
  10 110 210 T 108 VE ZL 0.00   17.50 3.76   17.50     10 110 210 T 109 VE ZL 0.00   17.50 2.16
17.50
  10 110 210 T 109 VE ZL 2.16   17.50 2.86   17.50     11 111  11 T 110 VE ZL 0.00   10.00 2.16
10.00
  11 111  11 T 109 VE ZL 0.00   17.50 2.16   17.50     11  11 -22 T 109 VE ZL 0.00   17.50 0.70
17.50
  11 -22 211 T 109 VE ZL 0.00   17.50 0.90   17.50     11 -22 211 T 210 VE ZL 0.00   10.00 0.90
10.00
  12 112  12 T 110 VE ZL 0.00   10.00 2.16   10.00     12 112  12 T 111 VE ZL 0.00   20.00 2.16
20.00
  12  12 -23 T 111 VE ZL 0.00   20.00 0.70   20.00     12 -23 212 T 111 VE ZL 0.00   20.00 0.90
20.00
  12 -23 212 T 210 VE ZL 0.00   10.00 0.90   10.00     13 113 213 T 111 VE ZL 2.86   20.00 3.76
20.00
  13 113 213 T 112 VE ZL 0.00   20.00 3.76   20.00     13 113 213 T 111 VE ZL 0.00   20.00 2.16
20.00
  13 113 213 T 111 VE ZL 2.16   20.00 2.86   20.00     14 114 214 T 113 VE ZL 0.00   20.00 3.76
20.00
  14 114 214 T 112 VE ZL 0.00   20.00 3.76   20.00     15 115 215 T 113 VE ZL 0.00   20.00 3.76
20.00
  26  26 226 T 314 VE ZL 0.00   15.00 2.76   15.00     27 127  27 T 115 VE ZL 0.00   10.00 0.50
10.00
  27  27 -17 T 115 VE ZL 0.00   10.00 0.50   10.00     28 128  28 T 115 VE ZL 0.50   10.00 1.00
10.00
  28 128  28 T 115 VE ZL 0.00   10.00 0.50   10.00     28  28 228 T 314 VE ZL 0.00   15.00 2.76
15.00
  29 129 -18 T 215 VE ZL 0.00   10.00 1.70   10.00     29 -18 229 T 315 VE ZL 0.00   10.00 2.06
10.00
  30 130  30 T 215 VE ZL 0.00   10.00 1.70   10.00     30  30 230 T 116 VE ZL 0.00   15.50 2.06
15.50
  30  30 230 T 315 VE ZL 0.00   10.00 2.06   10.00     31  31 231 T 117 VE ZL 0.00   15.50 2.06
15.50
  31  31 231 T 116 VE ZL 0.00   15.50 2.06   15.50     32  32 232 T 118 VE ZL 0.00   15.50 2.06
15.50
  32  32 232 T 117 VE ZL 0.00   15.50 2.06   15.50     33  33 233 T 119 VE ZL 0.00   15.50 2.06
15.50
  33  33 233 T 118 VE ZL 0.00   15.50 2.06   15.50     34  34 234 T 120 VE ZL 0.00   15.50 2.06
15.50
  34  34 234 T 119 VE ZL 0.00   15.50 2.06   15.50     36  36 236 T 120 VE ZL 0.00   15.50 2.06
15.50
  37  37 237 T 121 VE ZL 0.00   15.50 2.06   15.50     38  38 238 T 122 VE ZL 0.00   15.50 2.06
15.50
  38  38 238 T 121 VE ZL 0.00   15.50 2.06   15.50     39  39 239 T 123 VE ZL 0.00   15.50 2.06
15.50
  39  39 239 T 122 VE ZL 0.00   15.50 2.06   15.50     40  40 240 T 124 VE ZL 0.00   15.50 2.06
15.50
  40  40 240 T 123 VE ZL 0.00   15.50 2.06   15.50     41  41 241 T 125 VE ZL 0.00   15.50 2.06
15.50
  41  41 241 T 124 VE ZL 0.00   15.50 2.06   15.50     42 -19 242 T 125 VE ZL 0.00   15.50 2.06
15.50
1012 125 127 T 114 VE YL 0.00  -12.50 2.20  -12.50   3007 -72 -73 S 334 VE YL 0.00    4.38 0.75
4.38
3007 -72 -73 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -73 -74 S 334 VE YL 0.00    4.38 0.75
4.38
3007 -73 -74 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -74 -75 S 334 VE YL 0.00    4.38 0.75
4.38
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3007 -74 -75 S 334 VE ZL 0.00 13.75 0.75 13.75 3007 -75 -76 S 334 VE YL 0.00 4.38 0.75
4.38
3007 -75 -76 S 334 VE ZL 0.00 13.75 0.75 13.75 3007 -81 -82 S 330 VE YL 0.00 4.38 0.70
4.38
3007 -81 -82 S 330 VE ZL 0.00 13.75 0.70 13.75 3007 -82 -83 S 330 VE YL 0.00 4.38 0.70
4.38
3007 -82 -83 S 330 VE ZL 0.00 13.75 0.70 13.75 3007 -83 -84 S 330 VE YL 0.00 4.38 0.70
4.38
3007 -83 -84 S 330 VE ZL 0.00 13.75 0.70 13.75 3007 -84 -85 S 330 VE YL 0.00 4.38 1.40
4.38
3007 -84 -85 S 330 VE ZL 0.00 13.75 1.40 13.75 3008 -68 -69 S 334 VE YL 0.00 0.00 0.75
0.00
3008 -68 -69 S 334 VE ZL 0.00 14.43 0.75 14.43 3008 -68 -69 S 335 VE YL 0.00 0.00 3.00
0.00
3008 -68 -69 S 335 VE ZL 0.00 14.43 3.00 14.43 3008 -68 -69 S 334 VE YL 2.25 0.00 3.00
0.00
3008 -68 -69 S 334 VE ZL 2.25 14.43 3.00 14.43 3008 -68 -69 S 334 VE YL 1.50 0.00 2.25
0.00
3008 -68 -69 S 334 VE ZL 1.50 14.43 2.25 14.43 3008 -68 -69 S 334 VE YL 0.75 0.00 1.50
0.00
3008 -68 -69 S 334 VE ZL 0.75 14.43 1.50 14.43 3010 -51 -52 S 335 VE YL 0.00 0.00 3.00
0.00
3010 -51 -52 S 335 VE ZL 0.00 14.43 3.00 14.43 3010 -53 -54 S 331 VE YL 0.00 0.00 3.50
0.00
3010 -53 -54 S 331 VE ZL 0.00 14.43 3.50 14.43 3013 -38 -55 S 301 VE ZL 0.00 18.75 0.58
18.75
3013 -55 -72 S 319 VE ZL 0.00 18.75 0.58 18.75 3014 -39 -56 S 300 VE ZL 0.00 18.75 0.58
18.75
3014 -39 -56 S 301 VE ZL 0.00 18.75 0.58 18.75 3014 -56 -73 S 318 VE ZL 0.00 18.75 0.58
18.75
3014 -56 -73 S 319 VE ZL 0.00 18.75 0.58 18.75 3015 -24 -27 S 316 VE ZL 0.00 18.75 0.58
18.75
3015 -27 -40 S 333 VE ZL 0.00 18.75 0.58 18.75 3015 -40 -57 S 300 VE ZL 0.00 18.75 0.58
18.75
3015 -57 -74 S 318 VE ZL 0.00 18.75 0.58 18.75 3015 -57 -74 S 321 VE ZL 0.00 18.75 0.58
18.75
3016 204 -28 S 315 VE ZL 0.00 18.75 0.58 18.75 3016 204 -28 S 316 VE ZL 0.00 18.75 0.58
18.75
3016 -28 -41 S 332 VE ZL 0.00 18.75 0.58 18.75 3016 -28 -41 S 333 VE ZL 0.00 18.75 0.58
18.75
3017 205 -29 S 312 VE ZL 0.00 17.50 0.58 17.50 3017 205 -29 S 315 VE ZL 0.00 18.75 0.58
18.75
3017 -29 -42 S 313 VE ZL 0.00 17.50 0.58 17.50 3017 -29 -42 S 332 VE ZL 0.00 18.75 0.58
18.75
3017 -59 -76 S 320 VE ZL 0.00 18.75 0.58 18.75 3017 -59 -76 S 322 VE ZL 0.00 17.50 0.58
17.50
3018 206 -30 S 311 VE ZL 0.00 17.50 0.58 17.50 3018 206 -30 S 312 VE ZL 0.00 17.50 0.58
17.50
3018 -30 -43 S 310 VE ZL 0.00 17.50 0.58 17.50 3018 -30 -43 S 313 VE ZL 0.00 17.50 0.58
17.50
3019 207 -31 S 308 VE ZL 0.00 17.50 0.58 17.50 3019 207 -31 S 311 VE ZL 0.00 17.50 0.58
17.50
3019 -31 -44 S 309 VE ZL 0.00 17.50 0.58 17.50 3019 -31 -44 S 310 VE ZL 0.00 17.50 0.58
17.50
3020 208 -32 S 307 VE ZL 0.00 17.50 0.58 17.50 3020 208 -32 S 308 VE ZL 0.00 17.50 0.58
17.50
3020 -32 -45 S 306 VE ZL 0.00 17.50 0.58 17.50 3020 -32 -45 S 309 VE ZL 0.00 17.50 0.58
17.50
3021 209 -33 S 304 VE ZL 0.00 17.50 0.58 17.50 3021 209 -33 S 307 VE ZL 0.00 17.50 0.58
17.50
3021 -33 -46 S 305 VE ZL 0.00 17.50 0.58 17.50 3021 -33 -46 S 306 VE ZL 0.00 17.50 0.58
17.50
3022 210 -34 S 302 VE ZL 0.00 17.50 0.58 17.50 3022 210 -34 S 304 VE ZL 0.00 17.50 0.58
17.50
3022 -34 -47 S 303 VE ZL 0.00 17.50 0.58 17.50 3022 -34 -47 S 305 VE ZL 0.00 17.50 0.58
17.50
3022 -64 -81 S 325 VE ZL 0.00 17.50 0.58 17.50 3022 -64 -81 S 327 VE ZL 0.00 17.50 0.58
17.50
3023 211 -35 S 302 VE ZL 0.00 17.50 0.58 17.50 3023 211 -35 S 317 VE ZL 0.00 17.50 0.58
17.50
3023 -35 -48 S 303 VE ZL 0.00 17.50 0.58 17.50 3024 -25 -36 S 314 VE ZL 0.00 17.50 0.58
17.50
3024 -25 -36 S 317 VE ZL 0.00 17.50 0.58 17.50 3025 -26 -37 S 314 VE ZL 0.00 17.50 0.58
17.50
3025 -67 -84 S 328 VE ZL 0.00 17.50 0.58 17.50 3039 -70 -71 S 330 VE YL 0.00 0.00 0.70
0.00
3039 -70 -71 S 330 VE ZL 0.00 14.43 0.70 14.43 3039 -70 -71 S 331 VE YL 0.00 0.00 3.50
0.00
3039 -70 -71 S 331 VE ZL 0.00 14.43 3.50 14.43 3039 -70 -71 S 330 VE YL 2.10 0.00 3.50
0.00
3039 -70 -71 S 330 VE ZL 2.10 14.43 3.50 14.43 3039 -70 -71 S 330 VE YL 1.40 0.00 2.10

```
0.00
3039 -70 -71 S 330 VE ZL 1.40   14.43 2.10   14.43   3039 -70 -71 S 330 VE YL 0.70    0.00 1.40
0.00
3039 -70 -71 S 330 VE ZL 0.70   14.43 1.40   14.43   3047 -58 -75 S 320 VE ZL 0.00   18.75 0.58
18.75
3047 -58 -75 S 321 VE ZL 0.00   18.75 0.58   18.75   3049 -60 -77 S 322 VE ZL 0.00   17.50 0.58
17.50
3049 -60 -77 S 323 VE ZL 0.00   17.50 0.58   17.50   3050 -61 -78 S 323 VE ZL 0.00   17.50 0.58
17.50
3050 -61 -78 S 324 VE ZL 0.00   17.50 0.58   17.50   3051 -62 -79 S 324 VE ZL 0.00   17.50 0.58
17.50
3051 -62 -79 S 326 VE ZL 0.00   17.50 0.58   17.50   3052 -63 -80 S 325 VE ZL 0.00   17.50 0.58
17.50
3052 -63 -80 S 326 VE ZL 0.00   17.50 0.58   17.50   3054 -65 -82 S 327 VE ZL 0.00   17.50 0.58
17.50
3054 -65 -82 S 329 VE ZL 0.00   17.50 0.58   17.50   3055 -66 -83 S 328 VE ZL 0.00   17.50 0.58
17.50
3055 -66 -83 S 329 VE ZL 0.00   17.50 0.58   17.50   5012  27 -14 T 214 VE ZL 0.20  -12.50 2.20  -
12.50
5012  27 -14 T 114 VE ZL 0.00  -12.50 2.20  -12.50   5012  27 -14 T 214 VE ZL 0.00  -12.50 0.20  -
12.50
5043  26 -16 T 214 VE ZL 0.00  -12.50 2.00  -12.50   5043 -17  26 T 214 VE ZL 0.00  -12.50 0.20  -
12.50


CONDIZIONE DI CARICO 12: Vento X-_2

CARICHI DISTRIBUITI

Asta  N1  N2 E  NE  T DC  Xi     Qi     Xf     Qf     Asta  N1  N2 E  NE  T DC  Xi     Qi     Xf     Qf
                          <m> <daN/m>  <m> <daN/m>                          <m> <daN/m>  <m>
<daN/m>
-------------------------------------------------  -------------------------------------------------
--
   0 143  45 T 126 VE YL 0.00  -12.38 2.30  -12.38      0 143  45 T 126 VE ZL 0.00   -5.13 2.30   -
5.13
   0 143  45 T 128 VE YL 0.00   -5.12 2.30   -5.12      0 143  45 T 128 VE ZL 0.00  -13.62 2.30  -
13.62
   0 145  46 T 129 VE YL 0.00    3.36 2.30    3.36      0 145  46 T 129 VE ZL 0.00  -12.91 2.30  -
12.91
   0 145  46 T 127 VE YL 0.00  -14.14 2.30  -14.14      0 145  46 T 127 VE ZL 0.00    5.84 2.30
5.84
   0  18  48 T 233 VE YL 0.00    0.00 0.56   -5.67      0  48  21 T 233 VE YL 0.00   -2.44 0.54   -
7.18
   0  49  21 T 134 VE YL 0.00    2.44 0.54    7.18      0  23  49 T 134 VE YL 0.00    0.00 0.56
5.67
  15 115 215 T 232 VE YL 0.00  -18.12 3.76  -18.12     16 116 216 T 232 VE ZL 0.00  -18.12 3.76  -
18.12
  16 116 216 T 133 VE ZL 0.00  -18.12 2.30  -18.12     16 116 216 T 133 VE ZL 2.30  -18.12 3.76  -
18.12
  18 118  18 T 133 VE ZL 0.00  -18.12 2.30  -18.12     18 118  18 T 126 VE YL 0.00  -12.38 2.30  -
12.38
  18 118  18 T 126 VE ZL 0.00   -5.13 2.30   -5.13     18  18 218 T 133 VE ZL 0.00  -18.12 1.46  -
18.12
  18  18 218 T 233 VE ZL 0.00    0.00 0.49   -6.38     18  18 218 T 233 VE ZL 0.49   -6.38 0.70  -
18.75
  18  18 218 T 233 VE ZL 0.70  -18.75 1.46  -18.75     19 119  19 T 128 VE YL 0.00   -5.12 2.30   -
5.12
  19 119  19 T 128 VE ZL 0.00  -13.62 2.30  -13.62     19 119  19 T 129 VE YL 0.00    3.36 2.30
3.36
  19 119  19 T 129 VE ZL 0.00  -12.91 2.30  -12.91     21  21 221 T 233 VE ZL 0.00  -18.75 0.76  -
18.75
  21  21 221 T 134 VE ZL 0.00  -18.75 0.76  -18.75     23 123  23 T 135 VE ZL 0.00  -18.12 2.30  -
18.12
  23 123  23 T 127 VE YL 0.00  -14.14 2.30  -14.14     23 123  23 T 127 VE ZL 0.00    5.84 2.30
5.84
  23  23 223 T 135 VE ZL 0.00  -18.12 1.46  -18.12     23  23 223 T 134 VE ZL 0.00    0.00 0.49   -
6.38
  23  23 223 T 134 VE ZL 0.49   -6.38 0.70  -18.75     23  23 223 T 134 VE ZL 0.70  -18.75 1.46  -
18.75
  24 124 224 T 136 VE ZL 1.70  -18.12 3.76  -18.12     24 124 224 T 135 VE ZL 0.00  -18.12 2.30  -
18.12
  24 124 224 T 135 VE ZL 2.30  -18.12 3.76  -18.12     24 124 224 T 136 VE ZL 0.00  -18.12 1.70  -
18.12
  42 142 -19 T 136 VE YL 0.00  -18.12 1.70  -18.12     42 -19 242 T 136 VE YL 0.00  -18.12 2.06  -
18.12
1013 101  -1 T 130 VE YL 0.00  -25.00 0.72  -25.00   1013  -1 117 T 130 VE YL 0.00  -25.00 0.72  -
25.00
1013 122 -11 T 132 VE YL 0.00  -25.00 0.72  -25.00   1013 -11 125 T 132 VE YL 0.00  -25.00 0.72  -
25.00
2013 201 220 T 330 VE YL 0.00    0.00 1.10   -8.75   2013 201 220 T 230 VE YL 1.45  -36.50 2.20  -
36.50
2013 201 220 T 230 VE YL 0.00  -69.00 1.45  -69.00   2013 201 220 T 330 VE YL 1.65  -13.12 2.20  -
```

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17.50
2013 201 220 T 330 VE YL 1.10   -8.75 1.65  -13.12   2013 220 225 T 131 VE YL 0.00  -36.50 0.75  -
36.50
2013 220 225 T 330 VE YL 1.10   -8.75 2.20    0.00   2013 220 225 T 330 VE YL 0.55  -13.12 1.10   -
8.75
2013 220 225 T 330 VE YL 0.00  -17.50 0.55  -13.12   2013 220 225 T 131 VE YL 0.75  -69.00 2.20  -
69.00
2026 215 216 T 333 VE YL 0.00    0.00 0.72   -5.77   2026 216 218 T 333 VE YL 0.00   -5.77 0.38   -
8.75
2026 216 218 T 333 VE YL 0.38   -8.75 0.72  -11.53   2026 218 221 T 333 VE YL 0.00  -11.53 0.75  -
17.50
2026 221 223 T 333 VE YL 0.00  -17.50 0.55  -13.12   2026 221 223 T 333 VE YL 0.55  -13.12 0.75  -
11.53
2026 223 224 T 333 VE YL 0.00  -11.53 0.35   -8.75   2026 223 224 T 333 VE YL 0.35   -8.75 0.72   -
5.77
2026 224 242 T 333 VE YL 0.00   -5.77 0.72    0.00   3007 -72 -73 S 334 VE YL 0.00    4.38 0.75
4.38
3007 -72 -73 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -73 -74 S 334 VE YL 0.00    4.38 0.75
4.38
3007 -73 -74 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -74 -75 S 334 VE YL 0.00    4.38 0.75
4.38
3007 -74 -75 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -75 -76 S 334 VE YL 0.00    4.38 0.75
4.38
3007 -75 -76 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -81 -82 S 330 VE YL 0.00    4.38 0.70
4.38
3007 -81 -82 S 330 VE ZL 0.00   13.75 0.70   13.75   3007 -82 -83 S 330 VE YL 0.00    4.38 0.70
4.38
3007 -82 -83 S 330 VE ZL 0.00   13.75 0.70   13.75   3007 -83 -84 S 330 VE YL 0.00    4.38 0.70
4.38
3007 -83 -84 S 330 VE ZL 0.00   13.75 0.70   13.75   3007 -84 -85 S 330 VE YL 0.00    4.38 1.40
4.38
3007 -84 -85 S 330 VE ZL 0.00   13.75 1.40   13.75   3008 -68 -69 S 334 VE YL 0.00    0.00 0.75
0.00
3008 -68 -69 S 334 VE ZL 0.00   14.43 0.75   14.43   3008 -68 -69 S 335 VE YL 0.00    0.00 3.00
0.00
3008 -68 -69 S 335 VE ZL 0.00   14.43 3.00   14.43   3008 -68 -69 S 334 VE YL 2.25    0.00 3.00
0.00
3008 -68 -69 S 334 VE ZL 2.25   14.43 3.00   14.43   3008 -68 -69 S 334 VE YL 1.50    0.00 2.25
0.00
3008 -68 -69 S 334 VE ZL 1.50   14.43 2.25   14.43   3008 -68 -69 S 334 VE YL 0.75    0.00 1.50
0.00
3008 -68 -69 S 334 VE ZL 0.75   14.43 1.50   14.43   3010 -51 -52 S 335 VE YL 0.00    0.00 3.00
0.00
3010 -51 -52 S 335 VE ZL 0.00   14.43 3.00   14.43   3010 -53 -54 S 331 VE YL 0.00    0.00 3.50
0.00
3010 -53 -54 S 331 VE ZL 0.00   14.43 3.50   14.43   3013 201 -38 T 330 VE YL 0.00    0.00 1.15   -
8.34
3013 -38 -55 S 301 VE ZL 0.00   18.75 0.58   18.75   3013 -38 -55 T 330 VE YL 0.00   -8.34 0.58  -
12.51
3013 -55 -72 S 319 VE ZL 0.00   18.75 0.58   18.75   3013 -55 -72 T 330 VE YL 0.00  -12.51 0.58  -
16.68
3014 -39 -56 S 300 VE ZL 0.00   18.75 0.58   18.75   3014 -39 -56 S 301 VE ZL 0.00   18.75 0.58
18.75
3014 -56 -73 S 318 VE ZL 0.00   18.75 0.58   18.75   3014 -56 -73 S 319 VE ZL 0.00   18.75 0.58
18.75
3015 -24 -27 S 316 VE ZL 0.00   18.75 0.58   18.75   3015 -27 -40 S 333 VE ZL 0.00   18.75 0.58
18.75
3015 -40 -57 S 300 VE ZL 0.00   18.75 0.58   18.75   3015 -57 -74 S 318 VE ZL 0.00   18.75 0.58
18.75
3015 -57 -74 S 321 VE ZL 0.00   18.75 0.58   18.75   3016 204 -28 S 315 VE ZL 0.00   18.75 0.58
18.75
3016 204 -28 S 316 VE ZL 0.00   18.75 0.58   18.75   3016 -28 -41 S 332 VE ZL 0.00   18.75 0.58
18.75
3016 -28 -41 S 333 VE ZL 0.00   18.75 0.58   18.75   3017 205 -29 S 312 VE ZL 0.00   17.50 0.58
17.50
3017 205 -29 S 315 VE ZL 0.00   18.75 0.58   18.75   3017 -29 -42 S 313 VE ZL 0.00   17.50 0.58
17.50
3017 -29 -42 S 332 VE ZL 0.00   18.75 0.58   18.75   3017 -59 -76 S 320 VE ZL 0.00   18.75 0.58
18.75
3017 -59 -76 S 322 VE ZL 0.00   17.50 0.58   17.50   3018 206 -30 S 311 VE ZL 0.00   17.50 0.58
17.50
3018 206 -30 S 312 VE ZL 0.00   17.50 0.58   17.50   3018 -30 -43 S 310 VE ZL 0.00   17.50 0.58
17.50
3018 -30 -43 S 313 VE ZL 0.00   17.50 0.58   17.50   3019 207 -31 S 308 VE ZL 0.00   17.50 0.58
17.50
3019 207 -31 S 311 VE ZL 0.00   17.50 0.58   17.50   3019 -31 -44 S 309 VE ZL 0.00   17.50 0.58
17.50
3019 -31 -44 S 310 VE ZL 0.00   17.50 0.58   17.50   3020 208 -32 S 307 VE ZL 0.00   17.50 0.58
17.50
3020 208 -32 S 308 VE ZL 0.00   17.50 0.58   17.50   3020 -32 -45 S 306 VE ZL 0.00   17.50 0.58
17.50
```

3020 -32 -45 S 309 VE ZL 0.00 17.50 0.58 17.50 3021 209 -33 S 304 VE ZL 0.00 17.50 0.58 17.50
3021 209 -33 S 307 VE ZL 0.00 17.50 0.58 17.50 3021 -33 -46 S 305 VE ZL 0.00 17.50 0.58 17.50
3021 -33 -46 S 306 VE ZL 0.00 17.50 0.58 17.50 3022 210 -34 S 302 VE ZL 0.00 17.50 0.58 17.50
3022 210 -34 S 304 VE ZL 0.00 17.50 0.58 17.50 3022 -34 -47 S 303 VE ZL 0.00 17.50 0.58 17.50
3022 -34 -47 S 305 VE ZL 0.00 17.50 0.58 17.50 3022 -64 -81 S 325 VE ZL 0.00 17.50 0.58 17.50
3022 -64 -81 S 327 VE ZL 0.00 17.50 0.58 17.50 3023 211 -35 S 302 VE ZL 0.00 17.50 0.58 17.50
3023 211 -35 S 317 VE ZL 0.00 17.50 0.58 17.50 3023 -35 -48 S 303 VE ZL 0.00 17.50 0.58 17.50
3024 -25 -36 S 314 VE ZL 0.00 17.50 0.58 17.50 3024 -25 -36 S 317 VE ZL 0.00 17.50 0.58 17.50
3025 -26 -37 S 314 VE ZL 0.00 17.50 0.58 17.50 3025 -67 -84 S 328 VE ZL 0.00 17.50 0.58 17.50
3026 215 -50 T 333 VE YL 0.00 0.00 0.76 -5.50 3026 215 -50 T 333 VE YL 0.76 -5.50 1.15 -8.34
3026 -50 -85 T 333 VE YL 0.00 -8.34 0.37 -10.99 3026 -50 -85 T 333 VE YL 0.37 -10.99 1.15 -16.68
3039 -70 -71 S 330 VE YL 0.00 0.00 0.70 0.00 3039 -70 -71 S 330 VE ZL 0.00 14.43 0.70 14.43
3039 -70 -71 S 331 VE YL 0.00 0.00 3.50 0.00 3039 -70 -71 S 331 VE ZL 0.00 14.43 3.50 14.43
3039 -70 -71 S 330 VE YL 2.10 0.00 3.50 0.00 3039 -70 -71 S 330 VE ZL 2.10 14.43 3.50 14.43
3039 -70 -71 S 330 VE YL 1.40 0.00 2.10 0.00 3039 -70 -71 S 330 VE ZL 1.40 14.43 2.10 14.43
3039 -70 -71 S 330 VE YL 0.70 0.00 1.40 0.00 3039 -70 -71 S 330 VE ZL 0.70 14.43 1.40 14.43
3044 -72 -68 T 330 VE YL 0.00 -16.68 0.58 -12.51 3044 -68 -51 T 330 VE YL 0.00 -12.51 0.58 -8.34
3044 -51 225 T 330 VE YL 0.00 -8.34 1.15 0.00 3047 -58 -75 S 320 VE ZL 0.00 18.75 0.58 18.75
3047 -58 -75 S 321 VE ZL 0.00 18.75 0.58 18.75 3049 -60 -77 S 322 VE ZL 0.00 17.50 0.58 17.50
3049 -60 -77 S 323 VE ZL 0.00 17.50 0.58 17.50 3050 -61 -78 S 323 VE ZL 0.00 17.50 0.58 17.50
3050 -61 -78 S 324 VE ZL 0.00 17.50 0.58 17.50 3051 -62 -79 S 324 VE ZL 0.00 17.50 0.58 17.50
3051 -62 -79 S 326 VE ZL 0.00 17.50 0.58 17.50 3052 -63 -80 S 325 VE ZL 0.00 17.50 0.58 17.50
3052 -63 -80 S 326 VE ZL 0.00 17.50 0.58 17.50 3054 -65 -82 S 327 VE ZL 0.00 17.50 0.58 17.50
3054 -65 -82 S 329 VE ZL 0.00 17.50 0.58 17.50 3055 -66 -83 S 328 VE ZL 0.00 17.50 0.58 17.50
3055 -66 -83 S 329 VE ZL 0.00 17.50 0.58 17.50 3057 -85 -71 T 333 VE YL 0.00 -16.68 0.58 -12.51
3057 -71 -54 T 333 VE YL 0.00 -12.51 0.21 -10.99 3057 -71 -54 T 333 VE YL 0.21 -10.99 0.58 -8.34
3057 -54 242 T 333 VE YL 0.00 -8.34 0.39 -5.50 3057 -54 242 T 333 VE YL 0.39 -5.50 1.15 0.00
5013 -15 17 T 230 VE ZL 0.00 69.00 1.45 69.00 5013 -15 17 T 130 VE ZL 0.72 25.00 1.45 25.00
5013 -15 17 T 130 VE ZL 0.00 25.00 0.72 25.00 5044 44 20 T 230 VE ZL 0.00 36.50 0.75 36.50
5044 20 47 T 131 VE ZL 0.00 36.50 0.75 36.50 5075 22 -16 T 131 VE ZL 0.00 69.00 1.45 69.00
5075 22 -16 T 132 VE ZL 0.72 25.00 1.45 25.00 5075 22 -16 T 132 VE ZL 0.00 25.00 0.72 25.00

CONDIZIONE DI CARICO 13: Vento Y-_2

CARICHI DISTRIBUITI

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
1	101	-15	T	101	VE	ZL	0.00	-23.75	1.00	-23.75	1	-15	201	T	101	VE	ZL	0.00	-23.75	2.76	-23.75
2	102	202	T	102	VE	ZL	2.86	-22.50	3.76	-22.50	2	102	202	T	101	VE	ZL	0.00	-23.75	1.00	-23.75
2	102	202	T	101	VE	ZL	1.00	-23.75	3.76	-23.75	2	102	202	T	102	VE	ZL	0.00	-22.50	2.16	-22.50
2	102	202	T	102	VE	ZL	2.16	-22.50	2.86	-22.50	3	103	3	T	103	VE	ZL	0.00	-10.00	2.16	-10.00
3	103	3	T	102	VE	ZL	0.00	-22.50	2.16	-22.50	3	3	-20	T	102	VE	ZL	0.00	-22.50	0.70	-22.50

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   3 -20 203 T 203 VE ZL 0.00  -10.00 0.90  -10.00      3 -20 203 T 102 VE ZL 0.00  -22.50 0.90  -
22.50
   4 104   4 T 104 VE ZL 1.60  -18.75 2.16  -18.75      4 104   4 T 103 VE ZL 0.00  -10.00 2.16  -
10.00
   4 104   4 T 104 VE ZL 0.00  -18.75 1.60  -18.75      4   4 -21 T 104 VE ZL 0.00  -18.75 0.70  -
18.75
   4 -21 204 T 104 VE ZL 0.00  -18.75 0.90  -18.75      4 -21 204 T 203 VE ZL 0.00  -10.00 0.90  -
10.00
   5 105  43 T 104 VE ZL 0.00  -18.75 1.60  -18.75      5  43 205 T 204 VE ZL 0.00  -17.50 2.16  -
17.50
   5  43 205 T 104 VE ZL 0.00  -18.75 0.56  -18.75      5  43 205 T 104 VE ZL 0.56  -18.75 1.26  -
18.75
   5  43 205 T 104 VE ZL 1.26  -18.75 2.16  -18.75      6 106   6 T 105 VE ZL 0.00  -17.50 1.60  -
17.50
   6   6 206 T 105 VE ZL 0.00  -17.50 2.16  -17.50      6   6 206 T 204 VE ZL 0.00  -17.50 2.16  -
17.50
   7 107 207 T 106 VE ZL 0.00  -17.50 3.76  -17.50      7 107 207 T 105 VE ZL 0.00  -17.50 1.60  -
17.50
   7 107 207 T 105 VE ZL 1.60  -17.50 3.76  -17.50      8 108 208 T 107 VE ZL 0.00  -17.50 3.76  -
17.50
   8 108 208 T 106 VE ZL 0.00  -17.50 3.76  -17.50      9 109 209 T 107 VE ZL 0.00  -17.50 3.76  -
17.50
   9 109 209 T 108 VE ZL 0.00  -17.50 3.76  -17.50     10 110 210 T 109 VE ZL 2.86  -17.50 3.76  -
17.50
  10 110 210 T 108 VE ZL 0.00  -17.50 3.76  -17.50     10 110 210 T 109 VE ZL 0.00  -17.50 2.16  -
17.50
  10 110 210 T 109 VE ZL 2.16  -17.50 2.86  -17.50     11 111  11 T 110 VE ZL 0.00  -10.00 2.16  -
10.00
  11 111  11 T 109 VE ZL 0.00  -17.50 2.16  -17.50     11  11 -22 T 109 VE ZL 0.00  -17.50 0.70  -
17.50
  11 -22 211 T 109 VE ZL 0.00  -17.50 0.90  -17.50     11 -22 211 T 210 VE ZL 0.00  -10.00 0.90  -
10.00
  12 112  12 T 110 VE ZL 0.00  -10.00 2.16  -10.00     12 112  12 T 111 VE ZL 0.00  -20.00 2.16  -
20.00
  12  12 -23 T 111 VE ZL 0.00  -20.00 0.70  -20.00     12 -23 212 T 111 VE ZL 0.00  -20.00 0.90  -
20.00
  12 -23 212 T 210 VE ZL 0.00  -10.00 0.90  -10.00     13 113 213 T 111 VE ZL 2.86  -20.00 3.76  -
20.00
  13 113 213 T 112 VE ZL 0.00  -20.00 3.76  -20.00     13 113 213 T 111 VE ZL 0.00  -20.00 2.16  -
20.00
  13 113 213 T 111 VE ZL 2.16  -20.00 2.86  -20.00     14 114 214 T 113 VE ZL 0.00  -20.00 3.76  -
20.00
  14 114 214 T 112 VE ZL 0.00  -20.00 3.76  -20.00     15 115 215 T 113 VE ZL 0.00  -20.00 3.76  -
20.00
  26  26 226 T 314 VE ZL 0.00  -15.00 2.76  -15.00     27 127  27 T 115 VE ZL 0.00  -10.00 0.50  -
10.00
  27  27 -17 T 115 VE ZL 0.00  -10.00 0.50  -10.00     28 128  28 T 115 VE ZL 0.50  -10.00 1.00  -
10.00
  28 128  28 T 115 VE ZL 0.00  -10.00 0.50  -10.00     28  28 228 T 314 VE ZL 0.00  -15.00 2.76  -
15.00
  29 129 -18 T 215 VE ZL 0.00  -10.00 1.70  -10.00     29 -18 229 T 315 VE ZL 0.00  -10.00 2.06  -
10.00
  30 130  30 T 215 VE ZL 0.00  -10.00 1.70  -10.00     30  30 230 T 116 VE ZL 0.00  -15.50 2.06  -
15.50
  30  30 230 T 315 VE ZL 0.00  -10.00 2.06  -10.00     31  31 231 T 117 VE ZL 0.00  -15.50 2.06  -
15.50
  31  31 231 T 116 VE ZL 0.00  -15.50 2.06  -15.50     32  32 232 T 118 VE ZL 0.00  -15.50 2.06  -
15.50
  32  32 232 T 117 VE ZL 0.00  -15.50 2.06  -15.50     33  33 233 T 119 VE ZL 0.00  -15.50 2.06  -
15.50
  33  33 233 T 118 VE ZL 0.00  -15.50 2.06  -15.50     34  34 234 T 120 VE ZL 0.00  -15.50 2.06  -
15.50
  34  34 234 T 119 VE ZL 0.00  -15.50 2.06  -15.50     36  36 236 T 120 VE ZL 0.00  -15.50 2.06  -
15.50
  37  37 237 T 121 VE ZL 0.00  -15.50 2.06  -15.50     38  38 238 T 122 VE ZL 0.00  -15.50 2.06  -
15.50
  38  38 238 T 121 VE ZL 0.00  -15.50 2.06  -15.50     39  39 239 T 123 VE ZL 0.00  -15.50 2.06  -
15.50
  39  39 239 T 122 VE ZL 0.00  -15.50 2.06  -15.50     40  40 240 T 124 VE ZL 0.00  -15.50 2.06  -
15.50
  40  40 240 T 123 VE ZL 0.00  -15.50 2.06  -15.50     41  41 241 T 125 VE ZL 0.00  -15.50 2.06  -
15.50
  41  41 241 T 124 VE ZL 0.00  -15.50 2.06  -15.50     42 -19 242 T 125 VE ZL 0.00  -15.50 2.06  -
15.50
1012 125 127 T 114 VE YL 0.00   12.50 2.20   12.50   3007 -72 -73 S 334 VE YL 0.00    4.38 0.75
4.38
3007 -72 -73 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -73 -74 S 334 VE YL 0.00    4.38 0.75
4.38
3007 -73 -74 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -74 -75 S 334 VE YL 0.00    4.38 0.75
4.38
3007 -74 -75 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -75 -76 S 334 VE YL 0.00    4.38 0.75
```

```
4.38
3007 -75 -76 S 334 VE ZL 0.00   13.75 0.75   13.75   3007 -81 -82 S 330 VE YL 0.00    4.38 0.70
4.38
3007 -81 -82 S 330 VE ZL 0.00   13.75 0.70   13.75   3007 -82 -83 S 330 VE YL 0.00    4.38 0.70
4.38
3007 -82 -83 S 330 VE ZL 0.00   13.75 0.70   13.75   3007 -83 -84 S 330 VE YL 0.00    4.38 0.70
4.38
3007 -83 -84 S 330 VE ZL 0.00   13.75 0.70   13.75   3007 -84 -85 S 330 VE YL 0.00    4.38 1.40
4.38
3007 -84 -85 S 330 VE ZL 0.00   13.75 1.40   13.75   3008 -68 -69 S 334 VE YL 0.00    0.00 0.75
0.00
3008 -68 -69 S 334 VE ZL 0.00   14.43 0.75   14.43   3008 -68 -69 S 335 VE YL 0.00    0.00 3.00
0.00
3008 -68 -69 S 335 VE ZL 0.00   14.43 3.00   14.43   3008 -68 -69 S 334 VE YL 2.25    0.00 3.00
0.00
3008 -68 -69 S 334 VE ZL 2.25   14.43 3.00   14.43   3008 -68 -69 S 334 VE YL 1.50    0.00 2.25
0.00
3008 -68 -69 S 334 VE ZL 1.50   14.43 2.25   14.43   3008 -68 -69 S 334 VE YL 0.75    0.00 1.50
0.00
3008 -68 -69 S 334 VE ZL 0.75   14.43 1.50   14.43   3010 -51 -52 S 335 VE YL 0.00    0.00 3.00
0.00
3010 -51 -52 S 335 VE ZL 0.00   14.43 3.00   14.43   3010 -53 -54 S 331 VE YL 0.00    0.00 3.50
0.00
3010 -53 -54 S 331 VE ZL 0.00   14.43 3.50   14.43   3013 -38 -55 S 301 VE ZL 0.00   18.75 0.58
18.75
3013 -55 -72 S 319 VE ZL 0.00   18.75 0.58   18.75   3014 -39 -56 S 300 VE ZL 0.00   18.75 0.58
18.75
3014 -39 -56 S 301 VE ZL 0.00   18.75 0.58   18.75   3014 -56 -73 S 318 VE ZL 0.00   18.75 0.58
18.75
3014 -56 -73 S 319 VE ZL 0.00   18.75 0.58   18.75   3015 -24 -27 S 316 VE ZL 0.00   18.75 0.58
18.75
3015 -27 -40 S 333 VE ZL 0.00   18.75 0.58   18.75   3015 -40 -57 S 300 VE ZL 0.00   18.75 0.58
18.75
3015 -57 -74 S 318 VE ZL 0.00   18.75 0.58   18.75   3015 -57 -74 S 321 VE ZL 0.00   18.75 0.58
18.75
3016 204 -28 S 315 VE ZL 0.00   18.75 0.58   18.75   3016 204 -28 S 316 VE ZL 0.00   18.75 0.58
18.75
3016 -28 -41 S 332 VE ZL 0.00   18.75 0.58   18.75   3016 -28 -41 S 333 VE ZL 0.00   18.75 0.58
18.75
3017 205 -29 S 312 VE ZL 0.00   17.50 0.58   17.50   3017 205 -29 S 315 VE ZL 0.00   18.75 0.58
18.75
3017 -29 -42 S 313 VE ZL 0.00   17.50 0.58   17.50   3017 -29 -42 S 332 VE ZL 0.00   18.75 0.58
18.75
3017 -59 -76 S 320 VE ZL 0.00   18.75 0.58   18.75   3017 -59 -76 S 322 VE ZL 0.00   17.50 0.58
17.50
3018 206 -30 S 311 VE ZL 0.00   17.50 0.58   17.50   3018 206 -30 S 312 VE ZL 0.00   17.50 0.58
17.50
3018 -30 -43 S 310 VE ZL 0.00   17.50 0.58   17.50   3018 -30 -43 S 313 VE ZL 0.00   17.50 0.58
17.50
3019 207 -31 S 308 VE ZL 0.00   17.50 0.58   17.50   3019 207 -31 S 311 VE ZL 0.00   17.50 0.58
17.50
3019 -31 -44 S 309 VE ZL 0.00   17.50 0.58   17.50   3019 -31 -44 S 310 VE ZL 0.00   17.50 0.58
17.50
3020 208 -32 S 307 VE ZL 0.00   17.50 0.58   17.50   3020 208 -32 S 308 VE ZL 0.00   17.50 0.58
17.50
3020 -32 -45 S 306 VE ZL 0.00   17.50 0.58   17.50   3020 -32 -45 S 309 VE ZL 0.00   17.50 0.58
17.50
3021 209 -33 S 304 VE ZL 0.00   17.50 0.58   17.50   3021 209 -33 S 307 VE ZL 0.00   17.50 0.58
17.50
3021 -33 -46 S 305 VE ZL 0.00   17.50 0.58   17.50   3021 -33 -46 S 306 VE ZL 0.00   17.50 0.58
17.50
3022 210 -34 S 302 VE ZL 0.00   17.50 0.58   17.50   3022 210 -34 S 304 VE ZL 0.00   17.50 0.58
17.50
3022 -34 -47 S 303 VE ZL 0.00   17.50 0.58   17.50   3022 -34 -47 S 305 VE ZL 0.00   17.50 0.58
17.50
3022 -64 -81 S 325 VE ZL 0.00   17.50 0.58   17.50   3022 -64 -81 S 327 VE ZL 0.00   17.50 0.58
17.50
3023 211 -35 S 302 VE ZL 0.00   17.50 0.58   17.50   3023 211 -35 S 317 VE ZL 0.00   17.50 0.58
17.50
3023 -35 -48 S 303 VE ZL 0.00   17.50 0.58   17.50   3024 -25 -36 S 314 VE ZL 0.00   17.50 0.58
17.50
3024 -25 -36 S 317 VE ZL 0.00   17.50 0.58   17.50   3025 -26 -37 S 314 VE ZL 0.00   17.50 0.58
17.50
3025 -67 -84 S 328 VE ZL 0.00   17.50 0.58   17.50   3039 -70 -71 S 330 VE YL 0.00    0.00 0.70
0.00
3039 -70 -71 S 330 VE ZL 0.00   14.43 0.70   14.43   3039 -70 -71 S 331 VE YL 0.00    0.00 3.50
0.00
3039 -70 -71 S 331 VE ZL 0.00   14.43 3.50   14.43   3039 -70 -71 S 330 VE YL 2.10    0.00 3.50
0.00
3039 -70 -71 S 330 VE ZL 2.10   14.43 3.50   14.43   3039 -70 -71 S 330 VE YL 1.40    0.00 2.10
0.00
3039 -70 -71 S 330 VE ZL 1.40   14.43 2.10   14.43   3039 -70 -71 S 330 VE YL 0.70    0.00 1.40
0.00
```

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3039 -70 -71 S 330 VE ZL 0.70   14.43 1.40   14.43   3047 -58 -75 S 320 VE ZL 0.00   18.75 0.58
18.75
3047 -58 -75 S 321 VE ZL 0.00   18.75 0.58   18.75   3049 -60 -77 S 322 VE ZL 0.00   17.50 0.58
17.50
3049 -60 -77 S 323 VE ZL 0.00   17.50 0.58   17.50   3050 -61 -78 S 323 VE ZL 0.00   17.50 0.58
17.50
3050 -61 -78 S 324 VE ZL 0.00   17.50 0.58   17.50   3051 -62 -79 S 324 VE ZL 0.00   17.50 0.58
17.50
3051 -62 -79 S 326 VE ZL 0.00   17.50 0.58   17.50   3052 -63 -80 S 325 VE ZL 0.00   17.50 0.58
17.50
3052 -63 -80 S 326 VE ZL 0.00   17.50 0.58   17.50   3054 -65 -82 S 327 VE ZL 0.00   17.50 0.58
17.50
3054 -65 -82 S 329 VE ZL 0.00   17.50 0.58   17.50   3055 -66 -83 S 328 VE ZL 0.00   17.50 0.58
17.50
3055 -66 -83 S 329 VE ZL 0.00   17.50 0.58   17.50   5012  27 -14 T 214 VE ZL 0.20   12.50 2.20
12.50
5012  27 -14 T 114 VE ZL 0.00   12.50 2.20   12.50   5012  27 -14 T 214 VE ZL 0.00   12.50 0.20
12.50
5043  26 -16 T 214 VE ZL 0.00   12.50 2.00   12.50   5043 -17  26 T 214 VE ZL 0.00   12.50 0.20
12.50


CONDIZIONE DI CARICO 14: Azione termica +

CARICHI TERMICI


Simbologia

Asta = Numero dell'asta
DT   = Incremento di temperatura
Gy   = Gradiente termico in dir. Y
Gz   = Gradiente termico in dir. Z
N1   = Nodo iniziale
N2   = Nodo finale

Asta  N1  N2   DT    Gy     Gz     Asta  N1  N2   DT    Gy     Gz     Asta  N1  N2   DT    Gy     Gz
              <°C> <°C/m> <°C/m>                <°C> <°C/m> <°C/m>                <°C> <°C/m>
<°C/m>
--------------------------------   --------------------------------   --------------------------------
-
   0 143  45 25.00                    0 145  46 25.00                    0  18  48 25.00
   0  48  21 25.00                    0  49  21 25.00                    0  23  49 25.00
   1   1 101 25.00                    1 101 -15 25.00                    1 -15 201 25.00
   2 102 202 25.00                    3 103   3 25.00                    3   3 -20 25.00
   3 -20 203 25.00                    4 104   4 25.00                    4   4 -21 25.00
   4 -21 204 25.00                    5   5 105 25.00                    5 105  43 25.00
   5  43 205 25.00                    6 106   6 25.00                    6   6 206 25.00
   7 107 207 25.00                    8 108 208 25.00                    9 109 209 25.00
  10  10 110 25.00                   10 110 210 25.00                   11 111  11 25.00
  11  11 -22 25.00                   11 -22 211 25.00                   12 112  12 25.00
  12  12 -23 25.00                   12 -23 212 25.00                   13 113 213 25.00
  14 114 214 25.00                   15  15 115 25.00                   15 115 215 25.00
  16 116 216 25.00                   17 117  17 25.00                   17  17  44 25.00
  18 118  18 25.00                   18  18 218 25.00                   19 119  19 25.00
  20  20 220 25.00                   21  21 221 25.00                   22 122  22 25.00
  22  22  47 25.00                   23 123  23 25.00                   23  23 223 25.00
  24 124 224 25.00                   25  25 125 25.00                   25 125 -14 25.00
  25 -14 -16 25.00                   25 -16 225 25.00                   26  26 226 25.00
  27 127  27 25.00                   27  27 -17 25.00                   28 128  28 25.00
  28  28 228 25.00                   29  29 129 25.00                   29 129 -18 25.00
  29 -18 229 25.00                   30 130  30 25.00                   30  30 230 25.00
  31  31 231 25.00                   32  32 232 25.00                   33  33 233 25.00
  34  34 234 25.00                   35  35 135 25.00                   36  36 236 25.00
  37  37 237 25.00                   38  38 238 25.00                   39  39 239 25.00
  40  40 240 25.00                   41  41 241 25.00                   42  42 142 25.00
  42 142 -19 25.00                   42 -19 242 25.00                 1001 101 102 25.00
1001 102 103 25.00                 1001 103 104 25.00                 1001 104 105 25.00
1001 105 106 25.00                 1001 106 107 25.00                 1001 107 108 25.00
1001 108 109 25.00                 1001 109 110 25.00                 1001 110 111 25.00
1001 111 112 25.00                 1001 112 113 25.00                 1001 113 114 25.00
1001 114 115 25.00                 1003  -1  -2 25.00                 1003  -2  -3 25.00
1003  -3 116 25.00                 1005 117  -4 25.00                 1005  -4  -5 25.00
1005  -5 118 25.00                 1007  -6  -7 25.00                 1007  -7  -8 25.00
1007  -8 144 25.00                 1009 122  -9 25.00                 1009  -9 -10 25.00
1009 -10 123 25.00                 1011 -11 -12 25.00                 1011 -12 -13 25.00
1011 -13 124 25.00                 1012 125 127 25.00                 1012 127 128 25.00
1012 128 129 25.00                 1012 129 130 25.00                 1012 130 135 25.00
1012 135 142 25.00                 1013 101  -1 25.00                 1013  -1 117 25.00
1013 117  -6 25.00                 1013  -6 122 25.00                 1013 122 -11 25.00
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1013 -11 125 25.00
1017  -4  -7 25.00
1017 -12 129 25.00
1022  -5  -8 25.00
1022 -13 135 25.00
1026 118 144 25.00
1026 124 142 25.00
1030 119 145 25.00
2001 202 -24 25.00
2001 204 205 25.00
2001 207 208 25.00
2001 210 211 25.00
2001 -25 213 25.00
2001 214 215 25.00
2012 228 229 25.00
2012 231 232 25.00
2012 234 236 25.00
2012 238 239 25.00
2012 241 242 25.00
2017 205 229 25.00
2026 216 218 25.00
2026 223 224 25.00
3002 -28 -29 25.00
3002 -31 -32 25.00
3002 -34 -35 25.00
3004 -38 -39 25.00
3004 -41 -42 25.00
3004 -44 -45 25.00
3004 -47 -48 25.00
3006 -55 -56 25.00
3006 -58 -59 25.00
3006 -61 -62 25.00
3006 -64 -65 25.00
3007 -72 -73 25.00
3007 -75 -76 25.00
3007 -78 -79 25.00
3007 -81 -82 25.00
3007 -84 -85 25.00
3010 -52 -53 25.00
3013 -38 -55 25.00
3014 -56 -73 25.00
3015 -40 -57 25.00
3016 -28 -41 25.00
3017 -42 -59 25.00
3018 -30 -43 25.00
3020 208 -32 25.00
3021 -33 -46 25.00
3022 -47 -64 25.00
3023 -35 -48 25.00
3025 -37 -49 25.00
3026 215 -50 25.00
3044 -72 -68 25.00
3047 -58 -75 25.00
3048 -52 229 25.00
3051 -62 -79 25.00
3053 -70 -53 25.00
3055 -66 -83 25.00
3057 -54 242 25.00
5013 -15  17 25.00
5029  19  21 25.00
5032   3   4 25.00
5043  28 -17 25.00
5063  43   6 25.00
5074  32  31 25.00
5074  36  34 25.00
5074  39  38 25.00
5074 -19  41 25.00
5125 -22 -23 25.00
1017 105  -2 25.00
1017  -7  -9 25.00
1022 110  -3 25.00
1022  -8 -10 25.00
1026 115 116 25.00
1026 144 123 25.00
1027 118 143 25.00
1031 145 123 25.00
2001 -24 203 25.00
2001 205 206 25.00
2001 208 209 25.00
2001 211 212 25.00
2001 213 -26 25.00
2012 225 226 25.00
2012 229 230 25.00
2012 232 233 25.00
2012 236 237 25.00
2012 239 240 25.00
2013 201 220 25.00
2022 210 236 25.00
2026 218 221 25.00
2026 224 242 25.00
3002 -29 -30 25.00
3002 -32 -33 25.00
3002 -35 -36 25.00
3004 -39 -40 25.00
3004 -42 -43 25.00
3004 -45 -46 25.00
3004 -48 -49 25.00
3006 -56 -57 25.00
3006 -59 -60 25.00
3006 -62 -63 25.00
3006 -65 -66 25.00
3007 -73 -74 25.00
3007 -76 -77 25.00
3007 -79 -80 25.00
3007 -82 -83 25.00
3008 -68 -69 25.00
3010 -53 -54 25.00
3013 -55 -72 25.00
3015 -24 -27 25.00
3015 -57 -74 25.00
3017 205 -29 25.00
3017 -59 -76 25.00
3019 207 -31 25.00
3020 -32 -45 25.00
3022 210 -34 25.00
3022 -64 -81 25.00
3024 -25 -36 25.00
3025 -49 -67 25.00
3026 -50 -85 25.00
3044 -68 -51 25.00
3048 -76 -69 25.00
3049 -60 -77 25.00
3052 -63 -80 25.00
3053 -53 236 25.00
3057 -85 -71 25.00
5001 -20 -21 25.00
5027  18  45 25.00
5030  19  46 25.00
5043  26 -16 25.00
5044  44  20 25.00
5074  30 -18 25.00
5074  33  32 25.00
5074  37  36 25.00
5074  40  39 25.00
5075  22 -16 25.00
1017  -2  -4 25.00
1017  -9 -12 25.00
1022  -3  -5 25.00
1022 -10 -13 25.00
1026 116 118 25.00
1026 123 124 25.00
1028 143 119 25.00
2001 201 202 25.00
2001 203 204 25.00
2001 206 207 25.00
2001 209 210 25.00
2001 212 -25 25.00
2001 -26 214 25.00
2012 226 228 25.00
2012 230 231 25.00
2012 233 234 25.00
2012 237 238 25.00
2012 240 241 25.00
2013 220 225 25.00
2026 215 216 25.00
2026 221 223 25.00
3002 -27 -28 25.00
3002 -30 -31 25.00
3002 -33 -34 25.00
3002 -36 -37 25.00
3004 -40 -41 25.00
3004 -43 -44 25.00
3004 -46 -47 25.00
3004 -49 -50 25.00
3006 -57 -58 25.00
3006 -60 -61 25.00
3006 -63 -64 25.00
3006 -66 -67 25.00
3007 -74 -75 25.00
3007 -77 -78 25.00
3007 -80 -81 25.00
3007 -83 -84 25.00
3010 -51 -52 25.00
3013 201 -38 25.00
3014 -39 -56 25.00
3015 -27 -40 25.00
3016 204 -28 25.00
3017 -29 -42 25.00
3018 206 -30 25.00
3019 -31 -44 25.00
3021 209 -33 25.00
3022 -34 -47 25.00
3023 211 -35 25.00
3025 -26 -37 25.00
3025 -67 -84 25.00
3039 -70 -71 25.00
3044 -51 225 25.00
3048 -69 -52 25.00
3050 -61 -78 25.00
3053 -81 -70 25.00
3054 -65 -82 25.00
3057 -71 -54 25.00
5012  27 -14 25.00
5028  45  19 25.00
5031  46  23 25.00
5043 -17  26 25.00
5044  20  47 25.00
5074  31  30 25.00
5074  34  33 25.00
5074  38  37 25.00
5074  41  40 25.00
5094  11  12 25.00
```

CONDIZIONE DI CARICO 15: Azione termica -

CARICHI TERMICI

Asta	N1	N2	DT <°C>	Gy <°C/m>	Gz <°C/m>	Asta	N1	N2	DT <°C>	Gy <°C/m>	Gz <°C/m>	Asta	N1	N2	DT <°C>	Gy <°C/m>	Gz <°C/m>
0	143	45	-25.00			0	145	46	-25.00			0	18	48	-25.00		
0	48	21	-25.00			0	49	21	-25.00			0	23	49	-25.00		
1	1	101	-25.00			1	101	-15	-25.00			1	-15	201	-25.00		

```
   2 102 202 -25.00
   3 -20 203 -25.00
   4 -21 204 -25.00
   5  43 205 -25.00
   7 107 207 -25.00
  10  10 110 -25.00
  11  11 -22 -25.00
  12  12 -23 -25.00
  14 114 214 -25.00
  16 116 216 -25.00
  18 118  18 -25.00
  20  20 220 -25.00
  22  22  47 -25.00
  24 124 224 -25.00
  25 -14 -16 -25.00
  27 127  27 -25.00
  28  28 228 -25.00
  29 -18 229 -25.00
  31  31 231 -25.00
  34  34 234 -25.00
  37  37 237 -25.00
  40  40 240 -25.00
  42 142 -19 -25.00
1001 102 103 -25.00
1001 105 106 -25.00
1001 108 109 -25.00
1001 111 112 -25.00
1001 114 115 -25.00
1003  -3 116 -25.00
1005  -5 118 -25.00
1007  -8 144 -25.00
1009 -10 123 -25.00
1011 -13 124 -25.00
1012 128 129 -25.00
1012 135 142 -25.00
1013 117  -6 -25.00
1013 -11 125 -25.00
1017  -4  -7 -25.00
1017 -12 129 -25.00
1022  -5  -8 -25.00
1022 -13 135 -25.00
1026 118 144 -25.00
1026 124 142 -25.00
1030 119 145 -25.00
2001 202 -24 -25.00
2001 204 205 -25.00
2001 207 208 -25.00
2001 210 211 -25.00
2001 -25 213 -25.00
2001 214 215 -25.00
2012 228 229 -25.00
2012 231 232 -25.00
2012 234 236 -25.00
2012 238 239 -25.00
2012 241 242 -25.00
2017 205 229 -25.00
2026 216 218 -25.00
2026 223 224 -25.00
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3007 -75 -76 -25.00
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3007 -81 -82 -25.00
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3013 -38 -55 -25.00
3014 -56 -73 -25.00
3015 -40 -57 -25.00
3016 -28 -41 -25.00
3017 -42 -59 -25.00
3018 -30 -43 -25.00
   3 103   3 -25.00
   4 104   4 -25.00
   5   5 105 -25.00
   6 106   6 -25.00
   8 108 208 -25.00
  10 110 210 -25.00
  11 -22 211 -25.00
  12 -23 212 -25.00
  15  15 115 -25.00
  17 117  17 -25.00
  18  18 218 -25.00
  21  21 221 -25.00
  23 123  23 -25.00
  25  25 125 -25.00
  25 -16 225 -25.00
  27  27 -17 -25.00
  29  29 129 -25.00
  30 130  30 -25.00
  32  32 232 -25.00
  35  35 135 -25.00
  38  38 238 -25.00
  41  41 241 -25.00
  42 -19 242 -25.00
1001 103 104 -25.00
1001 106 107 -25.00
1001 109 110 -25.00
1001 112 113 -25.00
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1005 117  -4 -25.00
1007  -6  -7 -25.00
1009 122  -9 -25.00
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1012 125 127 -25.00
1012 129 130 -25.00
1013 101  -1 -25.00
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1017  -7  -9 -25.00
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1026 144 123 -25.00
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2001 205 206 -25.00
2001 208 209 -25.00
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2001 213 -26 -25.00
2012 225 226 -25.00
2012 229 230 -25.00
2012 232 233 -25.00
2012 236 237 -25.00
2012 239 240 -25.00
2013 201 220 -25.00
2022 210 236 -25.00
2026 218 221 -25.00
2026 224 242 -25.00
3002 -29 -30 -25.00
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3002 -35 -36 -25.00
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3008 -68 -69 -25.00
3010 -53 -54 -25.00
3013 -55 -72 -25.00
3015 -24 -27 -25.00
3015 -57 -74 -25.00
3017 205 -29 -25.00
3017 -59 -76 -25.00
3019 207 -31 -25.00
   3   3 -20 -25.00
   4   4 -21 -25.00
   5 105  43 -25.00
   6   6 206 -25.00
   9 109 209 -25.00
  11 111  11 -25.00
  12 112  12 -25.00
  13 113 213 -25.00
  15 115 215 -25.00
  17  17  44 -25.00
  19 119  19 -25.00
  22 122  22 -25.00
  23  23 223 -25.00
  25 125 -14 -25.00
  26  26 226 -25.00
  28 128  28 -25.00
  29 129 -18 -25.00
  30  30 230 -25.00
  33  33 233 -25.00
  36  36 236 -25.00
  39  39 239 -25.00
  42  42 142 -25.00
1001 101 102 -25.00
1001 104 105 -25.00
1001 107 108 -25.00
1001 110 111 -25.00
1001 113 114 -25.00
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1005  -4  -5 -25.00
1007  -7  -8 -25.00
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1013  -1 117 -25.00
1013 122 -11 -25.00
1017  -2  -4 -25.00
1017  -9 -12 -25.00
1022  -3  -5 -25.00
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1026 123 124 -25.00
1028 143 119 -25.00
2001 201 202 -25.00
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2001 206 207 -25.00
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2012 226 228 -25.00
2012 230 231 -25.00
2012 233 234 -25.00
2012 237 238 -25.00
2012 240 241 -25.00
2013 220 225 -25.00
2026 215 216 -25.00
2026 221 223 -25.00
3002 -27 -28 -25.00
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3007 -83 -84 -25.00
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3013 201 -38 -25.00
3014 -39 -56 -25.00
3015 -27 -40 -25.00
3016 204 -28 -25.00
3017 -29 -42 -25.00
3018 206 -30 -25.00
3019 -31 -44 -25.00
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3023 -35 -48 -25.00
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3026 215 -50 -25.00
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3047 -58 -75 -25.00
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3051 -62 -79 -25.00
3053 -70 -53 -25.00
3055 -66 -83 -25.00
3057 -54 242 -25.00
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5029 19 21 -25.00
5032 3 4 -25.00
5043 28 -17 -25.00
5063 43 6 -25.00
5074 32 31 -25.00
5074 36 34 -25.00
5074 39 38 -25.00
5074 -19 41 -25.00
5125 -22 -23 -25.00

3020 -32 -45 -25.00
3022 210 -34 -25.00
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3024 -25 -36 -25.00
3025 -49 -67 -25.00
3026 -50 -85 -25.00
3044 -68 -51 -25.00
3048 -76 -69 -25.00
3049 -60 -77 -25.00
3052 -63 -80 -25.00
3053 -53 236 -25.00
3057 -85 -71 -25.00
5001 -20 -21 -25.00
5027 18 45 -25.00
5030 19 46 -25.00
5043 26 -16 -25.00
5044 44 20 -25.00
5074 30 -18 -25.00
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5074 37 36 -25.00
5074 40 39 -25.00
5075 22 -16 -25.00

3021 209 -33 -25.00
3022 -34 -47 -25.00
3023 211 -35 -25.00
3025 -26 -37 -25.00
3025 -67 -84 -25.00
3039 -70 -71 -25.00
3044 -51 225 -25.00
3048 -69 -52 -25.00
3050 -61 -78 -25.00
3053 -81 -70 -25.00
3054 -65 -82 -25.00
3057 -71 -54 -25.00
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5044 20 47 -25.00
5074 31 30 -25.00
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5074 38 37 -25.00
5074 41 40 -25.00
5094 11 12 -25.00

Analisi dei carichi da vento

Vento X_pareti

Calcolo delle azioni del vento
Normativa di riferimento: Norme tecniche per le costruzioni D.M. 17 gennaio 2018 e Circolare 21 gennaio 2019, n. 7 del Ministero delle Infrastrutture e dei Trasporti

Zona di ubicazione dell'edificio: 3 - Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria (esclusa la Provincia di Reggio Calabria)

Classe di rugosità del terreno: D - a) Mare e relativa fascia costiera, b) Lago e relativa fascia costiera, c) Area priva di ostacoli o con al più rari ostacoli isolati (tab. 3.3.III)

Categoria di esposizione del sito: II

Parametri derivati (tab. 3.3.I):
$V_{b,0}$ (velocità base di riferimento al livello del mare): 27.00<m/sec>
a_0: 500.00<m>
K_s: 0.37

Parametri derivati (tab. 3.3.II):
K_r: 0.19
z_0: 0.05<m>
z_{min}: 4.00<m>

Classificazione della costruzione: Edifici a pianta rettangolare con coperture piane, a falde, inclinate e curvilinee - Pareti verticali(C3.3.8.1.1)

a_s (altitudine sul livello del mare): 180.00<m>
T_r (tempo di ritorno): 50 anni
V_b (velocità base di riferimento [3.3.1]): 27.00<m/sec>
c_a (coefficiente di altitudine [3.3.1.b]): 1.00
V_r (velocità di riferimento [3.3.2]): 27.00<m/sec>
c_r (coefficiente di ritorno [3.3.3]): 1.00
c_t (coefficiente topografico): 1.00
q_r (pressione cinetica di riferimento): 45.56<daN/mq>
c_e (coefficiente di esposizione): 1.98
c_d (coefficiente dinamico): 1.00
h (altezza dell'edificio): 5.46<m>
b (dimensione in pianta ortogonale al flusso): 4.40<m>
d (profondità dell'edificio): 10.00<m>

Coefficienti di pressione C_{pe}:
sopravento: 0.75
laterale: -0.90
sottovento: -0.41

Pressioni esterne:
sopravento fino a quota 4.40<m>: 63.78<daN/mq>
sopravento oltre la quota 4.40<m>: 68.11<daN/mq>
laterale: -81.24<daN/mq>
sottovento: -36.94<daN/mq>

Criteri di valutazione del C_{pi} (C3.3.8.5) riferiti a edifici aventi:Area con distribuzione uniforme di aperture

Coefficiente di pressione C_{pi}:
positivo: 0.20
negativo: -0.30

Pressioni interna:
positiva: 18.05<daN/mq>
negativa: -27.08<daN/mq>

Pressioni massimizzate (esterne+interne):
sopravento fino a quota 4.40<m>: 90.86<daN/mq>
sopravento oltre la quota 4.40<m>: 95.19<daN/mq>
laterale: -99.29<daN/mq>
sottovento: -54.99<daN/mq>

Vento Y_pareti

Calcolo delle azioni del vento
Normativa di riferimento: Norme tecniche per le costruzioni D.M. 17 gennaio 2018 e Circolare 21 gennaio 2019, n. 7 del Ministero delle Infrastrutture e dei Trasporti

Zona di ubicazione dell'edificio: 3 - Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria (esclusa la Provincia di Reggio Calabria)

Classe di rugosità del terreno: D - a) Mare e relativa fascia costiera, b) Lago e relativa fascia costiera, c) Area priva di ostacoli o con al più rari ostacoli isolati (tab. 3.3.III)

Categoria di esposizione del sito: II

Parametri derivati (tab. 3.3.I):
$V_{b,0}$ (velocità base di riferimento al livello del mare): 27.00<m/sec>
a_0: 500.00<m>
K_s: 0.37

Parametri derivati (tab. 3.3.II):
K_r: 0.19
z_0: 0.05<m>
z_{min}: 4.00<m>

Classificazione della costruzione: Edifici a pianta rettangolare con coperture piane, a falde, inclinate e curvilinee - Pareti verticali(C3.3.8.1.1)

a_s (altitudine sul livello del mare): 180.00<m>
T_r (tempo di ritorno): 50 anni
V_b (velocità base di riferimento [3.3.1]): 27.00<m/sec>
c_a (coefficiente di altitudine [3.3.1.b]): 1.00
V_r (velocità di riferimento [3.3.2]): 27.00<m/sec>
c_r (coefficiente di ritorno [3.3.3]): 1.00
c_t (coefficiente topografico): 1.00
q_r (pressione cinetica di riferimento): 45.56<daN/mq>
c_e (coefficiente di esposizione): 1.98
c_d (coefficiente dinamico): 1.00
h (altezza dell'edificio): 5.46<m>
b (dimensione in pianta ortogonale al flusso): 10.00<m>
d (profondità dell'edificio): 4.40<m>

Coefficienti di pressione C_{pe}:
sopravento: 0.80
laterale: -0.90
sottovento: -0.51

Pressioni esterne:
sopravento: 72.21<daN/mq>
laterale: -81.24<daN/mq>
sottovento: -46.22<daN/mq>

Criteri di valutazione del C_{pi} (C3.3.8.5) riferiti a edifici aventi:Area con distribuzione uniforme di aperture

Coefficiente di pressione C_{pi}:
positivo: 0.20
negativo: -0.30

Pressioni interna:
positiva: 18.05<daN/mq>
negativa: -27.08<daN/mq>

Pressioni massimizzate (esterne+interne):
sopravento: 99.29<daN/mq>
laterale: -99.29<daN/mq>
sottovento: -64.27<daN/mq>

Vento X_copertura

Calcolo delle azioni del vento
Normativa di riferimento: Norme tecniche per le costruzioni D.M. 17 gennaio 2018 e Circolare 21 gennaio 2019, n. 7 del Ministero delle Infrastrutture e dei Trasporti

Zona di ubicazione dell'edificio: 3 - Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria (esclusa la Provincia di Reggio Calabria)

Classe di rugosità del terreno: D - a) Mare e relativa fascia costiera, b) Lago e relativa fascia costiera, c) Area priva di ostacoli o con al più rari ostacoli isolati (tab. 3.3.III)

Categoria di esposizione del sito: II

Parametri derivati (tab. 3.3.I):
$V_{b,0}$ (velocità base di riferimento al livello del mare): 27.00<m/sec>
a_0: 500.00<m>
K_s: 0.37

Parametri derivati (tab. 3.3.II):
K_r: 0.19
z_0: 0.05<m>
z_{min}: 4.00<m>

Classificazione della costruzione: Edifici a pianta rettangolare con coperture piane, a falde, inclinate e curvilinee - Coperture piane(C3.3.8.1.2)

a_s (altitudine sul livello del mare): 180.00<m>
T_r (tempo di ritorno): 50 anni
V_b (velocità base di riferimento [3.3.1]): 27.00<m/sec>
c_a (coefficiente di altitudine [3.3.1.b]): 1.00
V_r (velocità di riferimento [3.3.2]): 27.00<m/sec>
c_r (coefficiente di ritorno [3.3.3]): 1.00
c_t (coefficiente topografico): 1.00
q_r (pressione cinetica di riferimento): 45.56<daN/mq>
c_e (coefficiente di esposizione): 1.98
c_d (coefficiente dinamico): 1.00
h (altezza dell'edificio): 5.46<m>
b (dimensione in pianta ortogonale al flusso): 4.40<m>

Si considera una fascia sopravento di 2.20<m> e sottovento le zone restanti.

Coefficienti di pressione C_{pe}:
sopravento $C_{pe,A}$: -0.80
positivo sottovento $C_{pe,B}$: 0.20
negativo sottovento $C_{pe,B}$: -0.20

Pressioni esterne:
sopravento $C_{pe,A}$: -72.21<daN/mq>
positivo sottovento $C_{pe,B}$: 18.05<daN/mq>
negativo sottovento $C_{pe,B}$: -18.05<daN/mq>

Criteri di valutazione del C_{pi} (C3.3.8.5) riferiti a edifici aventi:Area con distribuzione uniforme di aperture

Coefficiente di pressione C_{pi}:
positivo: 0.20
negativo: -0.30

Pressioni interna:
positiva: 18.05<daN/mq>
negativa: -27.08<daN/mq>

Pressioni massimizzate (esterne+interne):
sopravento: -90.26<daN/mq>
positivo sottovento: 45.13<daN/mq>
negativo sottovento: -36.11<daN/mq>

Vento Y_copertura

Calcolo delle azioni del vento
Normativa di riferimento: Norme tecniche per le costruzioni D.M. 17 gennaio 2018 e Circolare 21 gennaio 2019, n. 7 del Ministero delle Infrastrutture e dei Trasporti

Zona di ubicazione dell'edificio: 3 - Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria (esclusa la Provincia di Reggio Calabria)

Classe di rugosità del terreno: D - a) Mare e relativa fascia costiera, b) Lago e relativa fascia costiera, c) Area priva di ostacoli o con al più rari ostacoli isolati (tab. 3.3.III)

Categoria di esposizione del sito: II

Parametri derivati (tab. 3.3.I):
$V_{b,0}$ (velocità base di riferimento al livello del mare): 27.00<m/sec>
a_0: 500.00<m>
K_s: 0.37

Parametri derivati (tab. 3.3.II):
K_r: 0.19
z_0: 0.05<m>
z_{min}: 4.00<m>

Classificazione della costruzione: Edifici a pianta rettangolare con coperture piane, a falde, inclinate e curvilinee - Coperture a falda doppia(C3.3.8.1.4)

a_s (altitudine sul livello del mare): 180.00<m>
T_r (tempo di ritorno): 50 anni
V_b (velocità base di riferimento [3.3.1]): 27.00<m/sec>
c_a (coefficiente di altitudine [3.3.1.b]): 1.00
V_r (velocità di riferimento [3.3.2]): 27.00<m/sec>
c_r (coefficiente di ritorno [3.3.3]): 1.00
c_t (coefficiente topografico): 1.00
q_r (pressione cinetica di riferimento): 45.56<daN/mq>
c_e (coefficiente di esposizione): 1.98
c_d (coefficiente dinamico): 1.00
h (altezza dell'edificio): 5.46<m>
b (dimensione in pianta del lato parallelo alla direzione del colmo): 10.00<m>
α (angolo inclinazione): 17.65<grad>

Per il vento parallelo si considera una fascia sopravento di 5.00<m> e sottovento le zone restanti.

Coefficienti di pressione C_{pe}:
vento perpendicolare al colmo sopravento positivo: 0.24
vento perpendicolare al colmo sopravento negativo: -0.56
vento perpendicolare al colmo sottovento: -0.57
vento parallelo al colmo sopravento $C_{pe,A}$: -0.92
vento parallelo al colmo sottovento $C_{pe,B}$: -0.50

Pressioni esterne:
vento perpendicolare al colmo sopravento positivo: 21.24<daN/mq>
vento perpendicolare al colmo sopravento negativo: -50.97<daN/mq>
vento perpendicolare al colmo sottovento: -51.77<daN/mq>
vento parallelo al colmo sopravento $C_{pe,A}$: -82.83<daN/mq>
vento parallelo al colmo sottovento $C_{pe,B}$: -45.13<daN/mq>

Criteri di valutazione del C_{pi} (C3.3.8.5) riferiti a edifici aventi:Area con distribuzione uniforme di aperture

Coefficiente di pressione C_{pi}:
positivo: 0.20
negativo: -0.30

Pressioni interna:
positiva: 18.05<daN/mq>
negativa: -27.08<daN/mq>

Pressioni massimizzate (esterne+interne):
vento perpendicolare al colmo sopravento positivo: 48.32<daN/mq>
vento perpendicolare al colmo sopravento negativo: -69.02<daN/mq>
vento perpendicolare al colmo sottovento: -69.82<daN/mq>
vento parallelo al colmo sopravento: -100.89<daN/mq>
vento parallelo al colmo sottovento: -63.18<daN/mq>

Vento X_tettoia

Calcolo delle azioni del vento
Normativa di riferimento: Norme tecniche per le costruzioni D.M. 17 gennaio 2018 e Circolare 21 gennaio 2019, n. 7 del Ministero delle Infrastrutture e dei Trasporti

Zona di ubicazione dell'edificio: 3 - Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria (esclusa la Provincia di Reggio Calabria)

Classe di rugosità del terreno: C - Area con ostacoli diffusi (quali alberi, case, muri, recinzioni, ...); aree con rugosità non riconducibile alle Classi A, B, D (tab. 3.3.III)

Categoria di esposizione del sito: III

Parametri derivati (tab. 3.3.I):
$V_{b,0}$ (velocità base di riferimento al livello del mare): 27.00<m/sec>
a_0: 500.00<m>
K_s: 0.37

Parametri derivati (tab. 3.3.II):
K_r: 0.20
z_0: 0.10<m>
z_{min}: 5.00<m>

Classificazione della costruzione: Tettoie - Tettoie a falda singola(C3.3.8.2.1)

a_s (altitudine sul livello del mare): 180.00<m>
T_r (tempo di ritorno): 50 anni
V_b (velocità base di riferimento [3.3.1]): 27.00<m/sec>
c_a (coefficiente di altitudine [3.3.1.b]): 1.00
V_r (velocità di riferimento [3.3.2]): 27.00<m/sec>
c_r (coefficiente di ritorno [3.3.3]): 1.00
c_t (coefficiente topografico): 1.00
q_r (pressione cinetica di riferimento): 45.56<daN/mq>
c_e (coefficiente di esposizione): 1.76
c_d (coefficiente dinamico): 1.00
h (altezza dell'edificio): 5.46<m>
d (dimensione falda): 10.00<m>
b (dimensione in pianta ortogonale al flusso): 4.40<m>
α (angolo inclinazione): 0.00<grad>
ϕ (grado di bloccaggio): 0.00

Coefficienti di forza C_f:
perpendicolare al colmo positivo: 0.20
perpendicolare al colmo negativo: -0.50

Forza risultante:
perpendicolare al colmo positivo: 705.68<daN>
perpendicolare al colmo negativo: -1764.20<daN>

Coefficienti di forza C_f:
vento parallelo al colmo positivo: 0.20
vento parallelo al colmo negativo: -0.50

Forza risultante:
vento parallelo al colmo positivo: 705.68<daN>
vento parallelo al colmo negativo: -1764.20<daN>

Vento Y_tettoia

Calcolo delle azioni del vento
Normativa di riferimento: Norme tecniche per le costruzioni D.M. 17 gennaio 2018 e Circolare 21 gennaio 2019, n. 7 del Ministero delle Infrastrutture e dei Trasporti

Zona di ubicazione dell'edificio: 3 - Toscana, Marche, Umbria, Lazio, Abruzzo, Molise, Puglia, Campania, Basilicata, Calabria (esclusa la Provincia di Reggio Calabria)

Classe di rugosità del terreno: C - Area con ostacoli diffusi (quali alberi, case, muri, recinzioni, ...); aree con rugosità non riconducibile alle Classi A, B, D (tab. 3.3.III)

Categoria di esposizione del sito: III

Parametri derivati (tab. 3.3.I):
$V_{b,0}$ (velocità base di riferimento al livello del mare): 27.00<m/sec>
a_0: 500.00<m>
K_s: 0.37

Parametri derivati (tab. 3.3.II):
K_r: 0.20
z_0: 0.10<m>
z_{min}: 5.00<m>

Classificazione della costruzione: Tettoie - Tettoie a falda doppia(C3.3.8.2.2)

a_s (altitudine sul livello del mare): 180.00<m>
T_r (tempo di ritorno): 50 anni
V_b (velocità base di riferimento [3.3.1]): 27.00<m/sec>
c_a (coefficiente di altitudine [3.3.1.b]): 1.00
V_r (velocità di riferimento [3.3.2]): 27.00<m/sec>
c_r (coefficiente di ritorno [3.3.3]): 1.00
c_t (coefficiente topografico): 1.00
q_r (pressione cinetica di riferimento): 45.56<daN/mq>
c_e (coefficiente di esposizione): 1.76
c_d (coefficiente dinamico): 1.00
h (altezza dell'edificio): 5.46<m>
d (dimensione falda): 4.40<m>
b (dimensione in pianta ortogonale al flusso): 10.00<m>
α (angolo inclinazione): 17.65<grad>
ϕ (grado di bloccaggio): 0.00

Coefficienti di forza C_f:
perpendicolare al colmo positivo: 0.61
perpendicolare al colmo negativo: -0.85

Forza risultante:
perpendicolare al colmo positivo: 2158.79<daN>
perpendicolare al colmo negativo: -3009.73<daN>

Coefficienti di forza C_f:
vento parallelo al colmo positivo: 0.20
vento parallelo al colmo negativo: -0.50

Forza risultante:
vento parallelo al colmo positivo: 705.68<daN>
vento parallelo al colmo negativo: -1764.20<daN>

Nome dell'analisi dei carichi da neve

Neve

Calcolo delle azioni della neve
Normativa di riferimento: Norme tecniche per le costruzioni D.M. 17 gennaio 2018 e Circolare 21 gennaio 2019, n. 7 del Ministero delle Infrastrutture e dei Trasporti

Zona di ubicazione dell'edificio: III
Agrigento, Brindisi, Cagliari, Caltanissetta, Carbonia - Iglesias, Caserta, Catania, Catanzaro, Cosenza, Crotone, Enna, Grosseto, Latina, Lecce, Livorno, Matera, Medio Campidano, Messina, Napoli, Nuoro, Ogliastra, Olbia - Tempio, Oristano, Palermo, Pisa, Potenza, Ragusa, Reggio Calabria, Roma, Salerno, Sassari, Siena, Siracusa, Taranto, Terni, Trapani, Vibo Valentia, Viterbo

Coefficiente di esposizione del sito: Normale

Classificazione della costruzione:Copertura a due falde

T_r (tempo di ritorno): 50 anni
C_t (coefficiente termico): 1.00
a_s (altitudine sul livello del mare): 180.00<m>

α_1 (angolo sinistro d'inclinazione della falda): 17.62<grad>
α_2 (angolo destro d'inclinazione della falda): 17.62<grad>

Parametri derivati (3.4.2):
qsk (valore di riferimento del carico neve al suolo): 60.00<daN/mq>

Parametri derivati (tab. 3.4.I):
C_E (coefficiente d'esposizione): 1.00
$\mu_1(\alpha_1)$ (coefficiente di forma della copertura): 0.80
$\mu_1(\alpha_2)$ (coefficiente di forma della copertura): 0.80

```
Carichi agenti:
     qss (carico sinistro provocato dalla neve sulle coperture nel caso I): 48.00<daN/mq>
     qsd (carico destro provocato dalla neve sulle coperture nel caso I): 48.00<daN/mq>
     qss (carico sinistro provocato dalla neve sulle coperture nel caso II): 24.00<daN/mq>
     qsd (carico destro  provocato dalla neve sulle coperture nel caso II): 48.00<daN/mq>
     qss (carico sinistro provocato dalla neve sulle coperture nel caso III): 48.00<daN/mq>
     qsd (carico destro provocato dalla neve sulle coperture nel caso III): 24.00<daN/mq>
PARAMETRI DI CALCOLO
La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati
con:
ModeSt ver. 8.37, licenza n. 7481, prodotto da Tecnisoft s.a.s. - Prato
La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
Xfinest ver. 9.7.8, licenza n. 0, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 18
Tipo di calcolo: sismica dinamica
Vincoli esterni: Considera sempre vincoli assegnati in modellazione
Schematizzazione piani rigidi: nessun impalcato rigido
Modalità di recupero masse secondarie: trasferire le masse
- All'impalcato più vicino in assoluto: Sì
- Anche sui nodi degli impalcati non rigidi: Sì
- Modificare coordinate baricentro impalcati rigidi: XY

Generazione combinazioni
- Tipo di analisi: Lineare
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo
- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi
bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore
Opzioni generali:
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Ricerca autovettori aggiuntivi nel metodo di Ritz-vectors: Sì
- Check sequenza di Sturm: Sì
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No

Opzioni per analisi P-Delta:
- Numero massimo di iterazioni: 15
- Valore della norma euclidea degli spostamenti: 1.0000E-04

Opzioni per analisi pushover:
- Esegui analisi in regime di piccoli spostamenti: Sì

Opzioni per analisi pushover murature:
- Interrompi analisi nel caso di plasticizzazione per carichi statici: Sì
- Utilizza sforzo normale medio: Sì

Metodo di convergenza:
- Forze e momenti residui (F)
  Valore della norma euclidea delle forze: 1.0000E-03
  Valore della norma euclidea dei momenti: 1.0000E-02

- Opzioni aggiuntive per analisi non lineari in presenza di elementi bidimensionali con comportamento
Drucker-Prager:
OPTION PARAM AUTO_INCREMENT=YES
OPTION PARAM LINE_SEARCHES=YES
OPTION PARAM BGINCRS=1.0
OPTION PARAM AVINCRS=1.0

Dati struttura
- Sito di costruzione: Via di Monti, 44, 56037 Peccioli PI, Italia LON. 10.81230 LAT. 43.53690
   Contenuto tra ID reticolo: 20940 21162 20941 21163

Simbologia

Ag  = Accelerazione orizzontale massima al sito
Cc  = Coefficiente funzione della categoria del suolo
Fo  = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
Ss  = Coefficiente di amplificazione stratigrafica
TR  = Periodo di ritorno <anni>
```

TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLD = Stato limite di danno
SND = Stato limite di salvaguardia della vita (non dissipativo)
Tc* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale
<sec>

TCC	T_R	Ag <g>	Fo	Tc*	S_S	C_C
SLD	35	0.0500	2.49	0.24	1.50	1.68
SLV	332	0.1247	2.48	0.27	1.50	1.61

- Edificio esistente: No
- Spettri: Automatici da normativa
- Tipo di opera: Provvisoria
- Vita nominale V_N: 10.00
- Classe d'uso: Classe I
- SL Esercizio: SLOPvr No, SLDPvr 63.00
- SL Ultimi: SLVPvr 10.00, SLCPvr No
- Struttura dissipativa: No
- Quota di riferimento: 0.00 <m>
- Quota max della struttura: 5.46 <m>
- Altezza della struttura: 5.46 <m>
- Numero piani edificio: 2
- Coefficiente θ: 0.00
- Edificio regolare in altezza: No
- Edificio regolare in pianta: No
- Forze orizzontali convenzionali per stati limite non sismici: No
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di piano

Simbologia

Ea = Eccentricità complessiva
Ex = Eccentricità in dir. X
Ey = Eccentricità in dir. Y
Imp. = Numero dell'impalcato
Lx = Dimensione del piano in dir. X
Ly = Dimensione del piano in dir. Y

Imp.	Lx <m>	Ly <m>	Ex <m>	Ey <m>	Ea <m>
1	10.57	4.40	0.53	0.22	0.57
2	10.00	4.40	0.50	0.22	0.55

- Eccentricità di calcolo: 0.57 <m>
- Considera eccentricità aggiuntiva sugli impalcati non rigidi: Sì

Dati di calcolo
- Categoria del suolo di fondazione: C
- Tipologia strutturale: c.a. o prefabbricata a telaio a più piani e più campate

Periodo T_1	0.25152
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovraresistenza (α_u/α_1)	1.15
Valore di riferimento del fattore di comportamento (q_0)	3.45
Fattore riduttivo (K_w)	1.00
Fattore riduttivo regolarità in altezza (KR)	0.80
Fattore di comportamento dissipativo (q)	1.50
Fattore di comportamento non dissipativo (qND)	1.50
Fattore di comportamento per SLD (qD)	1.50

- Categoria topografica: T2 - Pendii con inclinazione media i > 15°
- Coeff. amplificazione topografica S_T: 1.20
- Fattore di comportamento per sisma verticale (qv): 1.50
- Modalità di calcolo modi di vibrare: Autovalori
- Numero modi: 30
- Modi da considerare: Tutti i modi calcolati
- Smorzamento spettro: 5.00%

- Angolo di ingresso del sisma: 0.00 <grad>

AMBIENTI DI CARICO:

Simbologia

N. = Numero

```
Comm. = Commento
    1 = Permanenti strutturali
    2 = Permanenti non strutturali
    3 = Esercizio cat.C
    4 = Esercizio cat.H
    5 = Neve
    6 = Vento X+_1
    7 = Vento Y+_1
    8 = Vento X-_1
    9 = Vento Y-_1
   10 = Vento X+_2
   11 = Vento Y+_2
   12 = Vento X-_2
   13 = Vento Y-_2
   14 = Azione termica +
   15 = Azione termica -
F     = azioni orizzontali convenzionali
SLU   = Stato limite ultimo
SLR   = Stato limite per combinazioni rare
SLF   = Stato limite per combinazioni frequenti
SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
        S = Sì
        N = No
```

N.	Comm.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	S	S	S	S	S	N	N	N	N	N	N	N	N	S	S	S	S	N	S	S
2	Calcolo statico	S	S	S	S	S	N	N	N	N	N	N	N	N	S	S	N	S	S	S	S
3	Vento da 0°	S	S	S	S	S	S	N	S	N	S	N	S	N	S	S	N	S	S	S	S
4	Vento da 90°	S	S	S	S	S	N	S	N	S	N	S	N	S	S	S	N	S	S	S	S

ELENCO COMBINAZIONI DI CARICO SIMBOLICHE:

Simbologia

```
CC    = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC   = Tipo di combinazione di carico
        SLU = Stato limite ultimo
        SLE R = Stato limite d'esercizio, combinazione rara
        SLD = Stato limite di danno
        SND = Stato limite di salvaguardia della vita (non dissipativo)
```

CC	Comm.	TCC	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	S
1	Amb. 1 (Sisma)	SLU S	1	ψ_2	ψ_2	ψ_2	-----	-----	-----	-----	-----	-----	ψ_2	ψ_2	1			
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	γ max	γ max	-----	-----	-----	-----	-----	γ max	γ max	-----			
3	Amb. 2 (SLE R)	SLE R	1	1	1	1	1	-----	-----	-----	-----	-----	-----	1	1	-----		
4	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	ψ_1	ψ_1	-----	-----	-----	-----	-----	ψ_1	ψ_1	-----			
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	ψ_2	-----	-----	-----	-----	-----	ψ_2	ψ_2	-----			
6	Amb. 3 (SLU)	SLU	γ max	γ max	γ max	γ max	γ max	γ max	-----	γ max	-----	γ max	-----	γ max	γ max	-----		
7	Amb. 3 (SLU)	SLU	γ max	γ max	γ max	γ max	γ max	ψ_0*γ max	-----	ψ_0*γ max	-----	ψ_0*γ max	-----	ψ_0*γ max	γ max	-----		
8	Amb. 3 (SLE R)	SLE R	1	1	1	1	1	1	-----	1	-----	1	-----	1	1	-----		
9	Amb. 3 (SLE R)	SLE R	1	1	1	1	1	ψ_0	-----	ψ_0	-----	ψ_0	-----	1	1	-----		
10	Amb. 3 (SLE F)	SLE F	1	1	ψ_1	ψ_1	ψ_1	ψ_1	-----	ψ_1	-----	ψ_1	-----	ψ_1	ψ_1	-----		
11	Amb. 3 (SLE F)	SLE F	1	1	ψ_1	ψ_1	ψ_1	ψ_2	-----	ψ_2	-----	ψ_2	-----	ψ_1	ψ_1	-----		
12	Amb. 3 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	ψ_2	ψ_2	-----	ψ_2	-----	ψ_2	-----	ψ_2	ψ_2	-----		
13	Amb. 4 (SLU)	SLU	γ max	γ max	γ max	γ max	γ max	-----	γ max	-----	γ max	-----	γ max	-----	γ max	γ max	-----	
14	Amb. 4 (SLU)	SLU	γ max	γ max	γ max	γ max	γ max	-----	ψ_0*γ max	-----	ψ_0*γ max	-----	ψ_0*γ max	-----	ψ_0*γ max	γ max	-----	
15	Amb. 4 (SLE R)	SLE R	1	1	1	1	1	-----	1	-----	1	-----	1	-----	1	1	-----	

16 Amb. 4 (SLE R) SLE R 1 1 1 1 1 ----- ψ_0 ----- ψ_0 ----- ψ_0 ----- ψ_0 1 1 -----
17 Amb. 4 (SLE F) SLE F 1 1 ψ_1 ψ_1 ψ_1 ----- ψ_1 ----- ψ_1 ----- ψ_1 ----- ψ_1 ψ_1 -----
18 Amb. 4 (SLE F) SLE F 1 1 ψ_1 ψ_1 ψ_1 ----- ψ_2 ----- ψ_2 ----- ψ_2 ----- ψ_2 ψ_1 -----
19 Amb. 4 (SLE Q) SLE Q 1 1 ψ_2 ψ_2 ψ_2 ----- ψ_2 ----- ψ_2 ----- ψ_2 ----- ψ_2 ψ_2 -----

Genera le combinazioni con un solo carico di tipo variabile come di base: No

Considera sollecitazioni dinamiche con segno dei modi principali: No

COMBINAZIONI DELLE CCE:

Simbologia

An. = Tipo di analisi
L = Lineare
NL = Non lineare
PD = P-Delta
Bk = Buckling
S = Sì
N = No
CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLE R = Stato limite d'esercizio, combinazione rara
SLD = Stato limite di danno
SND = Stato limite di salvaguardia della vita (non dissipativo)

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	Mt	±S X	±S Y
1	Amb. 1 (SLU S) S Mt+X+0.3Y	SND	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	1.00	0.30
2	Amb. 1 (SLE) S Mt+X+0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	1.00	0.30
3	Amb. 1 (SLU S) S Mt+X-0.3Y	SND	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	1.00	-0.30
4	Amb. 1 (SLE) S Mt+X-0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	1.00	-0.30
5	Amb. 1 (SLU S) S Mt+0.3X+Y	SND	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30	1.00
6	Amb. 1 (SLE) S Mt+0.3X+Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.30	1.00
7	Amb. 1 (SLU S) S Mt-0.3X+Y	SND	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30	1.00
8	Amb. 1 (SLE) S Mt-0.3X+Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	-0.30	1.00
9	Amb. 1 (SLU S) S -Mt+X+0.3Y	SND	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-1.00	1.00	0.30
10	Amb. 1 (SLE) S -Mt+X+0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-1.00	1.00	0.30
11	Amb. 1 (SLU S) S -Mt+X-0.3Y	SND	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-1.00	1.00	-0.30
12	Amb. 1 (SLE) S -Mt+X-0.3Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-1.00	1.00	-0.30
13	Amb. 1 (SLU S) S -Mt+0.3X+Y	SND	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30	1.00
14	Amb. 1 (SLE) S -Mt+0.3X+Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-1.00	0.30	1.00
15	Amb. 1 (SLU S) S -Mt-0.3X+Y	SND	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30	1.00
16	Amb. 1 (SLE) S -Mt-0.3X+Y	SLD	L	N	1.00	1.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-1.00	-0.30	1.00
17	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.50	0.00	0.75	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
18	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.05	1.50	0.75	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
19	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.05	0.00	1.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
20	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.05	0.00	0.00	1.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21	Amb. 2 (SLU)	SLU	L	N	1.30	1.50	1.05	0.00	0.00	0.00	1.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

0.00 0.00 0.00 0.00 0.00 0.00 0.00
22 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.00 0.00 0.00 1.50 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00
23 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.00 0.00 0.00 0.00 1.50 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00
24 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 1.50 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00
25 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 1.50 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00
26 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 1.50 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00
27 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 1.50 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00
28 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.90 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
29 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.90 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
30 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.90 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
31 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 1.50 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
32 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.90 0.00 0.00 0.00 0.00 0.00
0.00 0.00 1.50 0.00 0.00 0.00 0.00
33 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.90 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
34 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.90 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
35 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.90 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
36 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 1.50 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
37 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.90 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 1.50 0.00 0.00 0.00
38 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.90 0.00 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
39 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.90 0.00 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
40 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.90 0.00 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
41 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 1.50 0.00 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
42 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.90 0.00 0.00 0.00 0.00
0.00 0.00 1.50 0.00 0.00 0.00 0.00
43 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.90 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
44 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.90 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
45 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.90 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
46 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 1.50 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
47 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.90 0.00 0.00 0.00 0.00
0.00 0.00 0.00 1.50 0.00 0.00 0.00
48 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.90 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
49 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.90 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
50 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.90 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
51 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 1.50 0.00 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
52 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.90 0.00 0.00 0.00
0.00 0.00 1.50 0.00 0.00 0.00 0.00
53 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.90 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
54 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.90 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
55 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.90 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
56 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 1.50 0.00 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
57 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.90 0.00 0.00 0.00
0.00 0.00 0.00 1.50 0.00 0.00 0.00
58 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.90 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
59 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.90 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
60 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.90 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
61 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 1.50 0.00 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
62 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.90 0.00 0.00
0.00 0.00 1.50 0.00 0.00 0.00 0.00

63 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.90 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
64 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.90 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
65 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.90 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
66 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 1.50 0.00 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
67 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.90 0.00 0.00
0.00 0.00 0.00 1.50 0.00 0.00 0.00
68 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.00 0.00 0.00 0.00 0.00 1.50 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00
69 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.50
0.00 0.00 0.00 0.00 0.00 0.00 0.00
70 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
1.50 0.00 0.00 0.00 0.00 0.00 0.00
71 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 1.50 0.00 0.00 0.00 0.00 0.00
72 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 1.50 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00
73 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 1.50
0.00 0.00 0.00 0.00 0.00 0.00 0.00
74 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
1.50 0.00 0.00 0.00 0.00 0.00 0.00
75 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.00 1.50 0.00 0.00 0.00 0.00 0.00
76 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.00 0.90 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
77 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.00 0.90 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
78 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.00 0.90 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
79 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 1.50 0.00
0.00 0.00 0.90 0.00 0.00 0.00 0.00
80 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.90 0.00
0.00 0.00 1.50 0.00 0.00 0.00 0.00
81 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.00 0.90 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
82 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.00 0.90 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
83 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.00 0.90 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
84 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 1.50 0.00
0.00 0.00 0.00 0.90 0.00 0.00 0.00
85 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.90 0.00
0.00 0.00 0.00 1.50 0.00 0.00 0.00
86 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.90
0.00 0.00 0.90 0.00 0.00 0.00 0.00
87 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.00 0.00 0.90
0.00 0.00 0.90 0.00 0.00 0.00 0.00
88 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.00 0.00 0.90
0.00 0.00 0.90 0.00 0.00 0.00 0.00
89 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 1.50
0.00 0.00 0.90 0.00 0.00 0.00 0.00
90 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.90
0.00 0.00 1.50 0.00 0.00 0.00 0.00
91 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.90
0.00 0.00 0.00 0.90 0.00 0.00 0.00
92 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.00 0.00 0.90
0.00 0.00 0.00 0.90 0.00 0.00 0.00
93 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.00 0.00 0.90
0.00 0.00 0.00 0.90 0.00 0.00 0.00
94 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 1.50
0.00 0.00 0.00 0.90 0.00 0.00 0.00
95 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.90
0.00 0.00 0.00 1.50 0.00 0.00 0.00
96 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.90 0.00 0.90 0.00 0.00 0.00 0.00
97 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.90 0.00 0.90 0.00 0.00 0.00 0.00
98 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.00 0.00 0.00
0.90 0.00 0.90 0.00 0.00 0.00 0.00
99 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
1.50 0.00 0.90 0.00 0.00 0.00 0.00
100 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.90 0.00 1.50 0.00 0.00 0.00 0.00
101 Amb. 2 (SLU) SLU L N 1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.90 0.00 0.00 0.90 0.00 0.00 0.00
102 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.90 0.00 0.00 0.90 0.00 0.00 0.00
103 Amb. 2 (SLU) SLU L N 1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.00 0.00 0.00

```
0.90 0.00 0.00 0.90  0.00  0.00  0.00
104 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
1.50 0.00 0.00 0.90  0.00  0.00  0.00
105 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.90 0.00 0.00 1.50  0.00  0.00  0.00
106 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.90 0.90 0.00  0.00  0.00  0.00
107 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.90 0.90 0.00  0.00  0.00  0.00
108 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.90 0.90 0.00  0.00  0.00  0.00
109 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.00 1.50 0.90 0.00  0.00  0.00  0.00
110 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.90 1.50 0.00  0.00  0.00  0.00
111 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.50 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.90 0.00 0.90  0.00  0.00  0.00
112 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 1.50 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.90 0.00 0.90  0.00  0.00  0.00
113 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 0.00 1.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.90 0.00 0.90  0.00  0.00  0.00
114 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.00 1.50 0.00 0.90  0.00  0.00  0.00
115 Amb. 2 (SLU)               SLU   L   N  1.30 1.50 1.05 0.00 0.75 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.90 0.00 1.50  0.00  0.00  0.00
116 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
117 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
118 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
119 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 1.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
120 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 1.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
121 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 1.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
122 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 1.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
123 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.00 1.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
124 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.00 0.00 1.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
125 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.00 0.00 0.00 1.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
126 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.00 0.00 0.00 0.00 1.00 0.00 0.00
0.00 0.00 0.00 0.00  0.00  0.00  0.00
127 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.60 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.60 0.00  0.00  0.00  0.00
128 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.60 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.60 0.00  0.00  0.00  0.00
129 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.60 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.60 0.00  0.00  0.00  0.00
130 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 1.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.60 0.00  0.00  0.00  0.00
131 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.60 0.00 0.00 0.00 0.00 0.00
0.00 0.00 1.00 0.00  0.00  0.00  0.00
132 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.60 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.60  0.00  0.00  0.00
133 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.60 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.60  0.00  0.00  0.00
134 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.60 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.60  0.00  0.00  0.00
135 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 1.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.60  0.00  0.00  0.00
136 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.60 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 1.00  0.00  0.00  0.00
137 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.00 0.60 0.00 0.00 0.00 0.00
0.00 0.00 0.60 0.00  0.00  0.00  0.00
138 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.00 0.60 0.00 0.00 0.00 0.00
0.00 0.00 0.60 0.00  0.00  0.00  0.00
139 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.00 0.60 0.00 0.00 0.00 0.00
0.00 0.00 0.60 0.00  0.00  0.00  0.00
140 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 1.00 0.00 0.00 0.00 0.00
0.00 0.00 0.60 0.00  0.00  0.00  0.00
141 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.60 0.00 0.00 0.00 0.00
0.00 0.00 1.00 0.00  0.00  0.00  0.00
142 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.00 0.60 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.60  0.00  0.00  0.00
143 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.00 0.60 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.60  0.00  0.00  0.00
144 Amb. 2 (SLE R)             SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.00 0.60 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.60  0.00  0.00  0.00
```

145	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
146	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00
147	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	1.00	0.00	0.50	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
148	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
149	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	1.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
150	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
151	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00
152	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	1.00	0.00	0.50	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
153	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
154	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	1.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
155	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
156	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00
157	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	1.00	0.00	0.50	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
158	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
159	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
160	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
161	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00
162	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	1.00	0.00	0.50	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
163	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
164	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
165	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
166	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00
167	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
168	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
169	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
170	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
171	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
172	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
173	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
174	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
175	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	1.00	0.00	0.50	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.60	0.00	0.00	0.00
176	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.60	0.00	0.00	0.00
177	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.60	0.00	0.00	0.00
178	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
179	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	1.00	0.00	0.00	0.00
180	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	1.00	0.00	0.50	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.60	0.00	0.00	0.00
181	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	1.00	0.50	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.60	0.00	0.00	0.00
182	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.60	0.00	0.00	0.00
183	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
184	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	0.70	0.00	0.50	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	1.00	0.00	0.00	0.00
185	Amb. 2 (SLE R)			SLE	R	L	N	1.00	1.00	1.00	0.00	0.50	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.60	0.00	0.00	0.00

```
0.00 0.00 0.60 0.00  0.00  0.00  0.00
186 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.00 0.00 0.00 0.00 0.00 0.60
0.00 0.00 0.60 0.00  0.00  0.00  0.00
187 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.60
0.00 0.00 0.60 0.00  0.00  0.00  0.00
188 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 1.00
0.00 0.00 0.60 0.00  0.00  0.00  0.00
189 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.60
0.00 0.00 1.00 0.00  0.00  0.00  0.00
190 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.60
0.00 0.00 0.00 0.60  0.00  0.00  0.00
191 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.00 0.00 0.00 0.00 0.00 0.60
0.00 0.00 0.00 0.60  0.00  0.00  0.00
192 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.60
0.00 0.00 0.00 0.60  0.00  0.00  0.00
193 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 1.00
0.00 0.00 0.00 0.60  0.00  0.00  0.00
194 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.60
0.00 0.00 0.00 1.00  0.00  0.00  0.00
195 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.60 0.00 0.60 0.00  0.00  0.00  0.00
196 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.60 0.00 0.60 0.00  0.00  0.00  0.00
197 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.00
0.60 0.00 0.60 0.00  0.00  0.00  0.00
198 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
1.00 0.00 0.60 0.00  0.00  0.00  0.00
199 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.60 0.00 1.00 0.00  0.00  0.00  0.00
200 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.60 0.00 0.00 0.60  0.00  0.00  0.00
201 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.60 0.00 0.00 0.60  0.00  0.00  0.00
202 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.00
0.60 0.00 0.00 0.60  0.00  0.00  0.00
203 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
1.00 0.00 0.00 0.60  0.00  0.00  0.00
204 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.60 0.00 0.00 1.00  0.00  0.00  0.00
205 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.60 0.60 0.00  0.00  0.00  0.00
206 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.60 0.60 0.00  0.00  0.00  0.00
207 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.60 0.60 0.00  0.00  0.00  0.00
208 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 1.00 0.60 0.00  0.00  0.00  0.00
209 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.60 1.00 0.00  0.00  0.00  0.00
210 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 1.00 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.60 0.00 0.60  0.00  0.00  0.00
211 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 1.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.60 0.00 0.60  0.00  0.00  0.00
212 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 1.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.60 0.00 0.60  0.00  0.00  0.00
213 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 1.00 0.00 0.60  0.00  0.00  0.00
214 Amb. 2 (SLE R)              SLE R L   N  1.00 1.00 0.70 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.60 0.00 1.00  0.00  0.00  0.00
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ELENCO BARICENTRI E MASSE IMPALCATI:

Simbologia

Mo = Massa orizzontale
Nodo = Numero del nodo

Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo	Nodo	Mo
Nodo	Mo	Nodo	Mo										
	<kg>		<kg>		<kg>		<kg>		<kg>		<kg>		<kg>
<kg>		<kg>											
-26	85.94	-25	53.87	-24	65.53	-13	631.51	-12	587.59	-11	293.51	-10	641.43
-9	596.81	-8	651.35										
-7	606.04	-6	298.98	-5	641.43	-4	596.81	-3	631.51	-2	587.59	-1	293.51
101	336.09	102	118.36										
103	74.00	104	67.46	105	410.54	106	114.39	107	96.92	108	96.92	109	96.92
110	363.35	111	65.28										
112	69.64	113	106.45	114	106.45	115	276.74	116	377.87	117	374.77	118	368.42
122	374.77	123	369.36										

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 124 377.87    125 410.70    127 180.83    128  77.60    129 642.83    135 632.15    142 510.40
143 372.09    145  99.73
 201 307.67    202 115.28    203  88.65    204 179.98    205 483.48    206 145.27    207 163.84
208 163.84    209 163.84
 210 535.59    211 178.58    212  85.68    213  67.93    214  89.29    215 216.25    216  90.27
218 229.34    220 519.75
 221 205.75    223 301.54    224  90.27    225 359.91    229 626.00    230  50.76    231  58.79
232  58.79    233  58.79
 234  58.79    236 434.33    237  48.66    238  58.79    239  58.79    240  58.79    241  58.79
242 149.97


TOTALI MASSE NODI:

 Mo <kg>
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21394.30


ELENCO FORZE SISMICHE DI IMPALCATO

Simbologia

Fx   = Forza in dir. X
Fy   = Forza in dir. Y
Imp. = Numero dell'impalcato
cx   = Coeff. c in dir. X
cy   = Coeff. c in dir. Y

Imp.  cx   cy    Fx    Fy    Imp.  cx   cy    Fx    Fy    Imp.  cx   cy    Fx    Fy    Imp.  cx   cy
Fx    Fy
                <daN> <daN>                 <daN> <daN>                 <daN> <daN>
<daN> <daN>
-------------------------   -------------------------   -------------------------   -------------
------------
   1 0.27 0.27 -1.48  1.16      1 0.27 0.27 -1.48 -1.50      1 0.27 0.27 -1.48 -3.77      1 0.27 0.27
-0.93  1.16
   1 0.27 0.27 -0.93 -1.50      1 0.27 0.27 -0.36  1.16      1 0.27 0.27 -0.36 -1.50      1 0.27 0.27
-0.36 -3.77
   1 0.27 0.27  0.21  1.16      1 0.27 0.27  0.21 -1.50      1 0.27 0.27  0.76  1.16      1 0.27 0.27
0.76 -1.50
   1 0.27 0.27  0.76 -3.77      1 0.27 0.27  1.31 -3.77      1 0.27 0.27  1.31 -3.05      1 0.27 0.27
1.31 -2.37
   1 0.27 0.27  1.31 -2.07      1 0.27 0.27  1.31 -1.50      1 0.27 0.27  1.31 -0.97      1 0.27 0.27
1.31 -0.43
   1 0.27 0.27  1.31  0.10      1 0.27 0.27  1.31  0.63      1 0.27 0.27  1.31  1.16      1 0.27 0.27
1.31  1.69
   1 0.27 0.27  1.31  1.99      1 0.27 0.27  1.31  2.60      1 0.27 0.27  1.31  3.21      1 0.27 0.27
1.31  3.82
   1 0.27 0.27  0.76  3.82      1 0.27 0.27  0.21 -3.77      1 0.27 0.27  0.21  3.82      1 0.27 0.27
-0.93 -3.77
   1 0.27 0.27 -0.93  3.82      1 0.27 0.27 -1.48  3.82      1 0.27 0.27 -2.03 -3.77      1 0.27 0.27
-2.03 -2.10
   1 0.27 0.27 -2.03 -1.80      1 0.27 0.27 -2.03 -1.50      1 0.27 0.27 -2.03  1.16      1 0.27 0.27
-2.03  3.82
   1 0.27 0.27  0.06  4.19      1 0.27 0.27 -0.75  4.25      2 0.40 0.40  2.57  3.42      2 0.40 0.40
2.57  2.50
   2 0.40 0.40  2.57 -5.85      2 0.40 0.40  2.57 -7.81      2 0.40 0.40  2.57 -6.57      2 0.40 0.40
2.57 -5.40
   2 0.40 0.40  2.57 -4.88      2 0.40 0.40  2.57 -3.90      2 0.40 0.40  2.57 -2.98      2 0.40 0.40
2.57 -2.07
   2 0.40 0.40  2.57 -1.15      2 0.40 0.40  2.57 -0.24      2 0.40 0.40  2.57  0.68      2 0.40 0.40
2.57  1.59
   2 0.40 0.40  2.57  2.11      2 0.40 0.40  2.57  3.16      2 0.40 0.40  2.57  4.20      2 0.40 0.40
2.57  5.25
   2 0.40 0.40  1.62  5.25      2 0.40 0.40  0.68  5.25      2 0.40 0.40 -0.30 -7.81      2 0.40 0.40
-0.30  5.25
   2 0.40 0.40 -1.28  5.25      2 0.40 0.40 -2.23  5.25      2 0.40 0.40 -3.18 -7.81      2 0.40 0.40
-3.18 -3.90
   2 0.40 0.40 -3.18 -3.37      2 0.40 0.40 -3.18 -2.56      2 0.40 0.40 -3.18 -1.75      2 0.40 0.40
-3.18 -0.94
   2 0.40 0.40 -3.18 -0.13      2 0.40 0.40 -3.18  0.68      2 0.40 0.40 -3.18  1.20      2 0.40 0.40
-3.18  2.01
   2 0.40 0.40 -3.18  2.82      2 0.40 0.40 -3.18  3.63      2 0.40 0.40 -3.18  4.44      2 0.40 0.40
-3.18  5.25

TOTALI FORZE SISMICHE:

  Fx
<daN>
-----
```

0.00

ELENCO FORZE SISMICHE DI IMPALCATO

Imp.	cx	cy	Fx <daN>	Fy <daN>	Imp.	cx	cy	Fx <daN>	Fy <daN>	Imp.	cx	cy	Fx <daN>	Fy <daN>	Imp.	cx	cy	Fx <daN>	Fy <daN>
1	0.27	0.27	-3.67	2.88	1	0.27	0.27	-3.67	-3.71	1	0.27	0.27	-3.67	-9.37	1	0.27	0.27	-2.30	2.88
1	0.27	0.27	-2.30	-3.71	1	0.27	0.27	-0.89	2.88	1	0.27	0.27	-0.89	-3.71	1	0.27	0.27	-0.89	-9.37
1	0.27	0.27	0.52	2.88	1	0.27	0.27	0.52	-3.71	1	0.27	0.27	1.89	2.88	1	0.27	0.27	1.89	-3.71
1	0.27	0.27	1.89	-9.37	1	0.27	0.27	3.26	-9.37	1	0.27	0.27	3.26	-7.58	1	0.27	0.27	3.26	-5.88
1	0.27	0.27	3.26	-5.13	1	0.27	0.27	3.26	-3.71	1	0.27	0.27	3.26	-2.40	1	0.27	0.27	3.26	-1.08
1	0.27	0.27	3.26	0.24	1	0.27	0.27	3.26	1.56	1	0.27	0.27	3.26	2.88	1	0.27	0.27	3.26	4.20
1	0.27	0.27	3.26	4.95	1	0.27	0.27	3.26	6.46	1	0.27	0.27	3.26	7.97	1	0.27	0.27	3.26	9.47
1	0.27	0.27	1.89	9.47	1	0.27	0.27	0.52	-9.37	1	0.27	0.27	0.52	9.47	1	0.27	0.27	-2.30	-9.37
1	0.27	0.27	-2.30	9.47	1	0.27	0.27	-3.67	9.47	1	0.27	0.27	-5.03	-9.37	1	0.27	0.27	-5.03	-5.22
1	0.27	0.27	-5.03	-4.47	1	0.27	0.27	-5.03	-3.71	1	0.27	0.27	-5.03	2.88	1	0.27	0.27	-5.03	9.47
1	0.27	0.27	0.14	10.41	1	0.27	0.27	-1.86	10.54	2	0.40	0.40	6.38	8.48	2	0.40	0.40	6.38	6.21
2	0.40	0.40	6.38	-14.53	2	0.40	0.40	6.38	-19.39	2	0.40	0.40	6.38	-16.32	2	0.40	0.40	6.38	-13.40
2	0.40	0.40	6.38	-12.10	2	0.40	0.40	6.38	-9.67	2	0.40	0.40	6.38	-7.40	2	0.40	0.40	6.38	-5.13
2	0.40	0.40	6.38	-2.86	2	0.40	0.40	6.38	-0.59	2	0.40	0.40	6.38	1.68	2	0.40	0.40	6.38	3.95
2	0.40	0.40	6.38	5.24	2	0.40	0.40	6.38	7.84	2	0.40	0.40	6.38	10.43	2	0.40	0.40	6.38	13.02
2	0.40	0.40	4.03	13.02	2	0.40	0.40	1.68	13.02	2	0.40	0.40	-0.75	-19.39	2	0.40	0.40	-0.75	13.02
2	0.40	0.40	-3.18	13.02	2	0.40	0.40	-5.53	13.02	2	0.40	0.40	-7.88	-19.39	2	0.40	0.40	-7.88	-9.67
2	0.40	0.40	-7.88	-8.37	2	0.40	0.40	-7.88	-6.36	2	0.40	0.40	-7.88	-4.35	2	0.40	0.40	-7.88	-2.34
2	0.40	0.40	-7.88	-0.33	2	0.40	0.40	-7.88	1.68	2	0.40	0.40	-7.88	2.97	2	0.40	0.40	-7.88	4.98
2	0.40	0.40	-7.88	6.99	2	0.40	0.40	-7.88	9.00	2	0.40	0.40	-7.88	11.01	2	0.40	0.40	-7.88	13.02

TOTALI FORZE SISMICHE:

Fx <daN>	Fy <daN>
0.00	0.00

ELENCO MODI DI VIBRARE, MASSE PARTECIPANTI E COEFFICIENTI DI PARTECIPAZIONE

Simbologia

Φx = Coefficiente di partecipazione in dir. X
Φy = Coefficiente di partecipazione in dir. Y
Φz = Coefficiente di partecipazione in dir. Z
%Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z
%Mx = Percentuale massa partecipante in dir. X
%My = Percentuale massa partecipante in dir. Y
%Mz = Percentuale massa partecipante in dir. Z
C = * indica che il modo è stato considerato
Diff. = Minima differenza percentuale dagli altri periodi
Modo = Numero del modo di vibrare
T = Periodo

Modo	C	T	Diff.	Φx	Φy	Φz	%Mx	%My	%Mz	%Jpz
1	*	0.2515	0.86	-35.15	-0.97	0.00	57.742	0.044	0.000	0.000
2	*	0.2494	0.86	-1.11	34.31	0.00	0.057	55.012	0.000	0.000
3	*	0.1946	18.06	0.51	9.30	0.00	0.012	4.042	0.000	0.000
4	*	0.1649	4.74	23.58	0.20	0.00	25.980	0.002	0.000	0.000

5	*	0.1574	4.74	2.21	-2.06	0.00	0.229	0.199	0.000	0.000
6	*	0.1046	19.06	-0.08	-2.27	0.00	0.000	0.241	0.000	0.000
7	*	0.0879	14.11	-0.26	18.91	0.00	0.003	16.709	0.000	0.000
8	*	0.0770	9.17	-0.46	-10.27	0.00	0.010	4.926	0.000	0.000
9	*	0.0705	9.17	-1.26	2.27	0.00	0.075	0.241	0.000	0.000
10	*	0.0586	9.95	0.25	-10.87	0.00	0.003	5.525	0.000	0.000
11	*	0.0533	4.88	-2.97	-2.05	0.00	0.414	0.196	0.000	0.000
12	*	0.0508	2.43	-1.43	-12.95	0.00	0.096	7.835	0.000	0.000
13	*	0.0496	2.43	6.00	-1.12	0.00	1.684	0.059	0.000	0.000
14	*	0.0470	4.91	-16.60	0.57	0.00	12.878	0.015	0.000	0.000
15	*	0.0448	4.91	-0.73	8.71	0.00	0.025	3.543	0.000	0.000
16	*	0.0403	8.12	-0.03	2.00	0.00	0.000	0.186	0.000	0.000
17	*	0.0373	8.12	-1.84	0.59	0.00	0.158	0.016	0.000	0.000
18	*	0.0345	3.04	0.34	1.41	0.00	0.006	0.092	0.000	0.000
19	*	0.0335	3.04	0.29	4.38	0.00	0.004	0.898	0.000	0.000
20	*	0.0297	12.67	1.49	1.78	0.00	0.103	0.148	0.000	0.000
21	*	0.0252	3.89	-3.15	0.50	0.00	0.465	0.012	0.000	0.000
22	*	0.0242	3.89	-0.02	-0.19	0.00	0.000	0.002	0.000	0.000
23	*	0.0227	2.20	0.98	0.51	0.00	0.045	0.012	0.000	0.000
24	*	0.0222	2.20	-0.06	0.10	0.00	0.000	0.000	0.000	0.000
25	*	0.0214	3.89	0.00	-0.86	0.00	0.000	0.035	0.000	0.000
26	*	0.0185	3.38	0.15	-0.05	0.00	0.001	0.000	0.000	0.000
27	*	0.0179	3.01	0.03	-0.10	0.00	0.000	0.000	0.000	0.000
28	*	0.0174	3.01	0.02	0.21	0.00	0.000	0.002	0.000	0.000
29	*	0.0161	6.51	-0.42	0.08	0.00	0.008	0.000	0.000	0.000
30	*	0.0151	6.51	0.14	0.09	0.00	0.001	0.000	0.000	0.000
Tot.cons.							100.00	99.99	0.00	0.00

ELENCO COEFFICIENTI DI RISPOSTA

Simbologia

Modo = Numero del modo di vibrare
Sx = Coefficiente di risposta (*100) in dir. X
Sy = Coefficiente di risposta (*100) in dir. Y

Stato limite di danno

Modo	Sx	Sy
1	14.93	14.93
2	14.93	14.93
3	14.93	14.93
4	14.93	14.93
5	14.93	14.93
6	13.60	13.60
7	12.86	12.86
8	12.38	12.38
9	12.10	12.10
10	11.57	11.57
11	11.34	11.34
12	11.23	11.23
13	11.18	11.18
14	11.06	11.06
15	10.97	10.97
16	10.77	10.77
17	10.64	10.64
18	10.51	10.51
19	10.47	10.47
20	10.30	10.30
21	10.10	10.10
22	10.06	10.06
23	10.00	10.00
24	9.98	9.98
25	9.94	9.94
26	9.81	9.81
27	9.79	9.79
28	9.76	9.76
29	9.71	9.71
30	9.66	9.66

Stato limite di salvaguardia della vita

Modo	Sx	Sy
1	37.06	37.06
2	37.06	37.06
3	37.06	37.06
4	37.06	37.06
5	37.06	37.06

6	32.91	32.91
7	31.24	31.24
8	30.15	30.15
9	29.50	29.50
10	28.30	28.30
11	27.78	27.78
12	27.53	27.53
13	27.41	27.41
14	27.15	27.15
15	26.93	26.93
16	26.48	26.48
17	26.18	26.18
18	25.90	25.90
19	25.80	25.80
20	25.42	25.42
21	24.97	24.97
22	24.87	24.87
23	24.72	24.72
24	24.67	24.67
25	24.59	24.59
26	24.30	24.30
27	24.24	24.24
28	24.19	24.19
29	24.06	24.06
30	23.97	23.97

DOMANDA IN DUTTILITÀ DI CURVATURA
Direzione X μ_{EdX}=11.63
Direzione Y μ_{EdY}=11.72

Simbologia

Δ	<cm>	= Spostamento relativo membratura
Φ_{LT}		= Coefficiente Φ per stabilità laterale membrature inflesse
Φ_y		= Coefficiente Φ per inflessione intorno all'asse y(c)
Φ_z		= Coefficiente Φ per inflessione intorno all'asse z(e)
α		= Esponente sfruttamento per flessione retta intorno all'asse y
α_{imp}		= Coefficiente di imperfezione
αmy, αmz, αLT		= Coefficienti correttivi per il momento flettente
β		= Esponente sfruttamento per flessione retta intorno all'asse z
β_{LT}		= Coefficiente per calcolo Φ_{LT}
χ_{LT}		= Coefficiente di riduzione per stabilità laterale membrature inflesse
χ_y		= Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
χ_z		= Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
χ,min		= Coefficiente χ di riduzione per instabilità
δ	<cm>	= Spostamento relativo asta
λ^*_y		= Snellezza adimensionale per inflessione intorno all'asse y(c)
λ^*_z		= Snellezza adimensionale per inflessione intorno all'asse z(e)
λ_{LT}		= Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$		= Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
λ_y		= Snellezza per inflessione intorno all'asse y(c)
λ_z		= Snellezza per inflessione intorno all'asse z(e)
$\sigma_{ID,max}$	<daN/cmq>	= Tensione ideale massima
σ_M	<daN/cmq>	= Tensione normale per momento flettente
σ_N	<daN/cmq>	= Tensione normale per sforzo normale
τ	<daN/cmq>	= Tensione tangenziale per taglio e/o torsione
ψ		= Coeff. di correzione momento critico per stabilità laterale membrature inflesse
Aeff	<cmq>	= Area effettiva per trazione
Anet	<cmq>	= Area netta per compressione
Area	<cmq>	= Area
Atag,y	<cmq>	= Area resistente a taglio in dir. Y
Atag,z	<cmq>	= Area resistente a taglio in dir. Z
CC		= Numero della combinazione delle condizioni di carico elementari
Cod.		= Codice
Curva		= Curva di instabilità adottata
D	<cm>	= Distanza
Fyk	<daN/cmq>	= Tensione caratteristica di snervamento dell'acciaio
Fyt	<daN/cmq>	= Tensione caratteristica di rottura
Iy	<cm>	= Raggio giratorio d'inerzia rispetto all'asse Y
Iz	<cm>	= Raggio giratorio d'inerzia rispetto all'asse Z
Jω	<cm6>	= Costante di ingobbamento
Jy	<cm4>	= Momento d'inerzia rispetto all'asse Y
Jz	<cm4>	= Momento d'inerzia rispetto all'asse Z
Kyy, Kyz, Kzy, Kzz		= Coefficienti di interazione
L	<m>	= Lunghezza dell'asta

L_{cr} <m> = Lunghezza di libera inflessione laterale fra ritegni torsionali
M,cr <daNm> = Momento critico per instabilità flesso torsionale
MNy,c,Rd <daNm> = Resistenza di calcolo a pressoflessione intorno all'asse Y
MNz,c,Rd <daNm> = Resistenza di calcolo a pressoflessione intorno all'asse Z
Mx <daNm> = Momento torcente intorno all'asse X
My <daNm> = Momento flettente intorno all'asse Y
My,Ed <daNm> = Momento flettente di calcolo intorno all'asse Y
My,V,c,Rd <daNm> = Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Y
My,c,Rd <daNm> = Resistenza di calcolo a flessione intorno all'asse Y
Mz <daNm> = Momento flettente intorno all'asse Z
Mz,Ed <daNm> = Momento flettente di calcolo intorno all'asse Z
Mz,V,c,Rd <daNm> = Resistenza di calcolo a flessione ridotta per taglio intorno all'asse Z
Mz,c,Rd <daNm> = Resistenza di calcolo a flessione intorno all'asse Z
N <daN> = Sforzo normale
N,Ed <daN> = Forza assiale di calcolo
Nb,Rd <daN> = Resistenza all'instabilità
Nc,Rd <daN> = Resistenza a compressione
Ncr,y <daN> = Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
Ncr,z <daN> = Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
Npl,Rd <daN> = Resistenza plastica a trazione per sezione lorda
Nt,Rd <daN> = Resistenza a trazione ultima
Nu,Rd <daN> = Resistenza a rottura di trazione per sezione netta
Sez. = Numero della sezione
Tipo = Tipo sezione
Ia = Inerzie assegnate
Rc = Rettangolare cava
Is = I stondata
Tp = Tipo di acciaio
Ty <daN> = Taglio in dir. Y
Tz <daN> = Taglio in dir. Z
V,Ed <daN> = Forza di taglio di calcolo
Vc,Rd <daN> = Resistenza a taglio
Vc,Rd,Red <daN> = Resistenza a taglio ridotta
Wy,plas <cmc> = Modulo di resistenza plastico intorno all'asse Y
Wymin <cmc> = Modulo di resistenza minimo rispetto all'asse Y
Wz,plas <cmc> = Modulo di resistenza plastico intorno all'asse Z
Wzmin <cmc> = Modulo di resistenza minimo rispetto all'asse Z
Xl <m> = Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
f = Fattore di modifica per il coefficiente di riduzione
$f_{z,G}$ <cm> = Freccia in direzione Z globale
$f_{z,L}$ <cm> = Freccia in direzione Z locale
k_c = Coeff. di correzione momento flettente per stabilità laterale membrature inflesse

Caratteristiche profilati utilizzati

Sez.	Cod.	Tipo	D	Area	Anet	Aeff	Jy	Jz	Iy	Iz	Wymin	Wzmin	Tp	Fyk	Fyt
			<cm>	<cmq>	<cmq>	<cmq>	<cm4>	<cm4>	<cm>	<cm>	<cmc>	<cmc>		<daN/cmq>	<daN/cmq>
1	Travi principali_sottostruttura	Is	--	45.25	45.25	45.25	2510.34	924.60	7.45	4.52	293.61	102.73	S275 UNI EN 10025-2	2750.00	4300.00
2	Travi principali_copertura	Is	--	78.08	78.08	78.08	5696.29	2003.37	8.54	5.07	569.63	200.34	S275 UNI EN 10025-2	2750.00	4300.00
3	Travi secondarie_copertura	Is	--	25.34	25.34	25.34	606.17	230.90	4.89	3.02	106.34	38.48	S275 UNI EN 10025-2	2750.00	4300.00
4	Colonne principali	Is	--	78.08	78.08	78.08	5696.29	2003.37	8.54	5.07	569.63	200.34	S275 UNI EN 10025-2	2750.00	4300.00
5	Traversi_facciata	Is	--	16.43	16.43	16.43	541.23	44.92	5.74	1.65	77.32	12.31	S275 UNI EN 10025-2	2750.00	4300.00
6	Montanti principali_facciata	Is	--	16.43	16.43	16.43	541.23	44.92	5.74	1.65	77.32	12.31	S275 UNI EN 10025-2	2750.00	4300.00
7	Profili per pannelli_copertura	Rc	--	5.76	5.76	5.76	12.60	12.60	1.48	1.48	6.30	6.30	S275H UNI EN 10210-1	2750.00	4300.00
8	Travi terziarie_copertura	Is	--	13.21	13.21	13.21	317.76	27.67	4.90	1.45	52.96	8.65	S275 UNI EN 10025-2	2750.00	4300.00
9	Travi_facciata	Is	--	31.42	31.42	31.42	1033.15	389.32	5.73	3.52	155.36	55.62	S275 UNI EN 10025-2	2750.00	4300.00
10	Travi secondarie_sottostruttura	Is	--	28.48	28.48	28.48	1943.23	142.37	8.26	2.24	194.32	28.47	S275 UNI EN 10025-2	2750.00	4300.00
11	Travi terziarie_sottostruttura	Is	--	20.09	20.09	20.09	869.32	68.31	6.58	1.84	108.66	16.66	S275 UNI EN 10025-2	2750.00	4300.00
12	Montanti secondari	Is	--	20.09	20.09	20.09	869.32	68.31	6.58	1.84	108.66	16.66	S275 UNI EN 10025-2	2750.00	4300.00
14	Montanti secondari_facciata vetrata	Is	--	34.01	34.01	34.01	864.39	317.52	5.04	3.06	144.06	52.92	S275 UNI EN 10025-2	2750.00	4300.00

15 Traversi secondari_facciata vetrata Is -- 34.01 34.01 34.01 864.39 317.52 5.04 3.06 144.06 52.92 S275 UNI EN 10025-2 2750.00 4300.00

Caratteristiche profilati utilizzati

Sez.	Cod.	Wy,plas <cmc>	Wz,plas <cmc>	Atag,y <cmq>	Atag,z <cmq>	Jω <cm6>
1	Travi principali_sottostruttura	326.12	156.65	37.93	14.47	60210.90
2	Travi principali_copertura	644.58	306.10	66.02	24.83	171125.00
3	Travi secondarie_copertura	120.00	58.93	21.64	8.46	6471.94
4	Colonne principali	644.58	306.10	66.02	24.83	171125.00
5	Traversi_facciata	88.58	19.27	11.15	7.64	1981.36
6	Montanti principali_facciata	88.58	19.27	11.15	7.64	1981.36
7	Profili per pannelli_copertura	7.81	7.81	2.88	2.88	
8	Travi terziarie_copertura	60.93	13.60	9.10	6.31	889.59
9	Travi_facciata	174.11	84.93	26.36	10.12	15063.70
10	Travi secondarie_sottostruttura	221.64	44.70	19.58	14.00	12988.10
11	Travi terziarie_sottostruttura	124.31	26.14	13.73	9.66	3958.87
12	Montanti secondari	124.31	26.14	13.73	9.66	3958.87
14	Montanti secondari_facciata vetrata	165.73	81.06	29.20	10.96	9409.75
15	Traversi secondari_facciata vetrata	165.73	81.06	29.20	10.96	9409.75

Asta n. 1 (1 101) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.83 - Classe 3
  Sollecitazioni: N=-3503.01 T_z=-531.54 M_y=440.65 T_y=-509.04 M_z=-422.00 M_x=5.22
  Tensioni: σ_N=-44.86 $\sigma_{m,d}$=-288.00 τ=14.72 σ_{max}=-332.86 (sic.=7.868)
  Tensioni: σ_N=-44.86 $\sigma_{m,d}$=61.31 τ=38.66 τ_{max}=38.66 (sic.=39.117)
  Tensioni: σ_N=-44.86 $\sigma_{m,d}$=-288.00 τ=14.72 $\sigma_{ID,max}$=333.84 (sic.=7.845)

- Verifica a taglio Dir. Y [4.2.16] - CC 62 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-1521.59
  V,Ed=-1521.59 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.02 (sic.=65.614)

- Verifica a taglio Dir. Z [4.2.16] - CC 62 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=-1772.03
  V,Ed=-1772.03 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.05 (sic.=21.191)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 100 SLU Xl=0.83 - Classe 1
  Sollecitazioni: N=-3682.81 T_z=-1460.69 M_y=1210.91 T_y=-1615.73 M_z=-1339.44 M_x=2.21
  N,Ed=-3682.81 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.02
  Pressoflessione retta YY [4.2.33]:
  My,Ed=1210.91 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.07 (sic.=13.941)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-1339.44 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.17 (sic.=5.985)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.17 (sic.=5.806)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 52 SLU - Classe 1
  Sollecitazioni: N,Ed=-3656.20 My,Ed=1236.77 Mz,Ed=-1336.99 L=1.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=204556.00 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.42 Ncr,y=2951560.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_z=39.48 Ncr,z=1038060.00 λ^*_z=0.45 Curva c: Φ_z=0.67 χ_z=0.87
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.96
  Verifica YY: 0.02+0.07+0.10=0.18 (sic.=5.444)
  Verifica ZZ: 0.02+0.04+0.16=0.22 (sic.=4.507)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 194
  δ=0.14 (L/596) (sic.=1.987)

Asta n. 1 (101 -15) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-1527.16 T_z=-170.06 M_y=-248.24 T_y=-484.45 M_z=829.39 M_x=-1.47
  Tensioni: σ_N=-19.56 $\sigma_{m,d}$=-457.58 τ=4.15 σ_{max}=-477.14 (sic.=5.489)
  Tensioni: σ_N=-19.56 $\sigma_{m,d}$=47.83 τ=14.31 τ_{max}=14.31 (sic. >100)
  Tensioni: σ_N=-19.56 $\sigma_{m,d}$=-457.58 τ=4.15 $\sigma_{ID,max}$=477.19 (sic.=5.488)

- Verifica a taglio Dir. Y [4.2.16] - CC 66 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-146.62
  V,Ed=-146.62 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 66 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=-750.23
  V,Ed=-750.23 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=50.053)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 57 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=-2407.74 T_z=-535.47 M_y=-978.46 T_y=-337.81 M_z=624.73 M_x=4.61
N,Ed=-2407.74 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-978.46 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=17.254)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=624.73 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.08 (sic.=12.833)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=12.302)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-1527.16 My,Ed=-248.24 Mz,Ed=829.39 L=1.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.36 M,cr=159488.00 λ_{LT}=0.31
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=23.42 Ncr,y=2951560.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_z=39.48 Ncr,z=1038060.00 λ^*_z=0.45 Curva c: Φ_z=0.67 χ_z=0.87
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.02+0.15=0.17 (sic.=5.747)
Verifica ZZ: 0.01+0.01+0.15=0.17 (sic.=5.821)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.08 (L/1181) (sic.=3.937)

Asta n. 1 (-15 201) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=2.57 - Classe 3
Sollecitazioni: N=-1364.89 T_z=-246.58 M_y=570.52 T_y=-446.52 M_z=830.64 M_x=1.54
Tensioni: σ_N=-17.48 $\sigma_{m,d}$=-514.78 τ=4.34 σ_{max}=-532.26 (sic.=4.921)
Tensioni: σ_N=-17.48 $\sigma_{m,d}$=48.45 τ=17.90 τ_{max}=17.90 (sic.=84.460)
Tensioni: σ_N=-17.48 $\sigma_{m,d}$=-514.78 τ=4.34 $\sigma_{ID,max}$=532.31 (sic.=4.920)

- Verifica a taglio Dir. Y [4.2.16] - CC 66 SLU Xl=0.06 - Classe 1
Sollecitazioni: T_y=-146.62
V,Ed=-146.62 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 66 SLU Xl=0.06 - Classe 1
Sollecitazioni: T_z=-570.29
V,Ed=-570.29 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=65.846)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 66 SLU Xl=2.57 - Classe 1
Sollecitazioni: N=-1996.46 T_z=-480.90 M_y=1098.70 T_y=-146.62 M_z=-205.01
N,Ed=-1996.46 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=1098.70 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.07 (sic.=15.365)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-205.01 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.03 (sic.=39.105)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.07 (sic.=15.365)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-1530.63 My,Ed=570.52 Mz,Ed=830.64 L=2.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=5.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.90 M,cr=51902.80 λ_{LT}=0.55
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
λ_y=64.63 Ncr,y=387465.00 λ^*_y=0.74 Curva b: Φ_y=0.87 χ_y=0.76
λ_z=108.98 Ncr,z=136271.00 λ^*_z=1.26 Curva c: Φ_z=1.55 χ_z=0.41
Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.01+0.04+0.15=0.20 (sic.=5.006)
Verifica ZZ: 0.02+0.03+0.15=0.20 (sic.=4.984)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 155
δ=0.14 (L/1735) (sic.=5.783)

Asta n. 2 (102 202) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a compressione (4.2.4.1.2.2) - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-647.97
Verifica a compressione [4.2.9]
N,Ed=-647.97 Nc,Rd=-52621.20 N,Ed/Nc,Rd=0.01 (sic.=81.210)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=3.56 - Classe 1
Sollecitazioni: T_z=-123.49
V,Ed=-123.49 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=1.78 - Classe 1
Sollecitazioni: N=27.73 M_y=-109.90
My,Ed=-109.90 My,c,Rd=3255.72
N,Ed=27.73 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03 (sic.=29.623)

- Verifica di stabilità (4.2.4.1.3.1) - CC 100 SLU
  Sollecitazioni: N=-1134.25
  L=3.76
  λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66
  Curva a: Φ_y=0.76 χ_y=0.87
  λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35
  Curva b: Φ_z=3.62 χ_z=0.16
  χ,min=0.16 N,Ed=-1134.25 Nb,Rd=8243.74 N,Ed/Nb,Rd=0.14 (sic.=7.268)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 110 SLU - Classe 1
  Sollecitazioni: N,Ed=-978.53 My,Ed=65.94 L=3.76
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
  λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
  λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
  Kyy, Kyz, Kzy, Kzz=0.96, 0.66, 0.00, 1.11
  Verifica YY: 0.02+0.03=0.05 (sic.=20.123)
  Verifica ZZ: 0.12=0.12 (sic.=8.425)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 160
  δ=0.30 (L/1184) (sic.=3.947)

Asta n. 3 (103 3) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a trazione (4.2.4.1.2.1) - CC 9 SND Xl=2.12 - Classe 3
  Sollecitazioni: N=177.60
  Verifica a trazione [4.2.5]
  N,Ed=177.60 Npl,Rd=52621.20 Nu,Rd=62204.00 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 73 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=83.70
  V,Ed=83.70 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 109 SLU Xl=1.74 - Classe 1
  Sollecitazioni: N=163.55 M_y=71.86
  My,Ed=71.86 My,c,Rd=3255.72
  N,Ed=163.55 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02
(sic.=45.304)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 94 SLU - Classe 1
  Sollecitazioni: N,Ed=-103.16 My,Ed=-71.85 Mz,Ed=0.05 L=2.16
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.16 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=6347.05 λ_{LT}=0.73
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.76 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
  λ_y=32.84 Ncr,y=386179.00 λ^*_y=0.38 Curva a: Φ_y=0.59 χ_y=0.96
  λ_z=117.14 Ncr,z=30347.70 λ^*_z=1.35 Curva b: Φ_z=1.61 χ_z=0.40
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.96
  Verifica YY: 0.00+0.02+0.00=0.03 (sic.=38.517)
  Verifica ZZ: 0.00+0.01+0.00=0.02 (sic.=51.945)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 160
  δ=0.24 (L/900) (sic.=3.000)

Asta n. 3 (3 -20) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.66 - Classe 3
  Sollecitazioni: N=183.99 T_y=-7.33 M_z=-4.07
  Tensioni: σ_N=9.16 $\sigma_{m,d}$=24.41 τ=0.00 σ_{max}=33.57 (sic.=78.019)
  Tensioni: σ_N=9.16 $\sigma_{m,d}$=-6.85 τ=0.83 τ_{max}=0.83 (sic. >100)
  Tensioni: σ_N=9.16 $\sigma_{m,d}$=24.41 τ=0.00 $\sigma_{ID,max}$=33.57 (sic.=78.019)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.66 - Classe 1
  Sollecitazioni: T_z=-44.00
  V,Ed=-44.00 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 109 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=180.68 T_z=22.82 M_y=66.22
  My,Ed=66.22 My,V,c,Rd=3255.72
  N,Ed=180.68 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02
(sic.=49.165)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 94 SLU - Classe 1
  Sollecitazioni: N,Ed=-33.47 My,Ed=-66.21 Mz,Ed=-0.52 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=27702.20 λ_{LT}=0.35
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=10.64 Ncr,y=3677050.00 λ^*_y=0.12 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=37.96 Ncr,z=288960.00 λ^*_z=0.44 Curva b: Φ_z=0.64 χ_z=0.91

Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.02+0.00=0.02 (sic.=49.052)
Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=76.878)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 160
δ=0.05 (L/1158) (sic.=3.860)

Asta n. 3 (-20 203) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.04 - Classe 3
Sollecitazioni: N=198.58 T_y=-6.16 M_z=4.09
Tensioni: σ_N=9.88 $\sigma_{m,d}$=24.52 τ=0.00 σ_{max}=34.40 (sic.=76.132)
Tensioni: σ_N=9.88 $\sigma_{m,d}$=6.88 τ=0.70 τ_{max}=0.70 (sic. >100)
Tensioni: σ_N=9.88 $\sigma_{m,d}$=24.52 τ=0.00 $\sigma_{ID,max}$=34.40 (sic.=76.132)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.70 - Classe 1
Sollecitazioni: T_z=-79.35
V,Ed=-79.35 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 89 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=194.66 T_z=-47.01 M_y=-41.92
My,Ed=-41.92 My,V,c,Rd=3255.72
N,Ed=194.66 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.01
(sic.=77.664)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 94 SLU - Classe 1
Sollecitazioni: N,Ed=-10.93 My,Ed=-41.92 Mz,Ed=-0.41 L=0.90
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.90 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=26080.30 λ_{LT}=0.36
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=13.68 Ncr,y=2224390.00 λ^*_y=0.16 Curva a: Φ_y=0.51 χ_y=1.00
λ_z=48.81 Ncr,z=174803.00 λ^*_z=0.56 Curva b: Φ_z=0.72 χ_z=0.86
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.00=0.01 (sic.=78.249)
Verifica ZZ: 0.00+0.01+0.00=0.01 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 208
δ=0.07 (L/899) (sic.=2.997)

Asta n. 4 (104 4) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a compressione (4.2.4.1.2.2) - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-582.11
Verifica a compressione [4.2.9]
N,Ed=-582.11 Nc,Rd=-52621.20 N,Ed/Nc,Rd=0.01 (sic.=90.398)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=75.32
V,Ed=75.32 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 89 SLU Xl=1.75 - Classe 1
Sollecitazioni: N=25.84 M_y=-65.78
My,Ed=-65.78 My,c,Rd=3255.72
N,Ed=25.84 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02 (sic.=49.497)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-582.11 My,Ed=-0.05 Mz,Ed=-0.38 L=2.16
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.16 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=6347.05 λ_{LT}=0.69
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
λ_y=32.84 Ncr,y=386179.00 λ^*_y=0.38 Curva a: Φ_y=0.59 χ_y=0.96
λ_z=117.14 Ncr,z=30347.70 λ^*_z=1.35 Curva b: Φ_z=1.61 χ_z=0.40
Kyy, Kyz, Kzy, Kzz=0.95, 0.97, 0.76, 0.97
Verifica YY: 0.01+0.00+0.00=0.01 (sic.=80.570)
Verifica ZZ: 0.03+0.00+0.00=0.03 (sic.=35.389)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 160
δ=0.22 (L/977) (sic.=3.257)

Asta n. 4 (4 -21) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.66 - Classe 3
Sollecitazioni: N=-520.09 T_y=7.47 M_z=4.47
Tensioni: σ_N=-25.89 $\sigma_{m,d}$=-26.82 τ=0.00 σ_{max}=-52.71 (sic.=49.689)
Tensioni: σ_N=-25.89 $\sigma_{m,d}$=7.52 τ=0.85 τ_{max}=0.85 (sic. >100)
Tensioni: σ_N=-25.89 $\sigma_{m,d}$=-26.82 τ=0.00 $\sigma_{ID,max}$=52.71 (sic.=49.689)

- Verifica a taglio Dir. Z [4.2.16] - CC 109 SLU Xl=0.66 - Classe 1
Sollecitazioni: T_z=36.51

V,Ed=36.51 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 89 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=42.19 T_z=-18.86 M_y=-61.46
  My,Ed=-61.46 My,V,c,Rd=3255.72
  N,Ed=42.19 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02 (sic.=52.976)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 94 SLU - Classe 1
  Sollecitazioni: N,Ed=-150.52 My,Ed=-61.46 Mz,Ed=0.56 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.15 M,cr=27196.00 λ_{LT}=0.35
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=10.64 Ncr,y=3677050.00 λ^*_y=0.12 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=37.96 Ncr,z=288960.00 λ^*_z=0.44 Curva b: Φ_z=0.64 χ_z=0.91
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.02+0.00=0.02 (sic.=47.051)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=68.159)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 160
  δ=0.05 (L/1256) (sic.=4.187)

Asta n. 4 (-21 204) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-516.01 T_y=-5.91 M_z=4.43
  Tensioni: σ_N=-25.68 $\sigma_{m,d}$=-26.59 τ=0.00 σ_{max}=-52.28 (sic.=50.099)
  Tensioni: σ_N=-25.68 $\sigma_{m,d}$=7.46 τ=0.67 τ_{max}=0.67 (sic. >100)
  Tensioni: σ_N=-25.68 $\sigma_{m,d}$=-26.59 τ=0.00 $\sigma_{ID,max}$=52.28 (sic.=50.099)

- Verifica a taglio Dir. Z [4.2.16] - CC 69 SLU Xl=0.79 - Classe 1
  Sollecitazioni: T_z=-71.40
  V,Ed=-71.40 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 109 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=55.09 T_z=39.11 M_y=41.40
  My,Ed=41.40 My,V,c,Rd=3255.72
  N,Ed=55.09 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.01 (sic.=78.644)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-516.01 My,Ed=0.02 Mz,Ed=4.43 L=0.90
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.90 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=26080.30 λ_{LT}=0.34
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=13.68 Ncr,y=2224390.00 λ^*_y=0.16 Curva a: Φ_y=0.51 χ_y=1.00
  λ_z=48.81 Ncr,z=174803.00 λ^*_z=0.56 Curva b: Φ_z=0.72 χ_z=0.86
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.01=0.02 (sic.=51.293)
  Verifica ZZ: 0.01+0.01=0.02 (sic.=47.282)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 160
  δ=0.05 (L/1562) (sic.=5.207)

Asta n. 5 (5 105) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.83 - Classe 3
  Sollecitazioni: N=-4006.28 T_z=-1170.68 M_y=970.49 T_y=1023.40 M_z=848.40
  Tensioni: σ_N=-51.31 $\sigma_{m,d}$=-593.86 τ=0.00 σ_{max}=-645.17 (sic.=4.059)
  Tensioni: σ_N=-51.31 $\sigma_{m,d}$=-19.06 τ=76.74 τ_{max}=76.74 (sic.=19.705)
  Tensioni: σ_N=-51.31 $\sigma_{m,d}$=-593.86 τ=0.00 $\sigma_{ID,max}$=645.17 (sic.=4.059)

- Verifica a taglio Dir. Y [4.2.16] - CC 58 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-491.22
  V,Ed=-491.22 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 58 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=-2863.79
  V,Ed=-2863.79 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.08 (sic.=13.112)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 58 SLU Xl=0.83 - Classe 1
  Sollecitazioni: N=-5890.18 T_z=-2863.79 M_y=2374.08 T_y=-491.22 M_z=-407.22
  N,Ed=-5890.18 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.03
  Pressoflessione retta YY [4.2.33]:
  My,Ed=2374.08 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.14 (sic.=7.111)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-407.22 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.05 (sic.=19.687)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.14 (sic.=7.111)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-4057.09 My,Ed=970.49 Mz,Ed=848.40 L=1.00

αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=204556.00 λ_{LT}=0.28
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=23.42 Ncr,y=2951560.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_Z=39.48 Ncr,z=1038060.00 λ^*_z=0.45 Curva c: Φ_z=0.67 χ_z=0.87
Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02+0.06+0.15=0.24 (sic.=4.221)
Verifica ZZ: 0.02+0.05+0.15=0.23 (sic.=4.405)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.15 (L/551) (sic.=1.837)

Asta n. 5 (105 43) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-1610.79 T_z=-252.94 M_y=-440.70 T_y=-573.77 M_z=991.26
Tensioni: σ_N=-20.63 $\sigma_{m,d}$=-572.16 τ=0.00 σ_{max}=-592.79 (sic.=4.418)
Tensioni: σ_N=-20.63 $\sigma_{m,d}$=-74.10 τ=16.92 τ_{max}=16.92 (sic.=89.364)
Tensioni: σ_N=-20.63 $\sigma_{m,d}$=-572.16 τ=0.00 $\sigma_{ID,max}$=592.79 (sic.=4.418)

- Verifica a taglio Dir. Y [4.2.16] - CC 66 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-60.30
V,Ed=-60.30 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 66 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=-753.12
V,Ed=-753.12 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=49.861)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 67 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-2069.34 T_z=-676.31 M_y=-1304.66 T_y=-63.84 M_z=132.75
N,Ed=-2069.34 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-1304.66 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.08 (sic.=12.940)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=132.75 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=60.392)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=12.940)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-1610.79 My,Ed=-440.70 Mz,Ed=991.26 L=1.60
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.28 M,cr=71691.00 λ_{LT}=0.47
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.59 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=37.47 Ncr,y=1152950.00 λ^*_y=0.43 Curva b: Φ_y=0.63 χ_y=0.91
λ_Z=63.18 Ncr,z=405491.00 λ^*_z=0.73 Curva c: Φ_z=0.89 χ_z=0.71
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.03+0.18=0.22 (sic.=4.604)
Verifica ZZ: 0.01+0.02+0.18=0.21 (sic.=4.672)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.20 (L/780) (sic.=2.600)

Asta n. 5 (43 205) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.97 - Classe 3
Sollecitazioni: N=-1439.09 T_z=-286.37 M_y=575.79 T_y=562.22 M_z=1035.79
Tensioni: σ_N=-18.43 $\sigma_{m,d}$=-618.11 τ=0.00 σ_{max}=-636.54 (sic.=4.115)
Tensioni: σ_N=-18.43 $\sigma_{m,d}$=-23.27 τ=18.87 τ_{max}=18.87 (sic.=80.135)
Tensioni: σ_N=-18.43 $\sigma_{m,d}$=-618.11 τ=0.00 $\sigma_{ID,max}$=636.54 (sic.=4.115)

- Verifica a taglio Dir. Y [4.2.16] - CC 66 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=-59.41
V,Ed=-59.41 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 66 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_z=-706.13
V,Ed=-706.13 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=53.179)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 66 SLU Xl=1.97 - Classe 1
Sollecitazioni: N=-1659.38 T_z=-601.03 M_y=1297.42 T_y=-59.41 M_z=-94.52
N,Ed=-1659.38 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=1297.42 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.08 (sic.=13.012)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-94.52 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic.=84.819)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=13.012)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-1571.58 My,Ed=575.79 Mz,Ed=1035.79 L=2.16
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=4.32 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.14 M,cr=79507.80 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=50.58 Ncr,y=632621.00 λ^*_y=0.58 Curva b: Φ_y=0.73 χ_y=0.85
  λ_z=85.29 Ncr,z=222491.00 λ^*_z=0.98 Curva c: Φ_z=1.17 χ_z=0.55
  Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.01+0.04+0.19=0.23 (sic.=4.256)
  Verifica ZZ: 0.01+0.03+0.19=0.23 (sic.=4.302)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 165
  δ=0.16 (L/1201) (sic.=4.003)

Asta n. 6 (106 6) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.56 - Classe 3
  Sollecitazioni: N=-549.20 M_z=1.02
  Tensioni: σ_N=-27.33 $\sigma_{m,d}$=-6.13 τ=0.00 σ_{max}=-33.46 (sic.=78.274)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=-27.33 $\sigma_{m,d}$=-6.13 τ=0.00 $\sigma_{ID,max}$=33.46 (sic.=78.274)

- Verifica a taglio Dir. Z [4.2.16] - CC 46 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=62.93
  V,Ed=62.93 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 46 SLU Xl=1.56 - Classe 1
  Sollecitazioni: N=96.82 T_z=21.89 M_y=-66.31
  My,Ed=-66.31 My,V,c,Rd=3255.72
  N,Ed=96.82 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02 (sic.=49.101)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 109 SLU - Classe 1
  Sollecitazioni: N,Ed=-321.40 My,Ed=66.29 Mz,Ed=-0.55 L=1.60
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.60 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=9895.49 λ_{LT}=0.59
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_y=24.32 Ncr,y=703811.00 λ^*_y=0.28 Curva a: Φ_y=0.55 χ_y=0.98
  λ_z=86.77 Ncr,z=55308.70 λ^*_z=1.00 Curva b: Φ_z=1.14 χ_z=0.60
  Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.57, 0.96
  Verifica YY: 0.01+0.02+0.00=0.03 (sic.=36.922)
  Verifica ZZ: 0.01+0.01+0.00=0.02 (sic.=43.037)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
  δ=0.19 (L/820) (sic.=2.733)

Asta n. 6 (6 206) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a compressione (4.2.4.1.2.2) - CC 9 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-589.19
  Verifica a compressione [4.2.9]
  N,Ed=-589.19 Nc,Rd=-52621.20 N,Ed/Nc,Rd=0.01 (sic.=89.311)

- Verifica a taglio Dir. Z [4.2.16] - CC 66 SLU Xl=2.05 - Classe 1
  Sollecitazioni: T_z=86.48
  V,Ed=86.48 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 66 SLU Xl=0.40 - Classe 1
  Sollecitazioni: N=39.33 M_y=71.23
  My,Ed=71.23 My,c,Rd=3255.72
  N,Ed=39.33 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02 (sic.=45.704)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-589.19 My,Ed=0.01 Mz,Ed=-0.96 L=2.16
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.16 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=6347.05 λ_{LT}=0.69
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
  λ_y=32.84 Ncr,y=386179.00 λ^*_y=0.38 Curva a: Φ_y=0.59 χ_y=0.96
  λ_z=117.14 Ncr,z=30347.70 λ^*_z=1.35 Curva b: Φ_z=1.61 χ_z=0.40
  Kyy, Kyz, Kzy, Kzz=0.95, 0.97, 0.76, 0.97
  Verifica YY: 0.01+0.00=0.01 (sic.=72.428)
  Verifica ZZ: 0.03+0.00=0.03 (sic.=33.502)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
  δ=0.17 (L/1205) (sic.=4.017)

Asta n. 7 (107 207) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a trazione (4.2.4.1.2.1) - CC 1 SND Xl=3.65 - Classe 3
  Sollecitazioni: N=225.79

Verifica a trazione [4.2.5]
N,Ed=225.79 Npl,Rd=52621.20 Nu,Rd=62204.00 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=95.70
V,Ed=95.70 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=1.82 - Classe 1
Sollecitazioni: N=91.37 M_y=-87.22
My,Ed=-87.22 My,c,Rd=3255.72
N,Ed=91.37 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03 (sic.=37.328)

- Verifica di stabilità (4.2.4.1.3.1)
In tutte le CC risulta N < 0.04*N,cr e quindi non sono necessarie le verifiche di stabilità

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 109 SLU - Classe 1
Sollecitazioni: N,Ed=-42.83 My,Ed=87.22 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
λ_Y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_Z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.96
Verifica YY: 0.00+0.04=0.04 (sic.=26.362)
Verifica ZZ: 0.01=0.01 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.40 (L/909) (sic.=3.030)

Asta n. 8 (108 208) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a trazione (4.2.4.1.2.1) - CC 9 SND Xl=3.65 - Classe 3
Sollecitazioni: N=227.79
Verifica a trazione [4.2.5]
N,Ed=227.79 Npl,Rd=52621.20 Nu,Rd=62204.00 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=95.70
V,Ed=95.70 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=1.82 - Classe 1
Sollecitazioni: N=85.82 M_y=-87.22
My,Ed=-87.22 My,c,Rd=3255.72
N,Ed=85.82 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03 (sic.=37.328)

- Verifica di stabilità (4.2.4.1.3.1)
In tutte le CC risulta N < 0.04*N,cr e quindi non sono necessarie le verifiche di stabilità

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
Sollecitazioni: N,Ed=-12.17 My,Ed=-87.22 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
λ_Y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_Z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.04=0.04 (sic.=26.846)
Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.44 (L/830) (sic.=2.767)

Asta n. 9 (109 209) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a compressione (4.2.4.1.2.2) - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-613.73
Verifica a compressione [4.2.9]
N,Ed=-613.73 Nc,Rd=-52621.20 N,Ed/Nc,Rd=0.01 (sic.=85.740)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=-95.70
V,Ed=-95.70 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=1.82 - Classe 1
Sollecitazioni: N=-49.32 M_y=-87.22
My,Ed=-87.22 My,c,Rd=3255.72
N,Ed=-49.32 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03
(sic.=37.328)

- Verifica di stabilità (4.2.4.1.3.1) - CC 1 SND

Sollecitazioni: N=-613.73 M_z=-0.00
L=3.76
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66
Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35
Curva b: Φ_z=3.62 χ_z=0.16
χ,min=0.16 N,Ed=-613.73 Nb,Rd=8243.74 N,Ed/Nb,Rd=0.07 (sic.=13.432)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
Sollecitazioni: N,Ed=-305.06 My,Ed=-87.22 Mz,Ed=-0.00 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.95, 0.60, 0.57, 1.00
Verifica YY: 0.01+0.04=0.04 (sic.=22.840)
Verifica ZZ: 0.04+0.02=0.06 (sic.=16.875)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.46 (L/791) (sic.=2.637)

Asta n. 10 (10 110) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.83 - Classe 3
Sollecitazioni: N=-3839.76 T_z=-1483.67 M_y=1229.96 T_y=-1032.47 M_z=-855.91
Tensioni: σ_N=-49.18 $\sigma_{m,d}$=-643.16 τ=0.00 σ_{max}=-692.34 (sic.=3.783)
Tensioni: σ_N=-49.18 $\sigma_{m,d}$=19.23 τ=97.21 τ_{max}=97.21 (sic.=15.556)
Tensioni: σ_N=-49.18 $\sigma_{m,d}$=-643.16 τ=0.00 $\sigma_{ID,max}$=692.34 (sic.=3.783)

- Verifica a taglio Dir. Y [4.2.16] - CC 106 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=358.54
V,Ed=358.54 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 106 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=-2965.22
V,Ed=-2965.22 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.08 (sic.=12.664)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 106 SLU Xl=0.83 - Classe 1
Sollecitazioni: N=-6478.30 T_z=-2965.22 M_y=2458.17 T_y=358.54 M_z=297.23
N,Ed=-6478.30 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.03
Pressoflessione retta YY [4.2.33]:
My,Ed=2458.17 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.15 (sic.=6.868)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=297.23 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.04 (sic.=26.972)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.15 (sic.=6.868)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-3890.58 My,Ed=1229.96 Mz,Ed=-855.91 L=1.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=204556.00 λ_{LT}=0.28
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=23.42 Ncr,y=2951560.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_z=39.48 Ncr,z=1038060.00 λ^*_z=0.45 Curva c: Φ_z=0.67 χ_z=0.87
Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.02+0.08+0.16=0.25 (sic.=3.937)
Verifica ZZ: 0.02+0.06+0.16=0.24 (sic.=4.155)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 160
δ=0.11 (L/743) (sic.=2.477)

Asta n. 10 (110 210) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-1409.83 T_z=-124.48 M_y=-441.34 T_y=-568.59 M_z=980.98
Tensioni: σ_N=-18.06 $\sigma_{m,d}$=-567.14 τ=0.00 σ_{max}=-585.20 (sic.=4.475)
Tensioni: σ_N=-18.06 $\sigma_{m,d}$=-176.03 τ=13.54 τ_{max}=13.54 (sic. >100)
Tensioni: σ_N=-18.06 $\sigma_{m,d}$=-567.14 τ=0.00 $\sigma_{ID,max}$=585.20 (sic.=4.475)

- Verifica a taglio Dir. Y [4.2.16] - CC 66 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-26.21
V,Ed=-26.21 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 66 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=-386.91
V,Ed=-386.91 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=97.054)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 66 SLU Xl=0.00 - Classe 1

Sollecitazioni: N=-1660.89 T_z=-386.91 M_y=-986.79 T_y=-26.21 M_z=34.17
N,Ed=-1660.89 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-986.79 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=17.108)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=34.17 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=17.108)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-1409.83 My,Ed=-441.34 Mz,Ed=-1048.72 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=7.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.81 M,cr=34496.40 λ_{LT}=0.67
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.72 β_{LT}=0.75 f=0.97 χ_{LT}=0.91
λ_y=88.04 Ncr,y=208773.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
λ_z=148.46 Ncr,z=73425.20 λ^*_z=1.71 Curva c: Φ_z=2.33 χ_z=0.26
Kyy, Kyz, Kzy, Kzz=0.96, 0.97, 0.77, 0.97
Verifica YY: 0.01+0.03+0.19=0.24 (sic.=4.241)
Verifica ZZ: 0.03+0.02+0.19=0.24 (sic.=4.084)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.46 (L/770) (sic.=2.567)

Asta n. 11 (111 11) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a compressione (4.2.4.1.2.2) - CC 9 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-600.55
Verifica a compressione [4.2.9]
N,Ed=-600.55 Nc,Rd=-52621.20 N,Ed/Nc,Rd=0.01 (sic.=87.622)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=71.89
V,Ed=71.89 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 94 SLU Xl=1.74 - Classe 1
Sollecitazioni: N=-221.07 M_y=-62.65
My,Ed=-62.65 My,c,Rd=3255.72
N,Ed=-221.07 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02 (sic.=51.968)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-600.55 My,Ed=-0.05 Mz,Ed=0.40 L=2.16
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.16 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=6347.05 λ_{LT}=0.69
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.73 β_{LT}=0.75 f=0.97 χ_{LT}=0.90
λ_y=32.84 Ncr,y=386179.00 λ^*_y=0.38 Curva a: Φ_y=0.59 χ_y=0.96
λ_z=117.14 Ncr,z=30347.70 λ^*_z=1.35 Curva b: Φ_z=1.61 χ_z=0.40
Kyy, Kyz, Kzy, Kzz=0.95, 0.97, 0.76, 0.97
Verifica YY: 0.01+0.00+0.00=0.01 (sic.=78.013)
Verifica ZZ: 0.03+0.00+0.00=0.03 (sic.=34.286)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.30 (L/712) (sic.=2.373)

Asta n. 11 (11 -22) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.66 - Classe 3
Sollecitazioni: N=-539.23 T_y=-7.80 M_z=-4.67
Tensioni: σ_N=-26.84 $\sigma_{m,d}$=-28.05 τ=0.00 σ_{max}=-54.88 (sic.=47.719)
Tensioni: σ_N=-26.84 $\sigma_{m,d}$=-7.87 τ=0.88 τ_{max}=0.88 (sic. >100)
Tensioni: σ_N=-26.84 $\sigma_{m,d}$=-28.05 τ=0.00 $\sigma_{ID,max}$=54.88 (sic.=47.719)

- Verifica a taglio Dir. Y [4.2.16] - CC 114 SLU Xl=0.66 - Classe 1
Sollecitazioni: T_y=-1.41
V,Ed=-1.41 Vc,Rd=20764.50 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=0.66 - Classe 1
Sollecitazioni: T_z=34.64
V,Ed=34.64 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 94 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-204.78 T_z=-18.17 M_y=-58.47
My,Ed=-58.47 My,V,c,Rd=3255.72
N,Ed=-204.78 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02 (sic.=55.685)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 114 SLU - Classe 1
Sollecitazioni: N,Ed=-241.47 My,Ed=58.46 Mz,Ed=-0.77 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95

L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.15 M,cr=27209.90 λ_{LT}=0.35
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=10.64 Ncr,y=3677050.00 λ^*_y=0.12 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=37.96 Ncr,z=288960.00 λ^*_z=0.44 Curva b: Φ_z=0.64 χ_z=0.91
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.02+0.00=0.02 (sic.=44.883)
Verifica ZZ: 0.01+0.01+0.00=0.02 (sic.=61.222)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.08 (L/814) (sic.=2.713)

Asta n. 11 (-22 211) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.04 - Classe 3
Sollecitazioni: N=-535.18 T_y=6.19 M_z=-4.64
Tensioni: σ_N=-26.64 $\sigma_{m,d}$=-27.83 τ=0.00 σ_{max}=-54.47 (sic.=48.085)
Tensioni: σ_N=-26.64 $\sigma_{m,d}$=-7.81 τ=0.70 τ_{max}=0.70 (sic. >100)
Tensioni: σ_N=-26.64 $\sigma_{m,d}$=-27.83 τ=0.00 $\sigma_{ID,max}$=54.47 (sic.=48.085)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=0.79 - Classe 1
Sollecitazioni: T_z=68.01
V,Ed=68.01 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 114 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-219.98 T_z=37.11 M_y=39.37
My,Ed=39.37 My,V,c,Rd=3255.72
N,Ed=-219.98 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.01
(sic.=82.685)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-535.18 My,Ed=0.02 Mz,Ed=-4.64 L=0.90
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.90 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=26080.30 λ_{LT}=0.34
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=13.68 Ncr,y=2224390.00 λ^*_y=0.16 Curva a: Φ_y=0.51 χ_y=1.00
λ_z=48.81 Ncr,z=174803.00 λ^*_z=0.56 Curva b: Φ_z=0.72 χ_z=0.86
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.01=0.02 (sic.=49.234)
Verifica ZZ: 0.01+0.01=0.02 (sic.=45.399)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.08 (L/949) (sic.=3.163)

Asta n. 12 (112 12) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a trazione (4.2.4.1.2.1) - CC 1 SND Xl=2.12 - Classe 3
Sollecitazioni: N=242.99
Verifica a trazione [4.2.5]
N,Ed=242.99 Npl,Rd=52621.20 Nu,Rd=62204.00 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 73 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=77.03
V,Ed=77.03 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 114 SLU Xl=1.74 - Classe 1
Sollecitazioni: N=-122.83 T_z=1.13 M_y=65.95
My,Ed=65.95 My,V,c,Rd=3255.72
N,Ed=-122.83 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02
(sic.=49.364)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 114 SLU - Classe 1
Sollecitazioni: N,Ed=-174.09 My,Ed=65.97 Mz,Ed=-0.09 L=2.16
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.16 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=6347.05 λ_{LT}=0.73
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.76 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
λ_y=32.84 Ncr,y=386179.00 λ^*_y=0.38 Curva a: Φ_y=0.59 χ_y=0.96
λ_z=117.14 Ncr,z=30347.70 λ^*_z=1.35 Curva b: Φ_z=1.61 χ_z=0.40
Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.57, 0.96
Verifica YY: 0.00+0.02+0.00=0.03 (sic.=39.291)
Verifica ZZ: 0.01+0.01+0.00=0.02 (sic.=46.572)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.31 (L/675) (sic.=2.250)

Asta n. 12 (12 -23) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.66 - Classe 3
Sollecitazioni: N=241.34 T_y=7.66 M_z=4.25
Tensioni: σ_N=12.01 $\sigma_{m,d}$=25.52 τ=0.00 σ_{max}=37.53 (sic.=69.777)

Tensioni: σ_N=12.01 $\sigma_{m,d}$=7.16 τ=0.87 τ_{max}=0.87 (sic. >100)
Tensioni: σ_N=12.01 $\sigma_{m,d}$=25.52 τ=0.00 $\sigma_{ID,max}$=37.53 (sic.=69.777)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=0.66 - Classe 1
Sollecitazioni: T_z=-40.07
V,Ed=-40.07 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 114 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-106.04 T_z=21.24 M_y=60.61 T_y=1.39
My,Ed=60.61 My,V,c,Rd=3255.72
N,Ed=-106.04 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02 (sic.=53.713)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 114 SLU - Classe 1
Sollecitazioni: N,Ed=-106.04 My,Ed=60.61 Mz,Ed=0.71 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=27711.80 λ_{LT}=0.35
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.64 Ncr,y=3677050.00 λ^*_y=0.12 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=37.96 Ncr,z=288960.00 λ^*_z=0.44 Curva b: Φ_z=0.64 χ_z=0.91
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.02+0.00=0.02 (sic.=49.291)
Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=72.444)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.08 (L/771) (sic.=2.570)

Asta n. 12 (-23 212) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.04 - Classe 3
Sollecitazioni: N=245.43 T_y=-6.34 M_z=4.21
Tensioni: σ_N=12.22 $\sigma_{m,d}$=25.24 τ=0.00 σ_{max}=37.46 (sic.=69.921)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=7.08 τ=0.72 τ_{max}=0.72 (sic. >100)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=25.24 τ=0.00 $\sigma_{ID,max}$=37.46 (sic.=69.921)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=0.70 - Classe 1
Sollecitazioni: T_z=-72.67
V,Ed=-72.67 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 94 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-65.98 T_z=-42.81 M_y=-38.31
My,Ed=-38.31 My,V,c,Rd=3255.72
N,Ed=-65.98 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.01 (sic.=84.984)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 114 SLU - Classe 1
Sollecitazioni: N,Ed=-84.02 My,Ed=38.30 Mz,Ed=0.60 L=0.90
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.90 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=26080.30 λ_{LT}=0.36
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=13.68 Ncr,y=2224390.00 λ^*_y=0.16 Curva a: Φ_y=0.51 χ_y=1.00
λ_Z=48.81 Ncr,z=174803.00 λ^*_z=0.56 Curva b: Φ_z=0.72 χ_z=0.86
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.00=0.01 (sic.=75.349)
Verifica ZZ: 0.00+0.01+0.00=0.01 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 213
δ=0.08 (L/847) (sic.=2.823)

Asta n. 13 (113 213) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a trazione (4.2.4.1.2.1) - CC 9 SND Xl=3.56 - Classe 3
Sollecitazioni: N=195.33
Verifica a trazione [4.2.5]
N,Ed=195.33 Npl,Rd=52621.20 Nu,Rd=62204.00 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=3.56 - Classe 1
Sollecitazioni: T_z=-106.80
V,Ed=-106.80 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=1.78 - Classe 1
Sollecitazioni: N=96.00 M_y=-95.05
My,Ed=-95.05 My,c,Rd=3255.72
N,Ed=96.00 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03 (sic.=34.252)

- Verifica di stabilità (4.2.4.1.3.1)
In tutte le CC risulta N < 0.04*N,cr e quindi non sono necessarie le verifiche di stabilità

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1

Sollecitazioni: N,Ed=-114.81 My,Ed=-95.05 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.00, 0.97
Verifica YY: 0.00+0.04=0.04 (sic.=23.330)
Verifica ZZ: 0.01=0.01 (sic.=71.806)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.44 (L/804) (sic.=2.680)

Asta n. 14 (114 214) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a compressione (4.2.4.1.2.2) - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-694.31
Verifica a compressione [4.2.9]
N,Ed=-694.31 Nc,Rd=-52621.20 N,Ed/Nc,Rd=0.01 (sic.=75.790)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=3.56 - Classe 1
Sollecitazioni: T_z=-106.80
V,Ed=-106.80 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=1.78 - Classe 1
Sollecitazioni: N=-124.42 M_y=-95.05
My,Ed=-95.05 My,c,Rd=3255.72
N,Ed=-124.42 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03 (sic.=34.252)

- Verifica di stabilità (4.2.4.1.3.1) - CC 80 SLU
Sollecitazioni: N=-1116.38
L=3.76
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66
Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35
Curva b: Φ_z=3.62 χ_z=0.16
χ,min=0.16 N,Ed=-1116.38 Nb,Rd=8243.74 N,Ed/Nb,Rd=0.14 (sic.=7.384)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 90 SLU - Classe 1
Sollecitazioni: N,Ed=-989.58 My,Ed=-57.03 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.96, 0.67, 0.00, 1.11
Verifica YY: 0.02+0.02=0.05 (sic.=21.680)
Verifica ZZ: 0.12=0.12 (sic.=8.331)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.37 (L/951) (sic.=3.170)

Asta n. 15 (15 115) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.83 - Classe 3
Sollecitazioni: N=-3693.58 T_z=-681.91 M_y=565.31 T_y=519.85 M_z=430.96 M_x=-5.27
Tensioni: σ_N=-47.30 $\sigma_{m,d}$=-314.36 τ=14.86 σ_{max}=-361.66 (sic.=7.242)
Tensioni: σ_N=-47.30 $\sigma_{m,d}$=-9.68 τ=47.71 τ_{max}=47.71 (sic.=31.692)
Tensioni: σ_N=-47.30 $\sigma_{m,d}$=-314.36 τ=14.86 $\sigma_{ID,max}$=362.57 (sic.=7.223)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 62 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=1580.66 M_x=-1.33
V,Ed=1580.66 Vc,Rd,Red=99738.00 V,Ed/Vc,Rd,Red=0.02 (sic.=63.099)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 62 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=-1918.78 M_x=-1.33
V,Ed=-1918.78 Vc,Rd,Red=37514.10 V,Ed/Vc,Rd,Red=0.05 (sic.=19.551)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 80 SLU Xl=0.83 - Classe 1
Sollecitazioni: N=-3945.52 T_z=-1591.45 M_y=1319.31 T_y=1708.64 M_z=1416.46 M_x=-2.38
N,Ed=-3945.52 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.02
Pressoflessione retta YY [4.2.33]:
My,Ed=1319.31 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.08 (sic.=12.796)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=1416.46 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.18 (sic.=5.660)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.18 (sic.=5.471)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 80 SLU - Classe 1
  Sollecitazioni: N,Ed=-4011.58 My,Ed=1319.31 Mz,Ed=1416.46 L=1.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=204556.00 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=23.42 Ncr,y=2951560.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_Z=39.48 Ncr,z=1038060.00 λ^*_z=0.45 Curva c: Φ_z=0.67 χ_z=0.87
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.96
  Verifica YY: 0.02+0.07+0.10=0.20 (sic.=5.105)
  Verifica ZZ: 0.02+0.04+0.17=0.24 (sic.=4.233)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 194
  δ=0.15 (L/563) (sic.=1.877)

Asta n. 15 (115 215) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=3.57 - Classe 3
  Sollecitazioni: N=-1204.08 T_z=-398.73 M_y=851.27 T_y=432.95 M_z=809.92 M_x=-1.42
  Tensioni: σ_N=-15.42 $\sigma_{m,d}$=-553.72 τ=4.02 σ_{max}=-569.14 (sic.=4.602)
  Tensioni: σ_N=-15.42 $\sigma_{m,d}$=-18.19 τ=26.71 τ_{max}=26.71 (sic.=56.609)
  Tensioni: σ_N=-15.42 $\sigma_{m,d}$=-553.72 τ=4.02 $\sigma_{ID,max}$=569.18 (sic.=4.601)

- Verifica a taglio Dir. Y [4.2.16] - CC 66 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=101.26
  V,Ed=101.26 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 66 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=-805.59
  V,Ed=-805.59 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=46.613)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 66 SLU Xl=3.57 - Classe 1
  Sollecitazioni: N=-2055.43 T_z=-698.51 M_y=1455.56 T_y=101.26 M_z=123.68
  N,Ed=-2055.43 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=1455.56 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.09 (sic.=11.598)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=123.68 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=64.822)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.09 (sic.=11.598)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-1450.09 My,Ed=851.27 Mz,Ed=809.92 L=3.76
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=7.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.59 M,cr=49304.20 λ_{LT}=0.56
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.65 β_{LT}=0.75 f=0.97 χ_{LT}=0.96
  λ_Y=88.04 Ncr,y=208773.00 λ^*_y=1.01 Curva b: Φ_y=1.15 χ_y=0.59
  λ_Z=148.46 Ncr,z=73425.20 λ^*_z=1.71 Curva c: Φ_z=2.33 χ_z=0.26
  Kyy, Kyz, Kzy, Kzz=0.96, 0.97, 0.77, 0.97
  Verifica YY: 0.01+0.06+0.15=0.22 (sic.=4.585)
  Verifica ZZ: 0.03+0.05+0.15=0.22 (sic.=4.496)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
  δ=0.30 (L/1207) (sic.=4.023)

Asta n. 16 (116 216) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a compressione (4.2.4.1.2.2) - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-1309.71
  Verifica a compressione [4.2.9]
  N,Ed=-1309.71 Nc,Rd=-52621.20 N,Ed/Nc,Rd=0.02 (sic.=40.178)

- Verifica a taglio Dir. Z [4.2.16] - CC 20 SLU Xl=3.56 - Classe 1
  Sollecitazioni: T_z=-96.79
  V,Ed=-96.79 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 20 SLU Xl=1.78 - Classe 1
  Sollecitazioni: N=-144.54 M_y=-86.14
  My,Ed=-86.14 My,c,Rd=3255.72
  N,Ed=-144.54 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03
(sic.=37.795)

- Verifica di stabilità (4.2.4.1.3.1) - CC 13 SND
  Sollecitazioni: N=-1309.71
  L=3.76
  λ_Y=57.16 Ncr,y=127444.00 λ^*_y=0.66
  Curva a: Φ_y=0.76 χ_y=0.87
  λ_Z=203.91 Ncr,z=10015.20 λ^*_z=2.35
  Curva b: Φ_z=3.62 χ_z=0.16

χ,min=0.16 N,Ed=-1309.71 Nb,Rd=8243.74 N,Ed/Nb,Rd=0.16 (sic.=6.294)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 32 SLU - Classe 1
  Sollecitazioni: N,Ed=-597.93 My,Ed=-51.68 L=3.76
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
  λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
  λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
  Kyy, Kyz, Kzy, Kzz=0.96, 0.63, 0.00, 1.05
  Verifica YY: 0.01+0.02=0.04 (sic.=28.442)
  Verifica ZZ: 0.07=0.07 (sic.=13.787)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
  δ=0.29 (L/1208) (sic.=4.027)

Asta n. 17 (117 17) - Sez. 14 (Montanti secondari_facciata vetrata) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.94 - Classe 3
  Sollecitazioni: N=565.27 T_y=-13.94 M_z=-13.11
  Tensioni: σ_N=16.62 $\sigma_{m,d}$=24.77 τ=0.00 σ_{max}=41.39 (sic.=63.280)
  Tensioni: σ_N=16.62 $\sigma_{m,d}$=-6.29 τ=0.74 τ_{max}=0.74 (sic. >100)
  Tensioni: σ_N=16.62 $\sigma_{m,d}$=24.77 τ=0.00 $\sigma_{ID,max}$=41.39 (sic.=63.280)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 31 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=25.66 M_x=3.34
  V,Ed=25.66 Vc,Rd,Red=43796.80 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 31 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=86.15 M_x=3.34
  V,Ed=86.15 Vc,Rd,Red=16443.40 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 47 SLU Xl=0.94 - Classe 1
  Sollecitazioni: N=750.13 T_y=-58.54 M_z=-55.03
  Mz,Ed=-55.03 Mz,V,c,Rd=2122.91
  N,Ed=750.13 Nc,Rd=89065.70 ZZ n=N,Ed/Nc,Rd=0.01 MNz,c,Rd=2122.91 Mz,Ed/MNz,c,Rd=0.03
(sic.=38.576)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 62 SLU - Classe 1
  Sollecitazioni: N,Ed=-112.47 My,Ed=-0.05 Mz,Ed=49.80 L=1.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=76924.90 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=19.83 Ncr,y=1791540.00 λ^*_y=0.23 Curva b: Φ_y=0.53 χ_y=0.99
  λ_z=32.73 Ncr,z=658102.00 λ^*_z=0.38 Curva c: Φ_z=0.61 χ_z=0.91
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.00+0.01=0.01 (sic.=68.210)
  Verifica ZZ: 0.00+0.02=0.02 (sic.=42.220)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 203
  δ=0.11 (L/829) (sic.=2.763)

Asta n. 17 (17 44) - Sez. 14 (Montanti secondari_facciata vetrata) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.30 - Classe 3
  Sollecitazioni: N=633.65 M_y=1.04 T_y=-102.75 M_z=-145.12
  Tensioni: σ_N=18.63 $\sigma_{m,d}$=274.93 τ=0.00 σ_{max}=293.57 (sic.=8.921)
  Tensioni: σ_N=18.63 $\sigma_{m,d}$=-68.98 τ=5.45 τ_{max}=5.45 (sic. >100)
  Tensioni: σ_N=18.63 $\sigma_{m,d}$=274.93 τ=0.00 $\sigma_{ID,max}$=293.57 (sic.=8.921)

- Verifica a taglio Dir. Y [4.2.16] - CC 66 SLU Xl=0.06 - Classe 1
  Sollecitazioni: T_y=122.73
  V,Ed=122.73 Vc,Rd=44150.20 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 66 SLU Xl=1.30 - Classe 1
  Sollecitazioni: N=289.50 T_y=122.73 M_z=142.66
  Mz,Ed=142.66 Mz,V,c,Rd=2122.91
  N,Ed=289.50 Nc,Rd=89065.70 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=2122.91 Mz,Ed/MNz,c,Rd=0.07
(sic.=14.881)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-133.42 My,Ed=-1.19 Mz,Ed=145.52 L=1.30
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.30 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=33823.60 λ_{LT}=0.34
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=25.79 Ncr,y=1060090.00 λ^*_y=0.30 Curva b: Φ_y=0.56 χ_y=0.97
  λ_z=42.54 Ncr,z=389410.00 λ^*_z=0.49 Curva c: Φ_z=0.69 χ_z=0.85
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.00+0.10=0.10 (sic.=9.838)

Verifica ZZ: 0.00+0.00+0.10=0.10 (sic.=9.823)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 203
  δ=0.11 (L/1118) (sic.=3.727)

Asta n. 18 (118 18) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=2.27 - Classe 3
  Sollecitazioni: N=656.48 T_z=-3.95 M_y=8.95 T_y=28.07 M_z=63.67
  Tensioni: σ_N=32.67 $\sigma_{m,d}$=390.35 τ=0.00 σ_{max}=423.02 (sic.=6.191)
  Tensioni: σ_N=32.67 $\sigma_{m,d}$=-99.70 τ=3.18 τ_{max}=3.18 (sic. >100)
  Tensioni: σ_N=32.67 $\sigma_{m,d}$=390.35 τ=0.00 $\sigma_{ID,max}$=423.02 (sic.=6.191)

- Verifica a taglio Dir. Y [4.2.16] - CC 51 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-18.61
  V,Ed=-18.61 Vc,Rd=20764.50 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 51 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=-81.15
  V,Ed=-81.15 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 66 SLU Xl=2.27 - Classe 1
  Sollecitazioni: N=505.91 T_z=-1.84 M_y=4.18 T_y=17.94 M_z=40.68
  N,Ed=505.91 Nc,Rd=52621.20 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=4.18 My,V,c,Rd=3255.72 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.00 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=40.68 Mz,V,c,Rd=684.55 MNz,c,Rd=684.55 Mz,Ed/MNz,c,Rd=0.06 (sic.=16.828)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.828)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
  δ=0.30 (L/749) (sic.=2.497)

Asta n. 18 (18 218) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=691.92 T_z=-8.60 M_y=-10.83 T_y=5.21 M_z=-6.57
  Tensioni: σ_N=34.44 $\sigma_{m,d}$=49.39 τ=0.00 σ_{max}=83.83 (sic.=31.242)
  Tensioni: σ_N=34.44 $\sigma_{m,d}$=2.40 τ=1.29 τ_{max}=1.29 (sic. >100)
  Tensioni: σ_N=34.44 $\sigma_{m,d}$=49.39 τ=0.00 $\sigma_{ID,max}$=83.83 (sic.=31.242)

- Verifica a taglio Dir. Y [4.2.16] - CC 84 SLU Xl=1.26 - Classe 1
  Sollecitazioni: T_y=-1.75
  V,Ed=-1.75 Vc,Rd=20764.50 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 84 SLU Xl=1.26 - Classe 1
  Sollecitazioni: T_z=-106.91
  V,Ed=-106.91 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 84 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=808.11 T_z=-50.67 M_y=-94.53 T_y=-1.75 M_z=2.20
  N,Ed=808.11 Nc,Rd=52621.20 n=N,Ed/Nc,Rd=0.02
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-94.53 My,V,c,Rd=3255.72 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03 (sic.=34.440)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=2.20 Mz,V,c,Rd=684.55 MNz,c,Rd=684.55 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=34.440)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 183
  δ=0.15 (L/853) (sic.=2.843)

Asta n. 19 (119 19) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a compressione (4.2.4.1.2.2) - CC 9 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-55.76
  Verifica a compressione [4.2.9]
  N,Ed=-55.76 Nc,Rd=-52621.20 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 20 SLU Xl=2.25 - Classe 1
  Sollecitazioni: T_y=-2.98
  V,Ed=-2.98 Vc,Rd=20764.50 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 20 SLU Xl=2.25 - Classe 1
  Sollecitazioni: T_z=-44.79
  V,Ed=-44.79 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 20 SLU Xl=1.13 - Classe 1
  Sollecitazioni: N=-62.96 M_y=-25.20 M_z=1.68

N,Ed=-62.96 Nc,Rd=52621.20 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-25.20 My,c,Rd=3255.72 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=1.68 Mz,c,Rd=684.55 MNz,c,Rd=684.55 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^{2}+(Mz,Ed/MNz,c,Rd)^{1}$=0.01 (sic. >100)

- Verifica di stabilità (4.2.4.1.3.1)
In tutte le CC risulta N < 0.04*N,cr e quindi non sono necessarie le verifiche di stabilità

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 36 SLU - Classe 1
Sollecitazioni: N,Ed=-96.73 My,Ed=-25.20 Mz,Ed=1.68 L=2.30
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.30 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=5816.22 λ_{LT}=0.77
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.78 β_{LT}=0.75 f=0.97 χ_{LT}=0.86
λ_y=34.97 Ncr,y=340597.00 λ^*_y=0.40 Curva a: Φ_y=0.60 χ_y=0.95
λ_z=124.73 Ncr,z=26765.70 λ^*_z=1.44 Curva b: Φ_z=1.74 χ_z=0.37
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.96
Verifica YY: 0.00+0.01+0.00=0.01 (sic.=84.155)
Verifica ZZ: 0.01+0.01+0.00=0.01 (sic.=80.081)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.33 (L/692) (sic.=2.307)

Asta n. 20 (20 220) - Sez. 14 (Montanti secondari_facciata vetrata) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=548.67 T_y=-206.05 M_z=259.63
Tensioni: σ_N=16.13 $\sigma_{m,d}$=490.60 τ=0.00 σ_{max}=506.73 (sic.=5.168)
Tensioni: σ_N=16.13 $\sigma_{m,d}$=124.69 τ=10.93 τ_{max}=10.93 (sic. >100)
Tensioni: σ_N=16.13 $\sigma_{m,d}$=490.60 τ=0.00 $\sigma_{ID,max}$=506.73 (sic.=5.168)

- Verifica a taglio Dir. Y [4.2.16] - CC 36 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=1.13
V,Ed=1.13 Vc,Rd=44150.20 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 36 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=-108.73
V,Ed=-108.73 Vc,Rd=16576.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 94 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=1167.72 T_y=-165.59 M_z=208.64
Mz,Ed=208.64 Mz,V,c,Rd=2122.91
N,Ed=1167.72 Nc,Rd=89065.70 ZZ n=N,Ed/Nc,Rd=0.01 MNz,c,Rd=2122.91 Mz,Ed/MNz,c,Rd=0.10 (sic.=10.175)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.09 (L/1462) (sic.=4.873)

Asta n. 21 (21 221) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.05 - Classe 3
Sollecitazioni: N=-106.31 T_z=14.32 M_y=7.31 T_y=-60.49 M_z=30.88
Tensioni: σ_N=-5.29 $\sigma_{m,d}$=-192.05 τ=0.00 σ_{max}=-197.34 (sic.=13.271)
Tensioni: σ_N=-5.29 $\sigma_{m,d}$=-45.88 τ=6.86 τ_{max}=6.86 (sic. >100)
Tensioni: σ_N=-5.29 $\sigma_{m,d}$=-192.05 τ=0.00 $\sigma_{ID,max}$=197.34 (sic.=13.271)

- Verifica a taglio Dir. Y [4.2.16] - CC 84 SLU Xl=0.05 - Classe 1
Sollecitazioni: T_y=-91.67
V,Ed=-91.67 Vc,Rd=20764.50 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 84 SLU Xl=0.05 - Classe 1
Sollecitazioni: T_z=12.64
V,Ed=12.64 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 84 SLU Xl=0.05 - Classe 1
Sollecitazioni: N=-254.71 T_z=12.64 T_y=-91.67 M_z=46.80
Mz,Ed=46.80 Mz,V,c,Rd=684.55
N,Ed=-254.71 Nc,Rd=-52621.20 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=684.55 Mz,Ed/MNz,c,Rd=0.07 (sic.=14.629)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-106.31 My,Ed=7.31 Mz,Ed=30.88 L=0.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=35494.20 λ_{LT}=0.29
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=11.55 Ncr,y=3119380.00 λ^*_y=0.13 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=41.22 Ncr,z=245136.00 λ^*_z=0.47 Curva b: Φ_z=0.66 χ_z=0.90
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.00+0.07=0.07 (sic.=13.942)
Verifica ZZ: 0.00+0.00+0.07=0.07 (sic.=13.991)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 178
δ=0.16 (L/329) (sic.=1.097)

Asta n. 22 (122 22) - Sez. 14 (Montanti secondari_facciata vetrata) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.94 - Classe 3
Sollecitazioni: N=564.68 T_y=13.69 M_z=12.87
Tensioni: σ_N=16.60 $\sigma_{m,d}$=24.32 τ=0.00 σ_{max}=40.92 (sic.=63.997)
Tensioni: σ_N=16.60 $\sigma_{m,d}$=6.18 τ=0.73 τ_{max}=0.73 (sic. >100)
Tensioni: σ_N=16.60 $\sigma_{m,d}$=24.32 τ=0.00 $\sigma_{ID,max}$=40.92 (sic.=63.997)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 104 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=30.17 M_x=3.34
V,Ed=30.17 Vc,Rd,Red=43796.70 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 104 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=-86.28 M_x=3.34
V,Ed=-86.28 Vc,Rd,Red=16443.40 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 67 SLU Xl=0.94 - Classe 1
Sollecitazioni: N=754.52 T_y=57.17 M_z=53.74
Mz,Ed=53.74 Mz,V,c,Rd=2122.91
N,Ed=754.52 Nc,Rd=89065.70 ZZ n=N,Ed/Nc,Rd=0.01 MNz,c,Rd=2122.91 Mz,Ed/MNz,c,Rd=0.03
(sic.=39.507)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 90 SLU - Classe 1
Sollecitazioni: N,Ed=-108.71 My,Ed=0.04 Mz,Ed=-48.97 L=1.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=76924.90 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=19.83 Ncr,y=1791540.00 λ^*_y=0.23 Curva b: Φ_y=0.53 χ_y=0.99
λ_z=32.73 Ncr,z=658102.00 λ^*_z=0.38 Curva c: Φ_z=0.61 χ_z=0.91
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01=0.01 (sic.=69.479)
Verifica ZZ: 0.00+0.02=0.02 (sic.=42.980)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 203
δ=0.11 (L/829) (sic.=2.763)

Asta n. 22 (22 47) - Sez. 14 (Montanti secondari_facciata vetrata) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.30 - Classe 3
Sollecitazioni: N=633.06 M_y=1.24 T_y=102.79 M_z=144.89
Tensioni: σ_N=18.62 $\sigma_{m,d}$=274.65 τ=0.00 σ_{max}=293.27 (sic.=8.931)
Tensioni: σ_N=18.62 $\sigma_{m,d}$=70.45 τ=5.45 τ_{max}=5.45 (sic. >100)
Tensioni: σ_N=18.62 $\sigma_{m,d}$=274.65 τ=0.00 $\sigma_{ID,max}$=293.27 (sic.=8.931)

- Verifica a taglio Dir. Y [4.2.16] - CC 94 SLU Xl=0.06 - Classe 1
Sollecitazioni: T_y=-126.25
V,Ed=-126.25 Vc,Rd=44150.20 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 94 SLU Xl=1.30 - Classe 1
Sollecitazioni: N=276.12 T_y=-126.25 M_z=-146.94
Mz,Ed=-146.94 Mz,V,c,Rd=2122.91
N,Ed=276.12 Nc,Rd=89065.70 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=2122.91 Mz,Ed/MNz,c,Rd=0.07
(sic.=14.447)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-134.55 My,Ed=-1.09 Mz,Ed=-146.03 L=1.30
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.30 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.15 M,cr=33333.30 λ_{LT}=0.34
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=25.79 Ncr,y=1060090.00 λ^*_y=0.30 Curva b: Φ_y=0.56 χ_y=0.97
λ_z=42.54 Ncr,z=389410.00 λ^*_z=0.49 Curva c: Φ_z=0.69 χ_z=0.85
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.00+0.10=0.10 (sic.=9.806)
Verifica ZZ: 0.00+0.00+0.10=0.10 (sic.=9.790)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 203
δ=0.11 (L/1114) (sic.=3.713)

Asta n. 23 (123 23) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=2.27 - Classe 3
Sollecitazioni: N=651.10 T_z=-4.76 M_y=10.80 T_y=-29.05 M_z=-65.88

Tensioni: σ_N=32.41 $\sigma_{m,d}$=405.35 τ=0.00 σ_{max}=437.76 (sic.=5.983)
Tensioni: σ_N=32.41 $\sigma_{m,d}$=119.93 τ=3.29 τ_{max}=3.29 (sic. >100)
Tensioni: σ_N=32.41 $\sigma_{m,d}$=405.35 τ=0.00 $\sigma_{ID,max}$=437.76 (sic.=5.983)

- Verifica a taglio Dir. Y [4.2.16] - CC 99 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-24.61
V,Ed=-24.61 Vc,Rd=20764.50 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 99 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=-61.56
V,Ed=-61.56 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=2.27 - Classe 1
Sollecitazioni: N=468.25 T_z=-3.06 M_y=6.95 T_y=-20.28 M_z=-46.00
N,Ed=468.25 Nc,Rd=52621.20 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=6.95 My,V,c,Rd=3255.72 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.00 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-46.00 Mz,V,c,Rd=684.55 MNz,c,Rd=684.55 Mz,Ed/MNz,c,Rd=0.07 (sic.=14.882)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.07 (sic.=14.880)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.32 (L/704) (sic.=2.347)

Asta n. 23 (23 223) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=684.96 T_z=-10.97 M_y=-13.82 T_y=-5.18 M_z=6.53
Tensioni: σ_N=34.09 $\sigma_{m,d}$=51.90 τ=0.00 σ_{max}=86.00 (sic.=30.456)
Tensioni: σ_N=34.09 $\sigma_{m,d}$=-2.39 τ=1.64 τ_{max}=1.64 (sic. >100)
Tensioni: σ_N=34.09 $\sigma_{m,d}$=51.90 τ=0.00 $\sigma_{ID,max}$=86.00 (sic.=30.456)

- Verifica a taglio Dir. Y [4.2.16] - CC 84 SLU Xl=1.26 - Classe 1
Sollecitazioni: T_y=-10.22
V,Ed=-10.22 Vc,Rd=20764.50 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 84 SLU Xl=1.26 - Classe 1
Sollecitazioni: T_z=-112.31
V,Ed=-112.31 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 84 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=950.36 T_z=-56.08 M_y=-101.35 T_y=-10.22 M_z=12.87
N,Ed=950.36 Nc,Rd=52621.20 n=N,Ed/Nc,Rd=0.02
Pressoflessione retta YY [4.2.33]:
My,Ed=-101.35 My,V,c,Rd=3255.72 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03 (sic.=32.125)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=12.87 Mz,V,c,Rd=684.55 MNz,c,Rd=684.55 Mz,Ed/MNz,c,Rd=0.02 (sic.=53.184)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=32.125)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 183
δ=0.15 (L/832) (sic.=2.773)

Asta n. 24 (124 224) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica a compressione (4.2.4.1.2.2) - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-1354.73
Verifica a compressione [4.2.9]
N,Ed=-1354.73 Nc,Rd=-52621.20 N,Ed/Nc,Rd=0.03 (sic.=38.843)

- Verifica a taglio Dir. Z [4.2.16] - CC 20 SLU Xl=3.56 - Classe 1
Sollecitazioni: T_z=-96.79
V,Ed=-96.79 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 20 SLU Xl=1.78 - Classe 1
Sollecitazioni: N=31.54 M_y=-86.14
My,Ed=-86.14 My,c,Rd=3255.72
N,Ed=31.54 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.03 (sic.=37.795)

- Verifica di stabilità (4.2.4.1.3.1) - CC 5 SND
Sollecitazioni: N=-1354.73
L=3.76
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66
Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35
Curva b: Φ_z=3.62 χ_z=0.16
χ,min=0.16 N,Ed=-1354.73 Nb,Rd=8243.74 N,Ed/Nb,Rd=0.16 (sic.=6.085)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 100 SLU - Classe 1

Sollecitazioni: N,Ed=-753.49 My,Ed=51.68 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.96, 0.64, 0.00, 1.07
Verifica YY: 0.02+0.02=0.04 (sic.=25.903)
Verifica ZZ: 0.09=0.09 (sic.=10.941)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.30 (L/1167) (sic.=3.890)

Asta n. 25 (25 125) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.83 - Classe 3
Sollecitazioni: N=-3266.85 T_z=540.29 M_y=-447.90 T_y=352.57 M_z=292.28 M_x=-5.06
Tensioni: σ_N=-41.84 $\sigma_{m,d}$=-224.52 τ=14.28 σ_{max}=-266.36 (sic.=9.833)
Tensioni: σ_N=-41.84 $\sigma_{m,d}$=-6.57 τ=38.67 τ_{max}=38.67 (sic.=39.107)
Tensioni: σ_N=-41.84 $\sigma_{m,d}$=-224.52 τ=14.28 $\sigma_{ID,max}$=267.51 (sic.=9.791)

- Verifica a taglio Dir. Y [4.2.16] - CC 90 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-1205.15
V,Ed=-1205.15 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.01 (sic.=82.842)

- Verifica a taglio Dir. Z [4.2.16] - CC 90 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=1752.33
V,Ed=1752.33 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.05 (sic.=21.429)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 85 SLU Xl=0.83 - Classe 1
Sollecitazioni: N=-1917.20 T_z=-582.28 M_y=482.71 T_y=1302.29 M_z=1079.59 M_x=1.76
N,Ed=-1917.20 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=482.71 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=34.973)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=1079.59 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.13 (sic.=7.426)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.14 (sic.=7.381)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 90 SLU - Classe 1
Sollecitazioni: N,Ed=-3586.81 My,Ed=-1452.68 Mz,Ed=-999.07 L=1.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=204556.00 λ_{LT}=0.29
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=23.42 Ncr,y=2951560.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_z=39.48 Ncr,z=1038060.00 λ^*_z=0.45 Curva c: Φ_z=0.67 χ_z=0.87
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.96
Verifica YY: 0.02+0.08+0.07=0.17 (sic.=5.837)
Verifica ZZ: 0.02+0.05+0.12=0.19 (sic.=5.307)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 166
δ=0.14 (L/587) (sic.=1.957)

Asta n. 25 (125 -14) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-1721.55 T_z=169.01 M_y=247.40 T_y=-597.51 M_z=931.54 M_x=1.61
Tensioni: σ_N=-22.05 $\sigma_{m,d}$=-508.42 τ=4.55 σ_{max}=-530.46 (sic.=4.937)
Tensioni: σ_N=-22.05 $\sigma_{m,d}$=8.17 τ=15.48 τ_{max}=15.48 (sic.=97.693)
Tensioni: σ_N=-22.05 $\sigma_{m,d}$=-508.42 τ=4.55 $\sigma_{ID,max}$=530.52 (sic.=4.937)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 94 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-188.80 M_x=6.42
V,Ed=-188.80 Vc,Rd,Red=99357.40 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 94 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=768.93 M_x=6.42
V,Ed=768.93 Vc,Rd,Red=37371.00 V,Ed/Vc,Rd,Red=0.02 (sic.=48.601)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 105 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-1993.33 T_z=532.61 M_y=971.45 T_y=-416.63 M_z=737.10 M_x=-4.31
N,Ed=-1993.33 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=971.45 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=17.378)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=737.10 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.09 (sic.=10.876)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.10 (sic.=10.498)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-1721.55 My,Ed=247.40 Mz,Ed=931.54 L=0.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=474636.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=11.71 Ncr,y=11806200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_z=19.74 Ncr,z=4152220.00 λ^*_z=0.23 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.02+0.17=0.19 (sic.=5.180)
  Verifica ZZ: 0.01+0.01+0.17=0.19 (sic.=5.263)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 165
  δ=0.04 (L/1068) (sic.=3.560)

Asta n. 25 (-14 -16) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-1668.41 T_z=169.01 M_y=158.98 T_y=-480.78 M_z=617.46 M_x=1.61
  Tensioni: σ_N=-21.37 $\sigma_{m,d}$=-336.12 τ=4.55 σ_{max}=-357.49 (sic.=7.326)
  Tensioni: σ_N=-21.37 $\sigma_{m,d}$=4.83 τ=14.51 τ_{max}=14.51 (sic. >100)
  Tensioni: σ_N=-21.37 $\sigma_{m,d}$=-336.12 τ=4.55 $\sigma_{ID,max}$=357.57 (sic.=7.325)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 95 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-197.78 M_x=1.35
  V,Ed=-197.78 Vc,Rd,Red=99736.50 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 95 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=730.38 M_x=1.35
  V,Ed=730.38 Vc,Rd,Red=37513.60 V,Ed/Vc,Rd,Red=0.02 (sic.=51.361)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 105 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-1923.13 T_z=532.61 M_y=685.69 T_y=-343.41 M_z=518.88 M_x=-4.31
  N,Ed=-1923.13 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=685.69 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.04 (sic.=24.620)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=518.88 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.06 (sic.=15.450)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.07 (sic.=15.066)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-1668.41 My,Ed=158.98 Mz,Ed=617.46 L=0.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.20 M,cr=489151.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=11.71 Ncr,y=11806200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_z=19.74 Ncr,z=4152220.00 λ^*_z=0.23 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.01+0.11=0.13 (sic.=7.680)
  Verifica ZZ: 0.01+0.01+0.11=0.13 (sic.=7.794)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 198
  δ=0.04 (L/1022) (sic.=3.407)

Asta n. 25 (-16 225) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=2.57 - Classe 3
  Sollecitazioni: N=-1491.85 T_z=246.29 M_y=-569.29 T_y=496.38 M_z=933.79 M_x=-1.51
  Tensioni: σ_N=-19.11 $\sigma_{m,d}$=-566.05 τ=4.25 σ_{max}=-585.16 (sic.=4.476)
  Tensioni: σ_N=-19.11 $\sigma_{m,d}$=-87.94 τ=18.16 τ_{max}=18.16 (sic.=83.285)
  Tensioni: σ_N=-19.11 $\sigma_{m,d}$=-566.05 τ=4.25 $\sigma_{ID,max}$=585.20 (sic.=4.475)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-157.03 M_x=-1.10
  V,Ed=-157.03 Vc,Rd,Red=99755.10 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=544.96 M_x=-1.10
  V,Ed=544.96 Vc,Rd,Red=37520.60 V,Ed/Vc,Rd,Red=0.01 (sic.=68.851)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=2.57 - Classe 1
  Sollecitazioni: N=-1765.11 T_z=544.96 M_y=-1150.34 T_y=-157.03 M_z=-181.84 M_x=-1.10
  N,Ed=-1765.11 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-1150.34 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.07 (sic.=14.676)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-181.84 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=44.088)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.07 (sic.=14.676)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-1647.11 My,Ed=-569.29 Mz,Ed=933.79 L=2.76
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=5.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.91 M,cr=52069.20 λ_{LT}=0.55
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.64 β_{LT}=0.75 f=0.97 χ_{LT}=0.97
  λ_y=64.63 Ncr,y=387465.00 λ^*_y=0.74 Curva b: Φ_y=0.87 χ_y=0.76
  λ_z=108.98 Ncr,z=136271.00 λ^*_z=1.26 Curva c: Φ_z=1.55 χ_z=0.41
  Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.01+0.04+0.17=0.22 (sic.=4.557)
  Verifica ZZ: 0.02+0.03+0.17=0.22 (sic.=4.525)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 203
  δ=0.20 (L/1271) (sic.=4.237)

Asta n. 26 (26 226) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a trazione (4.2.4.1.2.1) - CC 1 SND Xl=2.56 - Classe 3
  Sollecitazioni: N=160.39
  Verifica a trazione [4.2.5]
  N,Ed=160.39 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=2.56 - Classe 1
  Sollecitazioni: T_z=28.39
  V,Ed=28.39 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 85 SLU Xl=2.56 - Classe 1
  Sollecitazioni: N=352.96
  Verifica a trazione [4.2.5]
  N,Ed=352.96 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.01 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 203
  δ=0.20 (L/1241) (sic.=4.137)

Asta n. 27 (127 27) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.46 - Classe 3
  Sollecitazioni: N=97.10 T_y=56.88 M_z=26.36
  Tensioni: σ_N=5.91 $\sigma_{m,d}$=214.23 τ=0.00 σ_{max}=220.14 (sic.=11.897)
  Tensioni: σ_N=5.91 $\sigma_{m,d}$=54.88 τ=7.88 τ_{max}=7.88 (sic. >100)
  Tensioni: σ_N=5.91 $\sigma_{m,d}$=214.23 τ=0.00 $\sigma_{ID,max}$=220.14 (sic.=11.897)

- Verifica a taglio Dir. Y [4.2.16] - CC 94 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=19.68
  V,Ed=19.68 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=26.59
  V,Ed=26.59 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 104 SLU Xl=0.46 - Classe 1
  Sollecitazioni: N=218.46 T_y=38.18 M_z=17.70
  Mz,Ed=17.70 Mz,V,c,Rd=504.58
  N,Ed=218.46 Nc,Rd=43021.20 ZZ n=N,Ed/Nc,Rd=0.01 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.04 (sic.=28.510)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 32 SLU - Classe 1
  Sollecitazioni: N,Ed=-75.00 My,Ed=0.01 Mz,Ed=-11.80 L=0.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=45540.00 λ_{LT}=0.23
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=8.71 Ncr,y=4487080.00 λ^*_y=0.10 Curva a: Φ_y=0.49 χ_y=1.00
  λ_z=30.24 Ncr,z=372390.00 λ^*_z=0.35 Curva b: Φ_z=0.59 χ_z=0.95
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01=0.02 (sic.=66.302)
  Verifica ZZ: 0.00+0.02=0.02 (sic.=41.543)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 188
  δ=0.07 (L/679) (sic.=2.263)

Asta n. 27 (27 -17) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=117.30 T_y=-59.88 M_z=25.57
  Tensioni: σ_N=7.14 $\sigma_{m,d}$=207.76 τ=0.00 σ_{max}=214.90 (sic.=12.187)
  Tensioni: σ_N=7.14 $\sigma_{m,d}$=53.22 τ=8.30 τ_{max}=8.30 (sic. >100)
  Tensioni: σ_N=7.14 $\sigma_{m,d}$=207.76 τ=0.00 $\sigma_{ID,max}$=214.90 (sic.=12.187)

- Verifica a taglio Dir. Y [4.2.16] - CC 114 SLU Xl=0.46 - Classe 1
  Sollecitazioni: T_y=-11.92

V,Ed=-11.92 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=0.46 - Classe 1
  Sollecitazioni: T_z=27.95
  V,Ed=27.95 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 104 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=245.82 T_y=-39.19 M_z=16.73
  Mz,Ed=16.73 Mz,V,c,Rd=504.58
  N,Ed=245.82 Nc,Rd=43021.20 ZZ n=N,Ed/Nc,Rd=0.01 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.03 (sic.=30.157)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 32 SLU - Classe 1
  Sollecitazioni: N,Ed=-38.48 My,Ed=-0.01 Mz,Ed=-12.59 L=0.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=45540.00 λ_{LT}=0.23
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=8.71 Ncr,y=4487080.00 λ^*_y=0.10 Curva a: Φ_y=0.49 χ_y=1.00
  λ_z=30.24 Ncr,z=372390.00 λ^*_z=0.35 Curva b: Φ_z=0.59 χ_z=0.95
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01=0.02 (sic.=66.150)
  Verifica ZZ: 0.00+0.02=0.02 (sic.=40.572)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 188
  δ=0.07 (L/653) (sic.=2.177)

Asta n. 28 (128 28) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.96 - Classe 3
  Sollecitazioni: N=613.24 T_y=6.16 M_z=5.94
  Tensioni: σ_N=30.52 $\sigma_{m,d}$=35.63 τ=0.00 σ_{max}=66.16 (sic.=39.589)
  Tensioni: σ_N=30.52 $\sigma_{m,d}$=9.99 τ=0.70 τ_{max}=0.70 (sic. >100)
  Tensioni: σ_N=30.52 $\sigma_{m,d}$=35.63 τ=0.00 $\sigma_{ID,max}$=66.16 (sic.=39.589)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 114 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=8.93 M_x=1.85
  V,Ed=8.93 Vc,Rd,Red=20527.60 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 114 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=-79.23 M_x=1.85
  V,Ed=-79.23 Vc,Rd,Red=14437.40 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 114 SLU Xl=0.96 - Classe 1
  Sollecitazioni: N=105.50 T_z=-64.78 M_y=69.38 T_y=8.93 M_z=8.60 M_x=1.85
  N,Ed=105.50 Nc,Rd=52621.20 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=69.38 My,V,c,Rd=3255.72 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02 (sic.=46.927)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=8.60 Mz,V,c,Rd=684.55 MNz,c,Rd=684.55 Mz,Ed/MNz,c,Rd=0.01 (sic.=79.562)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=46.927)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-510.08 My,Ed=-0.01 Mz,Ed=5.62 L=1.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=21621.50 λ_{LT}=0.37
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=15.20 Ncr,y=1801760.00 λ^*_y=0.18 Curva a: Φ_y=0.51 χ_y=1.00
  λ_z=54.23 Ncr,z=141590.00 λ^*_z=0.62 Curva b: Φ_z=0.77 χ_z=0.82
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.01=0.02 (sic.=45.496)
  Verifica ZZ: 0.01+0.01=0.02 (sic.=41.593)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 188
  δ=0.12 (L/807) (sic.=2.690)

Asta n. 28 (28 228) - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=629.51 T_y=-2.12 M_z=5.34
  Tensioni: σ_N=31.33 $\sigma_{m,d}$=32.06 τ=0.00 σ_{max}=63.39 (sic.=41.316)
  Tensioni: σ_N=31.33 $\sigma_{m,d}$=8.99 τ=0.24 τ_{max}=0.24 (sic. >100)
  Tensioni: σ_N=31.33 $\sigma_{m,d}$=32.06 τ=0.00 $\sigma_{ID,max}$=63.39 (sic.=41.316)

- Verifica a taglio Dir. Y [4.2.16] - CC 114 SLU Xl=2.56 - Classe 1
  Sollecitazioni: T_y=-2.25
  V,Ed=-2.25 Vc,Rd=20764.50 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=2.56 - Classe 1
  Sollecitazioni: T_z=56.79
  V,Ed=56.79 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 114 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=184.94 M_y=71.67 T_y=-2.25 M_z=5.68
  N,Ed=184.94 Nc,Rd=52621.20 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=71.67 My,c,Rd=3255.72 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.02 (sic.=45.428)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=5.68 Mz,V,c,Rd=684.55 MNz,c,Rd=684.55 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.02 (sic.=45.428)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-457.42 My,Ed=-0.03 Mz,Ed=4.98 L=2.76
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4560.06 λ_{LT}=0.81
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.82 β_{LT}=0.75 f=0.97 χ_{LT}=0.84
  λ_y=41.96 Ncr,y=236525.00 λ^*_y=0.48 Curva a: Φ_y=0.65 χ_y=0.93
  λ_z=149.68 Ncr,z=18587.30 λ^*_z=1.72 Curva b: Φ_z=2.25 χ_z=0.27
  Kyy, Kyz, Kzy, Kzz=0.95, 0.97, 0.76, 0.97
  Verifica YY: 0.01+0.00+0.01=0.02 (sic.=48.987)
  Verifica ZZ: 0.03+0.01=0.04 (sic.=23.212)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
  δ=0.22 (L/1170) (sic.=3.900)

Asta n. 29 (29 129) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.83 - Classe 3
  Sollecitazioni: N=-4677.14 T_z=1075.50 M_y=-891.59 T_y=-1073.34 M_z=-889.80
  Tensioni: σ_N=-59.90 $\sigma_{m,d}$=-600.67 τ=0.00 σ_{max}=-660.57 (sic.=3.965)
  Tensioni: σ_N=-59.90 $\sigma_{m,d}$=19.99 τ=70.53 τ_{max}=70.53 (sic.=21.441)
  Tensioni: σ_N=-59.90 $\sigma_{m,d}$=-600.67 τ=0.00 $\sigma_{ID,max}$=660.57 (sic.=3.965)

- Verifica a taglio Dir. Y [4.2.16] - CC 86 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-741.83
  V,Ed=-741.83 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 86 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=2804.82
  V,Ed=2804.82 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.07 (sic.=13.388)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 100 SLU Xl=0.83 - Classe 1
  Sollecitazioni: N=-5242.12 T_z=2260.67 M_y=-1874.09 T_y=-1280.24 M_z=-1061.32
  N,Ed=-5242.12 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.03
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-1874.09 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.11 (sic.=9.008)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-1061.32 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.13 (sic.=7.554)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.14 (sic.=6.910)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-4727.95 My,Ed=-891.59 Mz,Ed=-889.80 L=1.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=204556.00 λ_{LT}=0.28
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.42 Ncr,y=2951560.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_z=39.48 Ncr,z=1038060.00 λ^*_z=0.45 Curva c: Φ_z=0.67 χ_z=0.87
  Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.02+0.06+0.16=0.24 (sic.=4.116)
  Verifica ZZ: 0.03+0.05+0.16=0.23 (sic.=4.264)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 165
  δ=0.15 (L/564) (sic.=1.880)

Asta n. 29 (129 -18) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-1500.19 T_z=269.94 M_y=466.79 T_y=599.95 M_z=1030.54
  Tensioni: σ_N=-19.21 $\sigma_{m,d}$=-596.35 τ=0.00 σ_{max}=-615.56 (sic.=4.255)
  Tensioni: σ_N=-19.21 $\sigma_{m,d}$=31.76 τ=18.00 τ_{max}=18.00 (sic.=83.997)
  Tensioni: σ_N=-19.21 $\sigma_{m,d}$=-596.35 τ=0.00 $\sigma_{ID,max}$=615.56 (sic.=4.255)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 94 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-106.95 M_x=13.33
  V,Ed=-106.95 Vc,Rd,Red=98838.90 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 94 SLU Xl=0.00 - Classe 1

Sollecitazioni: T_z=908.72 M_x=13.33
V,Ed=908.72 Vc,Rd,Red=37175.90 V,Ed/Vc,Rd,Red=0.02 (sic.=40.910)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 95 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-2205.47 T_z=797.15 M_y=1445.64 T_y=-209.96 M_z=376.18 M_x=8.08
N,Ed=-2205.47 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=1445.64 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.09 (sic.=11.678)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=376.18 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.05 (sic.=21.311)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.09 (sic.=11.678)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-1500.19 My,Ed=466.79 Mz,Ed=1030.54 L=1.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.30 M,cr=66786.00 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_y=39.81 Ncr,y=1021300.00 λ^*_y=0.46 Curva b: Φ_y=0.65 χ_y=0.90
λ_z=67.12 Ncr,z=359189.00 λ^*_z=0.77 Curva c: Φ_z=0.94 χ_z=0.68
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.03+0.19=0.23 (sic.=4.430)
Verifica ZZ: 0.01+0.02+0.19=0.22 (sic.=4.497)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 165
δ=0.20 (L/803) (sic.=2.677)

Asta n. 29 (-18 229) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.87 - Classe 3
Sollecitazioni: N=-1737.97 T_z=269.94 M_y=-504.85 T_y=-853.65 M_z=-1401.76
Tensioni: σ_N=-22.26 $\sigma_{m,d}$=-788.33 τ=0.00 σ_{max}=-810.59 (sic.=3.231)
Tensioni: σ_N=-22.26 $\sigma_{m,d}$=82.10 τ=20.44 τ_{max}=20.44 (sic.=73.989)
Tensioni: σ_N=-22.26 $\sigma_{m,d}$=-788.33 τ=0.00 $\sigma_{ID,max}$=810.59 (sic.=3.231)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 94 SLU Xl=0.07 - Classe 1
Sollecitazioni: T_y=-299.89 M_x=-10.48
V,Ed=-299.89 Vc,Rd,Red=99052.80 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 94 SLU Xl=0.07 - Classe 1
Sollecitazioni: T_z=644.01 M_x=-10.48
V,Ed=644.01 Vc,Rd,Red=37256.40 V,Ed/Vc,Rd,Red=0.02 (sic.=57.850)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 99 SLU Xl=1.87 - Classe 1
Sollecitazioni: N=-1598.01 T_z=140.82 M_y=-286.18 T_y=-687.72 M_z=-973.32
N,Ed=-1598.01 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-286.18 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=58.991)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-973.32 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.12 (sic.=8.237)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.12 (sic.=8.217)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-1851.86 My,Ed=-504.85 Mz,Ed=-1401.76 L=2.06
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=4.12 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.30 M,cr=90926.70 λ_{LT}=0.42
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.57 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=48.24 Ncr,y=695531.00 λ^*_y=0.56 Curva b: Φ_y=0.71 χ_y=0.86
λ_z=81.34 Ncr,z=244617.00 λ^*_z=0.94 Curva c: Φ_z=1.12 χ_z=0.58
Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
Verifica YY: 0.01+0.03+0.26=0.30 (sic.=3.346)
Verifica ZZ: 0.02+0.03+0.26=0.30 (sic.=3.361)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 193
δ=0.16 (L/1102) (sic.=3.673)

Asta n. 30 (130 30) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a compressione (4.2.4.1.2.2) - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-1140.84
Verifica a compressione [4.2.9]
N,Ed=-1140.84 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.03 (sic.=37.710)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=1.63 - Classe 1
Sollecitazioni: T_z=-12.22
V,Ed=-12.22 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a compressione (4.2.4.1.2.2) - CC 97 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-1501.23

Verifica a compressione [4.2.9]
N,Ed=-1501.23 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.03 (sic.=28.657)

- Verifica di stabilità (4.2.4.1.3.1) - CC 97 SLU
Sollecitazioni: N=-1501.23
L=1.70
λ_Y=29.62 Ncr,y=388156.00 λ^*_y=0.34
Curva a: Φ_y=0.57 χ_y=0.97
λ_Z=102.80 Ncr,z=32213.70 λ^*_z=1.18
Curva b: Φ_z=1.37 χ_z=0.49
χ,min=0.49 N,Ed=-1501.23 Nb,Rd=20942.20 N,Ed/Nb,Rd=0.07 (sic.=13.950)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 1
Sollecitazioni: N,Ed=-1434.38 My,Ed=-2.99 L=1.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=5600.66 λ_{LT}=0.66
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.71 β_{LT}=0.75 f=0.97 χ_{LT}=0.92
λ_Y=29.62 Ncr,y=388156.00 λ^*_y=0.34 Curva a: Φ_y=0.57 χ_y=0.97
λ_Z=102.80 Ncr,z=32213.70 λ^*_z=1.18 Curva b: Φ_z=1.37 χ_z=0.49
Kyy, Kyz, Kzy, Kzz=0.95, 0.62, 0.00, 1.04
Verifica YY: 0.03+0.00=0.04 (sic.=27.935)
Verifica ZZ: 0.07=0.07 (sic.=14.600)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 165
δ=0.30 (L/539) (sic.=1.797)

Asta n. 30 (30 230) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a compressione (4.2.4.1.2.2) - CC 1 SND Xl=0.07 - Classe 3
Sollecitazioni: N=-1382.93
Verifica a compressione [4.2.9]
N,Ed=-1382.93 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.03 (sic.=31.109)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=1.86 - Classe 1
Sollecitazioni: T_z=34.23
V,Ed=34.23 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a compressione (4.2.4.1.2.2) - CC 104 SLU Xl=0.07 - Classe 1
Sollecitazioni: N=-1247.02
Verifica a compressione [4.2.9]
N,Ed=-1247.02 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.03 (sic.=34.499)

- Verifica di stabilità (4.2.4.1.3.1) - CC 1 SND
Sollecitazioni: N=-1382.93
L=2.06
λ_Y=35.89 Ncr,y=264344.00 λ^*_y=0.41
Curva a: Φ_y=0.61 χ_y=0.95
λ_Z=124.57 Ncr,z=21938.30 λ^*_z=1.43
Curva b: Φ_z=1.74 χ_z=0.37
χ,min=0.37 N,Ed=-1382.93 Nb,Rd=15801.10 N,Ed/Nb,Rd=0.09 (sic.=11.426)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
Sollecitazioni: N,Ed=-976.88 My,Ed=-9.19 L=2.06
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.06 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4279.81 λ_{LT}=0.75
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.77 β_{LT}=0.75 f=0.97 χ_{LT}=0.87
λ_Y=35.89 Ncr,y=264344.00 λ^*_y=0.41 Curva a: Φ_y=0.61 χ_y=0.95
λ_Z=124.57 Ncr,z=21938.30 λ^*_z=1.43 Curva b: Φ_z=1.74 χ_z=0.37
Kyy, Kyz, Kzy, Kzz=0.95, 0.62, 0.00, 1.03
Verifica YY: 0.02+0.00=0.03 (sic.=35.358)
Verifica ZZ: 0.06=0.06 (sic.=16.175)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 198
δ=0.16 (L/1118) (sic.=3.727)

Asta n. 31 (31 231) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a compressione (4.2.4.1.2.2) - CC 9 SND Xl=0.07 - Classe 3
Sollecitazioni: N=-272.83
Verifica a compressione [4.2.9]
N,Ed=-272.83 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.01 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=1.86 - Classe 1
Sollecitazioni: T_z=41.62
V,Ed=41.62 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.96 - Classe 1
Sollecitazioni: N=21.67 M_y=-18.62

My,Ed=-18.62 My,c,Rd=2320.00
N,Ed=21.67 Nc,Rd=43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.01 (sic. >100)

- Verifica di stabilità (4.2.4.1.3.1)
In tutte le CC risulta N < 0.04*N,cr e quindi non sono necessarie le verifiche di stabilità

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 109 SLU - Classe 1
Sollecitazioni: N,Ed=-89.80 My,Ed=18.62 L=2.06
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.06 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4279.81 λ_{LT}=0.75
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.77 β_{LT}=0.75 f=0.97 χ_{LT}=0.87
λ_y=35.89 Ncr,y=264344.00 λ^*_y=0.41 Curva a: Φ_y=0.61 χ_y=0.95
λ_z=124.57 Ncr,z=21938.30 λ^*_z=1.43 Curva b: Φ_z=1.74 χ_z=0.37
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.96
Verifica YY: 0.00+0.01=0.01 (sic.=90.967)
Verifica ZZ: 0.01=0.01 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 213
δ=0.23 (L/788) (sic.=2.627)

Asta n. 32 (32 232) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a trazione (4.2.4.1.2.1) - CC 9 SND Xl=1.86 - Classe 3
Sollecitazioni: N=69.25
Verifica a trazione [4.2.5]
N,Ed=69.25 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=1.86 - Classe 1
Sollecitazioni: T_z=41.62
V,Ed=41.62 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.96 - Classe 1
Sollecitazioni: N=54.44 M_y=-18.62
My,Ed=-18.62 My,c,Rd=2320.00
N,Ed=54.44 Nc,Rd=43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.01 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 213
δ=0.37 (L/486) (sic.=1.620)

Asta n. 33 (33 233) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a trazione (4.2.4.1.2.1) - CC 9 SND Xl=1.86 - Classe 3
Sollecitazioni: N=49.65
Verifica a trazione [4.2.5]
N,Ed=49.65 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=1.86 - Classe 1
Sollecitazioni: T_z=41.62
V,Ed=41.62 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.96 - Classe 1
Sollecitazioni: N=36.26 M_y=-18.62
My,Ed=-18.62 My,c,Rd=2320.00
N,Ed=36.26 Nc,Rd=43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.01 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 213
δ=0.47 (L/378) (sic.=1.260)

Asta n. 34 (34 234) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a trazione (4.2.4.1.2.1) - CC 1 SND Xl=1.86 - Classe 3
Sollecitazioni: N=50.70
Verifica a trazione [4.2.5]
N,Ed=50.70 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=1.86 - Classe 1
Sollecitazioni: T_z=41.62
V,Ed=41.62 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.96 - Classe 1
Sollecitazioni: N=41.91 M_y=-18.62
My,Ed=-18.62 My,c,Rd=2320.00
N,Ed=41.91 Nc,Rd=43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.01 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 213
δ=0.54 (L/333) (sic.=1.110)

Asta n. 35 (35 135) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.83 - Classe 3
Sollecitazioni: N=-2184.49 T_z=1434.16 M_y=-1188.92 T_y=1243.40 M_z=1030.78 M_x=-1.01

Tensioni: σ_N=-27.98 $\sigma_{m,d}$=-723.24 τ=2.84 σ_{max}=-751.22 (sic.=3.486)
Tensioni: σ_N=-27.98 $\sigma_{m,d}$=-23.15 τ=94.19 τ_{max}=94.19 (sic.=16.054)
Tensioni: σ_N=-27.98 $\sigma_{m,d}$=-723.24 τ=2.84 $\sigma_{ID,max}$=751.23 (sic.=3.486)

- Verifica a taglio Dir. Y [4.2.16] - CC 86 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=383.27
V,Ed=383.27 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 86 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=3265.69
V,Ed=3265.69 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.09 (sic.=11.499)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 86 SLU Xl=0.83 - Classe 1
Sollecitazioni: N=-4275.30 T_z=3265.69 M_y=-2707.26 T_y=383.27 M_z=317.73
N,Ed=-4275.30 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.02
Pressoflessione retta YY [4.2.33]:
My,Ed=-2707.26 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.16 (sic.=6.236)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=317.73 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.04 (sic.=25.232)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.16 (sic.=6.236)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-2235.30 My,Ed=-1188.92 Mz,Ed=1030.78 L=1.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=204556.00 λ_{LT}=0.28
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=23.42 Ncr,y=2951560.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
λ_z=39.48 Ncr,z=1038060.00 λ^*_z=0.45 Curva c: Φ_z=0.67 χ_z=0.87
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.08+0.19=0.27 (sic.=3.645)
Verifica ZZ: 0.01+0.06+0.19=0.26 (sic.=3.838)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 166
δ=0.14 (L/592) (sic.=1.973)

Asta n. 36 (36 236) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a compressione (4.2.4.1.2.2) - CC 1 SND Xl=0.07 - Classe 3
Sollecitazioni: N=-33.75
Verifica a compressione [4.2.9]
N,Ed=-33.75 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=0.07 - Classe 1
Sollecitazioni: T_z=20.92
V,Ed=20.92 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.97 - Classe 1
Sollecitazioni: N=-8.61 M_y=-9.41
My,Ed=-9.41 My,c,Rd=2320.00
N,Ed=-8.61 Nc,Rd=-43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.00 (sic. >100)

- Verifica di stabilità (4.2.4.1.3.1)
In tutte le CC risulta N < 0.04*N,cr e quindi non sono necessarie le verifiche di stabilità

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
Sollecitazioni: N,Ed=-76.03 My,Ed=-9.41 L=2.06
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.06 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4279.81 λ_{LT}=0.75
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.77 β_{LT}=0.75 f=0.97 χ_{LT}=0.87
λ_y=35.89 Ncr,y=264344.00 λ^*_y=0.41 Curva a: Φ_y=0.61 χ_y=0.95
λ_z=124.57 Ncr,z=21938.30 λ^*_z=1.43 Curva b: Φ_z=1.74 χ_z=0.37
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.96
Verifica YY: 0.00+0.00=0.01 (sic. >100)
Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 213
δ=0.56 (L/323) (sic.=1.077)

Asta n. 37 (37 237) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a trazione (4.2.4.1.2.1) - CC 1 SND Xl=1.86 - Classe 3
Sollecitazioni: N=42.03
Verifica a trazione [4.2.5]
N,Ed=42.03 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=1.86 - Classe 1
Sollecitazioni: T_z=20.81
V,Ed=20.81 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.96 - Classe 1
  Sollecitazioni: N=34.48 M_y=-9.31
  My,Ed=-9.31 My,c,Rd=2320.00
  N,Ed=34.48 Nc,Rd=43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.00 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 213
  δ=0.55 (L/327) (sic.=1.090)

Asta n. 38 (38 238) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a trazione (4.2.4.1.2.1) - CC 1 SND Xl=1.86 - Classe 3
  Sollecitazioni: N=48.07
  Verifica a trazione [4.2.5]
  N,Ed=48.07 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=1.86 - Classe 1
  Sollecitazioni: T_z=41.62
  V,Ed=41.62 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.96 - Classe 1
  Sollecitazioni: N=38.52 M_y=-18.62
  My,Ed=-18.62 My,c,Rd=2320.00
  N,Ed=38.52 Nc,Rd=43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.01 (sic. >100)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 213
  δ=0.50 (L/357) (sic.=1.190)

Asta n. 39 (39 239) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a trazione (4.2.4.1.2.1) - CC 1 SND Xl=1.86 - Classe 3
  Sollecitazioni: N=48.54
  Verifica a trazione [4.2.5]
  N,Ed=48.54 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=1.86 - Classe 1
  Sollecitazioni: T_z=41.62
  V,Ed=41.62 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.96 - Classe 1
  Sollecitazioni: N=31.56 M_y=-18.62
  My,Ed=-18.62 My,c,Rd=2320.00
  N,Ed=31.56 Nc,Rd=43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.01 (sic. >100)

- Verifica di stabilità (4.2.4.1.3.1)
  In tutte le CC risulta N < 0.04*N,cr e quindi non sono necessarie le verifiche di stabilità

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 140
  δ=0.41 (L/438) (sic.=1.460)

Asta n. 40 (40 240) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a trazione (4.2.4.1.2.1) - CC 9 SND Xl=1.86 - Classe 3
  Sollecitazioni: N=229.03
  Verifica a trazione [4.2.5]
  N,Ed=229.03 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.01 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=1.86 - Classe 1
  Sollecitazioni: T_z=41.62
  V,Ed=41.62 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.96 - Classe 1
  Sollecitazioni: N=102.87 M_y=-18.62
  My,Ed=-18.62 My,c,Rd=2320.00
  N,Ed=102.87 Nc,Rd=43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.01 (sic. >100)

- Verifica di stabilità (4.2.4.1.3.1)
  In tutte le CC risulta N < 0.04*N,cr e quindi non sono necessarie le verifiche di stabilità

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 140
  δ=0.28 (L/634) (sic.=2.113)

Asta n. 41 (41 241) - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica a compressione (4.2.4.1.2.2) - CC 9 SND Xl=0.07 - Classe 3
  Sollecitazioni: N=-188.97
  Verifica a compressione [4.2.9]
  N,Ed=-188.97 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=1.86 - Classe 1
  Sollecitazioni: T_z=-41.62
  V,Ed=-41.62 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 21 SLU Xl=0.96 - Classe 1
  Sollecitazioni: N=-23.36 M_y=-18.62
  My,Ed=-18.62 My,c,Rd=2320.00
  N,Ed=-23.36 Nc,Rd=-43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.01 (sic. >100)

- Verifica di stabilità (4.2.4.1.3.1)
  In tutte le CC risulta N < 0.04*N,cr e quindi non sono necessarie le verifiche di stabilità

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 114 SLU - Classe 1
  Sollecitazioni: N,Ed=-160.66 My,Ed=18.62 L=2.06
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.06 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4279.81 λ_{LT}=0.75
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.77 β_{LT}=0.75 f=0.97 χ_{LT}=0.87
  λ_y=35.89 Ncr,y=264344.00 λ^*_y=0.41 Curva a: Φ_y=0.61 χ_y=0.95
  λ_z=124.57 Ncr,z=21938.30 λ^*_z=1.43 Curva b: Φ_z=1.74 χ_z=0.37
  Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.00, 0.96
  Verifica YY: 0.00+0.01=0.01 (sic.=78.546)
  Verifica ZZ: 0.01=0.01 (sic.=98.351)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 198
  δ=0.15 (L/1172) (sic.=3.907)

Asta n. 42 (42 142) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.83 - Classe 3
  Sollecitazioni: N=-4349.59 T_z=1251.21 M_y=-1037.26 T_y=209.75 M_z=173.89 M_x=2.42
  Tensioni: σ_N=-55.70 $\sigma_{m,d}$=-268.89 τ=6.82 σ_{max}=-324.60 (sic.=8.069)
  Tensioni: σ_N=-55.70 $\sigma_{m,d}$=3.91 τ=82.26 τ_{max}=82.26 (sic.=18.381)
  Tensioni: σ_N=-55.70 $\sigma_{m,d}$=-268.89 τ=6.82 $\sigma_{ID,max}$=324.81 (sic.=8.063)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 90 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=1574.90 M_x=1.12
  V,Ed=1574.90 Vc,Rd,Red=99753.50 V,Ed/Vc,Rd,Red=0.02 (sic.=63.340)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 90 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=1900.64 M_x=1.12
  V,Ed=1900.64 Vc,Rd,Red=37520.00 V,Ed/Vc,Rd,Red=0.05 (sic.=19.741)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 80 SLU Xl=0.83 - Classe 1
  Sollecitazioni: N=-4378.95 T_z=1489.05 M_y=-1234.42 T_y=1618.68 M_z=1341.88 M_x=1.64
  N,Ed=-4378.95 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.02
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-1234.42 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.07 (sic.=13.676)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=1341.88 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.17 (sic.=5.974)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.17 (sic.=5.789)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 90 SLU - Classe 1
  Sollecitazioni: N,Ed=-4929.29 My,Ed=-1575.63 Mz,Ed=1305.59 L=1.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=204556.00 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=23.42 Ncr,y=2951560.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.98
  λ_z=39.48 Ncr,z=1038060.00 λ^*_z=0.45 Curva c: Φ_z=0.67 χ_z=0.87
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.96
  Verifica YY: 0.02+0.09+0.09=0.21 (sic.=4.827)
  Verifica ZZ: 0.03+0.05+0.16=0.24 (sic.=4.218)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 189
  δ=0.15 (L/554) (sic.=1.847)

Asta n. 42 (142 -19) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-1924.48 T_z=428.60 M_y=616.99 T_y=-488.99 M_z=754.61 M_x=1.67
  Tensioni: σ_N=-24.65 $\sigma_{m,d}$=-484.99 τ=4.70 σ_{max}=-509.63 (sic.=5.139)
  Tensioni: σ_N=-24.65 $\sigma_{m,d}$=-16.95 τ=28.82 τ_{max}=28.82 (sic.=52.475)
  Tensioni: σ_N=-24.65 $\sigma_{m,d}$=-484.99 τ=4.70 $\sigma_{ID,max}$=509.70 (sic.=5.138)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 94 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=164.88 M_x=-11.32
  V,Ed=164.88 Vc,Rd,Red=98989.70 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 94 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=956.36 M_x=-11.32
  V,Ed=956.36 Vc,Rd,Red=37232.70 V,Ed/Vc,Rd,Red=0.03 (sic.=38.932)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 37 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-3082.49 T_z=466.02 M_y=927.17 T_y=519.52 M_z=-886.90
  N,Ed=-3082.49 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.02
  Pressoflessione retta YY [4.2.33]:
  My,Ed=927.17 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.05 (sic.=18.208)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-886.90 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.11 (sic.=9.039)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.11 (sic.=8.799)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-1924.48 My,Ed=616.99 Mz,Ed=754.61 L=1.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.91 M,cr=98000.60 λ_{LT}=0.40
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.56 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=39.81 Ncr,y=1021300.00 λ^*_y=0.46 Curva b: Φ_y=0.65 χ_y=0.90
  λ_z=67.12 Ncr,z=359189.00 λ^*_z=0.77 Curva c: Φ_z=0.94 χ_z=0.68
  Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.01+0.04+0.14=0.19 (sic.=5.338)
  Verifica ZZ: 0.01+0.03+0.14=0.18 (sic.=5.468)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 188
  δ=0.17 (L/979) (sic.=3.263)

Asta n. 42 (-19 242) - Sez. 4 (Colonne principali) - Crit. 4

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.87 - Classe 3
  Sollecitazioni: N=-1601.48 T_z=428.58 M_y=-914.40 T_y=633.41 M_z=1100.91 M_x=1.67
  Tensioni: σ_N=-20.51 $\sigma_{m,d}$=-710.05 τ=4.70 σ_{max}=-730.56 (sic.=3.585)
  Tensioni: σ_N=-20.51 $\sigma_{m,d}$=132.28 τ=28.98 τ_{max}=28.98 (sic.=52.169)
  Tensioni: σ_N=-20.51 $\sigma_{m,d}$=-710.05 τ=4.70 $\sigma_{ID,max}$=730.61 (sic.=3.585)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 94 SLU Xl=0.07 - Classe 1
  Sollecitazioni: T_y=357.82 M_x=10.27
  V,Ed=357.82 Vc,Rd,Red=99068.60 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 94 SLU Xl=0.07 - Classe 1
  Sollecitazioni: T_z=738.74 M_x=10.27
  V,Ed=738.74 Vc,Rd,Red=37262.30 V,Ed/Vc,Rd,Red=0.02 (sic.=50.441)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 84 SLU Xl=1.87 - Classe 1
  Sollecitazioni: N=-2703.83 T_z=351.10 M_y=-576.70 T_y=558.45 M_z=1005.42
  N,Ed=-2703.83 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-576.70 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=29.273)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=1005.42 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.13 (sic.=7.974)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.13 (sic.=7.900)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-1723.87 My,Ed=-914.40 Mz,Ed=1100.91 L=2.06
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=4.12 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.59 M,cr=62830.50 λ_{LT}=0.50
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.61 β_{LT}=0.75 f=0.98 χ_{LT}=0.98
  λ_y=48.24 Ncr,y=695531.00 λ^*_y=0.56 Curva b: Φ_y=0.71 χ_y=0.86
  λ_z=81.34 Ncr,z=244617.00 λ^*_z=0.94 Curva c: Φ_z=1.12 χ_z=0.58
  Kyy, Kyz, Kzy, Kzz=0.95, 0.96, 0.76, 0.96
  Verifica YY: 0.01+0.06+0.20=0.27 (sic.=3.702)
  Verifica ZZ: 0.01+0.05+0.20=0.26 (sic.=3.802)

- Verifica spostamento relativo massimo per singola asta (4.2.4.2.2) - CC 198
  δ=0.15 (L/1190) (sic.=3.967)

Asta n. 1001 (101 102) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-285.87 T_z=1159.20 M_y=1160.26 T_y=-183.26 M_z=308.26
  Tensioni: σ_N=-6.32 $\sigma_{m,d}$=-695.24 τ=0.00 σ_{max}=-701.55 (sic.=3.733)
  Tensioni: σ_N=-6.32 $\sigma_{m,d}$=-10.00 τ=131.91 τ_{max}=131.91 (sic.=11.464)
  Tensioni: σ_N=-6.32 $\sigma_{m,d}$=-695.24 τ=0.00 $\sigma_{ID,max}$=701.55 (sic.=3.733)

- Verifica a taglio Dir. Y [4.2.16] - CC 100 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=60.38
  V,Ed=60.38 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 100 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=1506.27
  V,Ed=1506.27 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.07 (sic.=14.529)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 100 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=-1274.59 T_z=1506.27 M_y=1302.55 T_y=60.38 M_z=-116.31
  N,Ed=-1274.59 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=1302.55 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.15 (sic.=6.557)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-116.31 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.03 (sic.=35.273)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.15 (sic.=6.557)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-285.87 My,Ed=1160.26 Mz,Ed=308.26 L=0.95
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.47 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.05 M,cr=1420340.00 λ_{LT}=0.08
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=6.38 Ncr,y=23060300.00 λ^*_y=0.07 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=10.51 Ncr,z=8493520.00 λ^*_z=0.12 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.14+0.11=0.25 (sic.=3.927)
  Verifica ZZ: 0.00+0.11+0.11=0.23 (sic.=4.426)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 151
  $f_{z,L}$=0.01 (L/6396) (sic.=21.320)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 199
  $f_{z,L}$=0.01 (L/6092) (sic.=24.368)

Asta n. 1001 (102 103) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-291.13 T_z=397.05 M_y=-284.62 T_y=-177.72 M_z=155.34
  Tensioni: σ_N=-6.43 $\sigma_{m,d}$=-248.15 τ=0.00 σ_{max}=-254.58 (sic.=10.288)
  Tensioni: σ_N=-6.43 $\sigma_{m,d}$=-5.04 τ=45.19 τ_{max}=45.19 (sic.=33.463)
  Tensioni: σ_N=-6.43 $\sigma_{m,d}$=-248.15 τ=0.00 $\sigma_{ID,max}$=254.58 (sic.=10.288)

- Verifica a taglio Dir. Y [4.2.16] - CC 99 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=55.24
  V,Ed=55.24 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 99 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=262.16
  V,Ed=262.16 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.01 (sic.=83.478)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 84 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=534.69 T_z=-133.97 M_y=-202.78 T_y=-74.35 M_z=61.30
  N,Ed=534.69 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-202.78 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.02 (sic.=42.122)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=61.30 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.01 (sic.=66.926)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.02 (sic.=42.122)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-291.13 My,Ed=-284.62 Mz,Ed=155.34 L=0.90
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.45 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.37 M,cr=1055790.00 λ_{LT}=0.09
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=6.04 Ncr,y=25693700.00 λ^*_y=0.07 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=9.96 Ncr,z=9463460.00 λ^*_z=0.11 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.04+0.05=0.09 (sic.=10.813)
  Verifica ZZ: 0.00+0.03+0.05=0.09 (sic.=11.703)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 184
  $f_{z,L}$=0.00 (L/59929) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 184
  $f_{z,L}$=0.00 (L/38442) (sic. >100)

Asta n. 1001 (103 104) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.36 - Classe 3
  Sollecitazioni: N=-293.24 T_z=-549.65 M_y=-301.26 T_y=176.63 M_z=-70.43
  Tensioni: σ_N=-6.48 $\sigma_{m,d}$=-171.17 τ=0.00 σ_{max}=-177.65 (sic.=14.743)
  Tensioni: σ_N=-6.48 $\sigma_{m,d}$=2.29 τ=62.55 τ_{max}=62.55 (sic.=24.175)
  Tensioni: σ_N=-6.48 $\sigma_{m,d}$=-171.17 τ=0.00 $\sigma_{ID,max}$=177.65 (sic.=14.743)

- Verifica a taglio Dir. Y [4.2.16] - CC 85 SLU Xl=0.36 - Classe 1

Sollecitazioni: T_y=-76.96
V,Ed=-76.96 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 85 SLU Xl=0.36 - Classe 1
Sollecitazioni: T_z=-486.56
V,Ed=-486.56 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.02 (sic.=44.978)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 99 SLU Xl=0.36 - Classe 1
Sollecitazioni: N=-696.17 T_z=229.38 M_y=-193.22 T_y=55.23 M_z=8.98
N,Ed=-696.17 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-193.22 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.02 (sic.=44.206)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=8.98 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=44.206)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-293.24 My,Ed=-301.26 Mz,Ed=-70.43 L=0.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.28 M,cr=4975000.00 λ_{LT}=0.04
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=2.69 Ncr,y=130075000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=4.42 Ncr,z=47908800.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.02=0.06 (sic.=15.488)
Verifica ZZ: 0.00+0.03+0.02=0.06 (sic.=17.507)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 198
$f_{Z,L}$=0.00 (L/106703) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 150
$f_{Z,G}$=0.00 (L/91985) (sic. >100)

Asta n. 1001 (104 105) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.65 - Classe 3
Sollecitazioni: N=-309.15 T_z=-1238.76 M_y=1064.37 T_y=-189.72 M_z=-195.07
Tensioni: σ_N=-6.83 $\sigma_{m,d}$=-552.40 τ=0.00 σ_{max}=-559.23 (sic.=4.683)
Tensioni: σ_N=-6.83 $\sigma_{m,d}$=6.33 τ=140.96 τ_{max}=140.96 (sic.=10.727)
Tensioni: σ_N=-6.83 $\sigma_{m,d}$=-552.40 τ=0.00 $\sigma_{ID,max}$=559.23 (sic.=4.683)

- Verifica a taglio Dir. Y [4.2.16] - CC 84 SLU Xl=0.65 - Classe 1
Sollecitazioni: T_y=-74.35
V,Ed=-74.35 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 84 SLU Xl=0.65 - Classe 1
Sollecitazioni: T_z=-989.24
V,Ed=-989.24 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.05 (sic.=22.123)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 84 SLU Xl=0.65 - Classe 1
Sollecitazioni: N=534.63 T_z=-989.24 M_y=754.86 T_y=-74.35 M_z=-80.63
N,Ed=534.63 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=754.86 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.09 (sic.=11.315)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-80.63 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.02 (sic.=50.882)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.09 (sic.=11.315)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-309.15 My,Ed=1064.37 Mz,Ed=-195.07 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.38 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.45 M,cr=1608850.00 λ_{LT}=0.07
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=5.03 Ncr,y=36999000.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=8.30 Ncr,z=13627400.00 λ^*_z=0.10 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.13+0.07=0.20 (sic.=4.926)
Verifica ZZ: 0.00+0.11+0.07=0.18 (sic.=5.659)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
$f_{Z,L}$=0.00 (L/16641) (sic.=55.470)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
$f_{Z,L}$=0.00 (L/14370) (sic.=57.480)

Asta n. 1001 (105 106) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.10 - Classe 3

Sollecitazioni: N=-113.90 T_z=1107.60 M_y=938.52 T_y=46.91 M_z=-71.48
Tensioni: σ_N=-2.52 $\sigma_{m,d}$=-389.23 τ=0.00 σ_{max}=-391.75 (sic.=6.685)
Tensioni: σ_N=-2.52 $\sigma_{m,d}$=2.32 τ=126.03 τ_{max}=126.03 (sic.=11.998)
Tensioni: σ_N=-2.52 $\sigma_{m,d}$=-389.23 τ=0.00 $\sigma_{ID,max}$=391.75 (sic.=6.685)

- Verifica a taglio Dir. Y [4.2.16] - CC 99 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_y=13.91
V,Ed=13.91 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 99 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_z=903.34
V,Ed=903.34 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.04 (sic.=24.227)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 99 SLU Xl=0.10 - Classe 1
Sollecitazioni: N=-1273.90 T_z=903.34 M_y=650.51 T_y=13.91 M_z=-20.98
N,Ed=-1273.90 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=650.51 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.08 (sic.=13.130)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-20.98 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=13.130)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-113.90 My,Ed=938.52 Mz,Ed=-71.48 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.41 M,cr=1792990.00 λ_{LT}=0.07
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=4.70 Ncr,y=42473300.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=7.74 Ncr,z=15643700.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.12+0.03=0.14 (sic.=7.035)
Verifica ZZ: 0.00+0.09+0.03=0.12 (sic.=8.406)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 198
$f_{Z,G}$=0.00 (L/16059) (sic.=53.530)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 198
$f_{Z,G}$=0.00 (L/12505) (sic.=50.020)

Asta n. 1001 (106 107) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
Sollecitazioni: N=-86.99 T_z=390.24 M_y=-294.70 T_y=49.75 M_z=-46.30
Tensioni: σ_N=-1.92 $\sigma_{m,d}$=-145.44 τ=0.00 σ_{max}=-147.37 (sic.=17.772)
Tensioni: σ_N=-1.92 $\sigma_{m,d}$=1.50 τ=44.41 τ_{max}=44.41 (sic.=34.053)
Tensioni: σ_N=-1.92 $\sigma_{m,d}$=-145.44 τ=0.00 $\sigma_{ID,max}$=147.37 (sic.=17.772)

- Verifica a taglio Dir. Y [4.2.16] - CC 99 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=13.91
V,Ed=13.91 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 99 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_z=318.00
V,Ed=318.00 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.01 (sic.=68.821)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.66 - Classe 1
Sollecitazioni: N=977.80 T_z=-12.50 M_y=-82.81 T_y=-45.08 M_z=-86.21
N,Ed=977.80 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-82.81 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-86.21 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.02 (sic.=47.588)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=47.376)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-86.99 My,Ed=-294.70 Mz,Ed=-46.30 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.36 M,cr=1720240.00 λ_{LT}=0.07
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=4.70 Ncr,y=42473300.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=7.74 Ncr,z=15643700.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.02=0.05 (sic.=18.694)
Verifica ZZ: 0.00+0.03+0.02=0.05 (sic.=21.640)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
$f_{Z,L}$=0.00 (L/62838) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
  $f_{Z,L}$=0.00 (L/52102) (sic. >100)

Asta n. 1001 (107 108) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-123.17 T_z=120.17 M_y=-70.56 T_y=61.33 M_z=-40.23
  Tensioni: σ_N=-2.72 $\sigma_{m,d}$=-63.19 τ=0.00 σ_{max}=-65.92 (sic.=39.733)
  Tensioni: σ_N=-2.72 $\sigma_{m,d}$=1.31 τ=13.68 τ_{max}=13.68 (sic. >100)
  Tensioni: σ_N=-2.72 $\sigma_{m,d}$=-63.19 τ=0.00 $\sigma_{ID,max}$=65.92 (sic.=39.733)

- Verifica a taglio Dir. Y [4.2.16] - CC 79 SLU Xl=0.66 - Classe 1
  Sollecitazioni: T_y=-2.65
  V,Ed=-2.65 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 79 SLU Xl=0.66 - Classe 1
  Sollecitazioni: T_z=-134.06
  V,Ed=-134.06 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=977.80 T_z=39.31 M_y=-83.91 T_y=50.62 M_z=-86.05
  N,Ed=977.80 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-83.91 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.01 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-86.05 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.02 (sic.=47.679)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=47.461)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
  Sollecitazioni: N,Ed=-1450.83 My,Ed=-88.94 Mz,Ed=-79.78 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.07 M,cr=1353200.00 λ_{LT}=0.08
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=4.70 Ncr,y=42473300.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=7.74 Ncr,z=15643700.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.01+0.01=0.03 (sic.=30.172)
  Verifica ZZ: 0.01+0.01+0.02=0.04 (sic.=27.364)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/185149) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/76802) (sic. >100)

Asta n. 1001 (108 109) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.66 - Classe 3
  Sollecitazioni: N=-98.48 T_z=-390.15 M_y=-298.19 T_y=48.79 M_z=47.26
  Tensioni: σ_N=-2.18 $\sigma_{m,d}$=-147.57 τ=0.00 σ_{max}=-149.74 (sic.=17.490)
  Tensioni: σ_N=-2.18 $\sigma_{m,d}$=-1.53 τ=44.39 τ_{max}=44.39 (sic.=34.061)
  Tensioni: σ_N=-2.18 $\sigma_{m,d}$=-147.57 τ=0.00 $\sigma_{ID,max}$=149.74 (sic.=17.490)

- Verifica a taglio Dir. Y [4.2.16] - CC 79 SLU Xl=0.66 - Classe 1
  Sollecitazioni: T_y=-2.65
  V,Ed=-2.65 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 79 SLU Xl=0.66 - Classe 1
  Sollecitazioni: T_z=-297.83
  V,Ed=-297.83 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.01 (sic.=73.482)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 90 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-2194.03 T_z=-96.24 M_y=-63.85 T_y=73.18 M_z=-32.07
  N,Ed=-2194.03 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.02
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-63.85 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.01 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-32.07 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=54.019)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-98.48 My,Ed=-298.19 Mz,Ed=47.26 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.35 M,cr=1710690.00 λ_{LT}=0.07
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=4.70 Ncr,y=42473300.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=7.74 Ncr,z=15643700.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.02=0.05 (sic.=18.396)
Verifica ZZ: 0.00+0.03+0.02=0.05 (sic.=21.281)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
$f_{Z,L}$=0.00 (L/87867) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 203
$f_{Z,L}$=0.00 (L/60633) (sic. >100)

Asta n. 1001 (109 110) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.60 - Classe 3
Sollecitazioni: N=-115.55 T_z=-1095.55 M_y=937.48 T_y=54.73 M_z=80.16
Tensioni: σ_N=-2.55 $\sigma_{m,d}$=-397.32 τ=0.00 σ_{max}=-399.88 (sic.=6.550)
Tensioni: σ_N=-2.55 $\sigma_{m,d}$=-2.60 τ=124.66 τ_{max}=124.66 (sic.=12.130)
Tensioni: σ_N=-2.55 $\sigma_{m,d}$=-397.32 τ=0.00 $\sigma_{ID,max}$=399.88 (sic.=6.550)

- Verifica a taglio Dir. Y [4.2.16] - CC 79 SLU Xl=0.60 - Classe 1
Sollecitazioni: T_y=-2.65
V,Ed=-2.65 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 79 SLU Xl=0.60 - Classe 1
Sollecitazioni: T_z=-885.74
V,Ed=-885.74 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.04 (sic.=24.708)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 79 SLU Xl=0.60 - Classe 1
Sollecitazioni: N=-1319.15 T_z=-885.74 M_y=631.64 T_y=-2.65 M_z=-4.46
N,Ed=-1319.15 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=631.64 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.07 (sic.=13.523)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-4.46 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.07 (sic.=13.523)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-115.55 My,Ed=937.48 Mz,Ed=80.16 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.41 M,cr=1786200.00 λ_{LT}=0.07
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=4.70 Ncr,y=42473300.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=7.74 Ncr,z=15643700.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.12+0.03=0.15 (sic.=6.892)
Verifica ZZ: 0.00+0.09+0.03=0.12 (sic.=8.201)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 178
$f_{Z,L}$=0.00 (L/22015) (sic.=73.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 178
$f_{Z,L}$=0.00 (L/17497) (sic.=69.988)

Asta n. 1001 (110 111) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.10 - Classe 3
Sollecitazioni: N=-294.88 T_z=1258.44 M_y=1076.77 T_y=153.97 M_z=180.36
Tensioni: σ_N=-6.52 $\sigma_{m,d}$=-542.29 τ=0.00 σ_{max}=-548.81 (sic.=4.772)
Tensioni: σ_N=-6.52 $\sigma_{m,d}$=-5.85 τ=143.19 τ_{max}=143.19 (sic.=10.560)
Tensioni: σ_N=-6.52 $\sigma_{m,d}$=-542.29 τ=0.00 $\sigma_{ID,max}$=548.81 (sic.=4.772)

- Verifica a taglio Dir. Y [4.2.16] - CC 105 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_y=26.90
V,Ed=26.90 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 105 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_z=1114.82
V,Ed=1114.82 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.05 (sic.=19.631)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 104 SLU Xl=0.10 - Classe 1
Sollecitazioni: N=636.17 T_z=1093.49 M_y=804.54 T_y=29.63 M_z=-20.12
N,Ed=636.17 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=804.54 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.09 (sic.=10.616)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-20.12 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.09 (sic.=10.616)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-294.88 My,Ed=1076.77 Mz,Ed=180.36 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.41 M,cr=1788710.00 λ_{LT}=0.07
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=4.70 Ncr,y=42473300.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=7.74 Ncr,z=15643700.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.13+0.06=0.20 (sic.=5.020)
  Verifica ZZ: 0.00+0.11+0.06=0.17 (sic.=5.794)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
  $f_{Z,L}$=0.00 (L/12918) (sic.=43.060)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 203
  $f_{Z,L}$=0.01 (L/10084) (sic.=40.336)

Asta n. 1001 (111 112) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-277.79 T_z=553.61 M_y=-328.13 T_y=-158.78 M_z=92.65
  Tensioni: σ_N=-6.14 $\sigma_{m,d}$=-201.94 τ=0.00 σ_{max}=-208.08 (sic.=12.587)
  Tensioni: σ_N=-6.14 $\sigma_{m,d}$=-3.01 τ=63.00 τ_{max}=63.00 (sic.=24.003)
  Tensioni: σ_N=-6.14 $\sigma_{m,d}$=-201.94 τ=0.00 $\sigma_{ID,max}$=208.08 (sic.=12.587)

- Verifica a taglio Dir. Y [4.2.16] - CC 105 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=26.91
  V,Ed=26.91 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 105 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=538.06
  V,Ed=538.06 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.02 (sic.=40.673)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 79 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-810.56 T_z=-164.27 M_y=-177.75 T_y=-50.97 M_z=27.01
  N,Ed=-810.56 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-177.75 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.02 (sic.=48.053)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=27.01 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=48.053)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-277.79 My,Ed=-328.13 Mz,Ed=92.65 L=0.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.21 M,cr=4677690.00 λ_{LT}=0.04
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=2.69 Ncr,y=130075000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=4.42 Ncr,z=47908800.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.04+0.03=0.08 (sic.=13.228)
  Verifica ZZ: 0.00+0.03+0.03=0.07 (sic.=14.817)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 155
  $f_{Z,L}$=0.00 (L/60627) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 155
  $f_{Z,L}$=0.00 (L/59279) (sic. >100)

Asta n. 1001 (112 113) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.76 - Classe 3
  Sollecitazioni: N=-276.79 T_z=276.05 M_y=-130.34 T_y=-143.21 M_z=87.17
  Tensioni: σ_N=-6.12 $\sigma_{m,d}$=-129.25 τ=0.00 σ_{max}=-135.36 (sic.=19.349)
  Tensioni: σ_N=-6.12 $\sigma_{m,d}$=-2.83 τ=31.42 τ_{max}=31.42 (sic.=48.128)
  Tensioni: σ_N=-6.12 $\sigma_{m,d}$=-129.25 τ=0.00 $\sigma_{ID,max}$=135.36 (sic.=19.349)

- Verifica a taglio Dir. Y [4.2.16] - CC 51 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=4.31
  V,Ed=4.31 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 51 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=199.87
  V,Ed=199.87 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 114 SLU Xl=0.76 - Classe 1
  Sollecitazioni: N=869.48 T_z=-2.20 M_y=-107.73 T_y=55.78 M_z=87.14
  N,Ed=869.48 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:

My,Ed=-107.73 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.01 (sic.=79.283)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=87.14 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.02 (sic.=47.083)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.02 (sic.=46.732)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-275.08 My,Ed=-181.61 Mz,Ed=-86.77 L=0.80
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=1135230.00 λ_{LT}=0.08
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=5.37 Ncr,y=32518600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=8.85 Ncr,z=11977200.00 λ^*_z=0.10 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.03=0.06 (sic.=18.051)
Verifica ZZ: 0.00+0.02+0.03=0.05 (sic.=19.642)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
$f_{z,L}$=0.00 (L/105667) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
$f_{z,L}$=0.00 (L/52834) (sic. >100)

Asta n. 1001 (113 114) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.76 - Classe 3
Sollecitazioni: N=-265.92 T_z=-398.20 M_y=-400.08 T_y=-145.81 M_z=-179.72
Tensioni: σ_N=-5.88 $\sigma_{m,d}$=-311.20 τ=0.00 σ_{max}=-317.07 (sic.=8.260)
Tensioni: σ_N=-5.88 $\sigma_{m,d}$=5.83 τ=45.32 τ_{max}=45.32 (sic.=33.369)
Tensioni: σ_N=-5.88 $\sigma_{m,d}$=-311.20 τ=0.00 $\sigma_{ID,max}$=317.07 (sic.=8.260)

- Verifica a taglio Dir. Y [4.2.16] - CC 80 SLU Xl=0.76 - Classe 1
Sollecitazioni: T_y=-48.31
V,Ed=-48.31 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 80 SLU Xl=0.76 - Classe 1
Sollecitazioni: T_z=-421.91
V,Ed=-421.91 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.02 (sic.=51.871)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 105 SLU Xl=0.76 - Classe 1
Sollecitazioni: N=1238.39 T_z=230.07 M_y=-348.37 T_y=26.90 M_z=56.86
N,Ed=1238.39 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-348.37 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.04 (sic.=24.518)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=56.86 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.01 (sic.=72.157)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.04 (sic.=24.518)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-265.92 My,Ed=-400.08 Mz,Ed=-179.72 L=0.80
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.38 M,cr=1347670.00 λ_{LT}=0.08
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=5.37 Ncr,y=32518600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=8.85 Ncr,z=11977200.00 λ^*_z=0.10 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.05+0.06=0.12 (sic.=8.685)
Verifica ZZ: 0.00+0.04+0.06=0.11 (sic.=9.501)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 204
$f_{z,L}$=0.00 (L/41827) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 204
$f_{z,L}$=0.00 (L/29817) (sic. >100)

Asta n. 1001 (114 115) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.70 - Classe 3
Sollecitazioni: N=-267.77 T_z=-1193.99 M_y=1131.41 T_y=138.17 M_z=-280.85
Tensioni: σ_N=-5.92 $\sigma_{m,d}$=-658.73 τ=0.00 σ_{max}=-664.65 (sic.=3.941)
Tensioni: σ_N=-5.92 $\sigma_{m,d}$=9.11 τ=135.86 τ_{max}=135.86 (sic.=11.130)
Tensioni: σ_N=-5.92 $\sigma_{m,d}$=-658.73 τ=0.00 $\sigma_{ID,max}$=664.65 (sic.=3.941)

- Verifica a taglio Dir. Y [4.2.16] - CC 80 SLU Xl=0.70 - Classe 1
Sollecitazioni: T_y=-48.31
V,Ed=-48.31 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 80 SLU Xl=0.70 - Classe 1

Sollecitazioni: T_z=-1653.02
V,Ed=-1653.02 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.08 (sic.=13.239)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 80 SLU Xl=0.70 - Classe 1
Sollecitazioni: N=-1409.72 T_z=-1653.02 M_y=1346.06 T_y=-48.31 M_z=-108.31
N,Ed=-1409.72 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=1346.06 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.16 (sic.=6.345)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-108.31 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.03 (sic.=37.879)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.16 (sic.=6.345)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-267.77 My,Ed=1131.41 Mz,Ed=-280.85 L=0.80
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.17 M,cr=2112200.00 λ_{LT}=0.06
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=5.37 Ncr,y=32518600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=8.85 Ncr,z=11977200.00 λ^*_z=0.10 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.14+0.10=0.24 (sic.=4.146)
Verifica ZZ: 0.00+0.11+0.10=0.21 (sic.=4.689)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 179
$f_{Z,L}$=0.01 (L/8389) (sic.=27.963)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 179
$f_{Z,L}$=0.01 (L/7954) (sic.=31.816)

Asta n. 1003 (-1 -2) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.50 - Classe 3
Sollecitazioni: N=229.83 M_y=-159.63
Tensioni: σ_N=11.44 $\sigma_{m,d}$=146.90 τ=0.00 σ_{max}=158.34 (sic.=16.541)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=11.44 $\sigma_{m,d}$=146.90 τ=0.00 $\sigma_{ID,max}$=158.34 (sic.=16.541)

- Verifica a taglio Dir. Z [4.2.16] - CC 18 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=347.63
V,Ed=347.63 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.02 (sic.=42.010)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=1.33 M_y=-349.40
My,Ed=-349.40 My,c,Rd=3255.72
N,Ed=1.33 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.11 (sic.=9.318)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 58 SLU - Classe 1
Sollecitazioni: N,Ed=-354.48 My,Ed=-349.40 L=3.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4099.15 λ_{LT}=0.91
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.90 β_{LT}=0.75 f=0.97 χ_{LT}=0.77
λ_Y=45.61 Ncr,y=200195.00 λ^*_y=0.53 Curva a: Φ_y=0.67 χ_y=0.92
λ_Z=162.69 Ncr,z=15732.30 λ^*_z=1.87 Curva b: Φ_z=2.54 χ_z=0.23
Kyy, Kyz, Kzy, Kzz=0.95, 0.59, 0.00, 0.99
Verifica YY: 0.01+0.13=0.14 (sic.=7.181)
Verifica ZZ: 0.03=0.03 (sic.=34.879)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 157
$f_{Z,G}$=0.10 (L/2964) (sic.=9.880)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 127
$f_{Z,G}$=0.12 (L/2450) (sic.=9.800)

Asta n. 1003 (-2 -3) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.75 - Classe 3
Sollecitazioni: N=-107.44 M_y=-222.80
Tensioni: σ_N=-5.35 $\sigma_{m,d}$=-205.03 τ=0.00 σ_{max}=-210.38 (sic.=12.449)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=-5.35 $\sigma_{m,d}$=-205.03 τ=0.00 $\sigma_{ID,max}$=210.38 (sic.=12.449)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=558.04
V,Ed=558.04 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.04 (sic.=26.170)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.75 - Classe 1
Sollecitazioni: N=-17.52 M_y=-488.28
My,Ed=-488.28 My,c,Rd=3255.72
N,Ed=-17.52 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.15

(sic.=6.668)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 58 SLU - Classe 1
  Sollecitazioni: N,Ed=-414.30 My,Ed=-488.28 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
  λ_Y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
  λ_Z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18
  Kyy, Kyz, Kzy, Kzz=0.95, 0.61, 0.00, 1.01
  Verifica YY: 0.01+0.20=0.21 (sic.=4.798)
  Verifica ZZ: 0.04=0.04 (sic.=22.671)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 127
  $f_{Z,G}$=0.19 (L/1815) (sic.=6.050)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 116
  $f_{Z,L}$=0.23 (L/1503) (sic.=6.012)

Asta n. 1003 (-3 116) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.71 - Classe 3
  Sollecitazioni: N=-355.75 M_y=-212.73
  Tensioni: σ_N=-17.71 $\sigma_{m,d}$=-195.77 τ=0.00 σ_{max}=-213.47 (sic.=12.269)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=-17.71 $\sigma_{m,d}$=-195.77 τ=0.00 $\sigma_{ID,max}$=213.47 (sic.=12.269)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=545.28
  V,Ed=545.28 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.04 (sic.=26.782)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.71 - Classe 1
  Sollecitazioni: N=-24.34 M_y=-466.22
  My,Ed=-466.22 My,c,Rd=3255.72
  N,Ed=-24.34 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.14
(sic.=6.983)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 58 SLU - Classe 1
  Sollecitazioni: N,Ed=-342.86 My,Ed=-466.22 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
  λ_Y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
  λ_Z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18
  Kyy, Kyz, Kzy, Kzz=0.95, 0.60, 0.00, 1.00
  Verifica YY: 0.01+0.19=0.20 (sic.=5.057)
  Verifica ZZ: 0.04=0.04 (sic.=27.395)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 152
  $f_{Z,G}$=0.22 (L/1575) (sic.=5.250)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 152
  $f_{Z,G}$=0.26 (L/1314) (sic.=5.256)

Asta n. 1005 (117 -4) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.53 - Classe 3
  Sollecitazioni: N=-296.05 M_y=-155.19
  Tensioni: σ_N=-14.73 $\sigma_{m,d}$=-142.81 τ=0.00 σ_{max}=-157.55 (sic.=16.624)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=-14.73 $\sigma_{m,d}$=-142.81 τ=0.00 $\sigma_{ID,max}$=157.55 (sic.=16.624)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=3.00 - Classe 1
  Sollecitazioni: T_z=-462.44
  V,Ed=-462.44 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=31.581)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.53 - Classe 1
  Sollecitazioni: N=-2.47 M_y=-339.89
  My,Ed=-339.89 My,c,Rd=3255.72
  N,Ed=-2.47 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.10 (sic.=9.579)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 53 SLU - Classe 1
  Sollecitazioni: N,Ed=-117.81 My,Ed=-339.89 L=3.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4099.15 λ_{LT}=0.91
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.90 β_{LT}=0.75 f=0.97 χ_{LT}=0.77
  λ_Y=45.61 Ncr,y=200195.00 λ^*_y=0.53 Curva a: Φ_y=0.67 χ_y=0.92
  λ_Z=162.69 Ncr,z=15732.30 λ^*_z=1.87 Curva b: Φ_z=2.54 χ_z=0.23

Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.00, 0.96
Verifica YY: 0.00+0.13=0.13 (sic.=7.660)
Verifica ZZ: 0.01=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 132
$f_{Z,L}$=0.16 (L/1822) (sic.=6.073)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 132
$f_{Z,L}$=0.19 (L/1508) (sic.=6.032)

Asta n. 1005 (-4 -5) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.75 - Classe 3
Sollecitazioni: N=-54.50 M_y=-225.62
Tensioni: σ_N=-2.71 $\sigma_{m,d}$=-207.63 τ=0.00 σ_{max}=-210.34 (sic.=12.451)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=-2.71 $\sigma_{m,d}$=-207.63 τ=0.00 $\sigma_{ID,max}$=210.34 (sic.=12.451)

- Verifica a taglio Dir. Z [4.2.16] - CC 18 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=421.55
V,Ed=421.55 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=34.644)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.75 - Classe 1
Sollecitazioni: N=1.42 M_y=-494.77
My,Ed=-494.77 My,c,Rd=3255.72
N,Ed=1.42 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.15 (sic.=6.580)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 53 SLU - Classe 1
Sollecitazioni: N,Ed=-115.15 My,Ed=-494.77 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
λ_y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
λ_z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18
Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.00, 0.97
Verifica YY: 0.00+0.20=0.20 (sic.=4.900)
Verifica ZZ: 0.01=0.01 (sic.=81.569)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 162
$f_{Z,L}$=0.20 (L/1789) (sic.=5.963)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 116
$f_{Z,L}$=0.24 (L/1483) (sic.=5.932)

Asta n. 1005 (-5 118) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.71 - Classe 3
Sollecitazioni: N=199.27 M_y=-215.42
Tensioni: σ_N=9.92 $\sigma_{m,d}$=198.25 τ=0.00 σ_{max}=208.16 (sic.=12.582)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=9.92 $\sigma_{m,d}$=198.25 τ=0.00 $\sigma_{ID,max}$=208.16 (sic.=12.582)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=552.52
V,Ed=552.52 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.04 (sic.=26.431)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.71 - Classe 1
Sollecitazioni: N=3.08 M_y=-472.41
My,Ed=-472.41 My,c,Rd=3255.72
N,Ed=3.08 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.15 (sic.=6.892)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 63 SLU - Classe 1
Sollecitazioni: N,Ed=-102.64 My,Ed=-472.41 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
λ_y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
λ_z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18
Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.00, 0.96
Verifica YY: 0.00+0.19=0.19 (sic.=5.136)
Verifica ZZ: 0.01=0.01 (sic.=91.510)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 195
$f_{Z,L}$=0.20 (L/1748) (sic.=5.827)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 147
$f_{Z,L}$=0.23 (L/1471) (sic.=5.884)

Asta n. 1007 (-6 -7) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.50 - Classe 3
  Sollecitazioni: N=86.99 M_y=-163.54
  Tensioni: σ_N=4.33 $\sigma_{m,d}$=150.50 τ=0.00 σ_{max}=154.83 (sic.=16.915)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=4.33 $\sigma_{m,d}$=150.50 τ=0.00 $\sigma_{ID,max}$=154.83 (sic.=16.915)

- Verifica a taglio Dir. Z [4.2.16] - CC 48 SLU Xl=3.00 - Classe 1
  Sollecitazioni: T_z=-477.88
  V,Ed=-477.88 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=30.560)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.50 - Classe 1
  Sollecitazioni: N=1.04 M_y=-358.41
  My,Ed=-358.41 My,c,Rd=3255.72
  N,Ed=1.04 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.11 (sic.=9.084)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
  Sollecitazioni: N,Ed=-22.41 My,Ed=-358.41 L=3.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4099.15 λ_{LT}=0.91
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.90 β_{LT}=0.75 f=0.97 χ_{LT}=0.77
  λ_y=45.61 Ncr,y=200195.00 λ^*_y=0.53 Curva a: Φ_y=0.67 χ_y=0.92
  λ_z=162.69 Ncr,z=15732.30 λ^*_z=1.87 Curva b: Φ_z=2.54 χ_z=0.23
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
  Verifica YY: 0.00+0.14=0.14 (sic.=7.382)
  Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 137
  $f_{Z,G}$=0.10 (L/2884) (sic.=9.613)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 137
  $f_{Z,G}$=0.13 (L/2388) (sic.=9.552)

Asta n. 1007 (-7 -8) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.75 - Classe 3
  Sollecitazioni: N=83.22 M_y=-228.44
  Tensioni: σ_N=4.14 $\sigma_{m,d}$=210.22 τ=0.00 σ_{max}=214.37 (sic.=12.218)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=4.14 $\sigma_{m,d}$=210.22 τ=0.00 $\sigma_{ID,max}$=214.37 (sic.=12.218)

- Verifica a taglio Dir. Z [4.2.16] - CC 18 SLU Xl=3.50 - Classe 1
  Sollecitazioni: T_z=-426.94
  V,Ed=-426.94 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=34.206)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.75 - Classe 1
  Sollecitazioni: N=1.36 M_y=-501.26
  My,Ed=-501.26 My,c,Rd=3255.72
  N,Ed=1.36 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.15 (sic.=6.495)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 28 SLU - Classe 1
  Sollecitazioni: N,Ed=-12.55 My,Ed=-501.26 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
  λ_y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
  λ_z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
  Verifica YY: 0.00+0.20=0.20 (sic.=4.894)
  Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 132
  $f_{Z,L}$=0.20 (L/1765) (sic.=5.883)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 147
  $f_{Z,L}$=0.24 (L/1464) (sic.=5.856)

Asta n. 1007 (-8 144) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.75 - Classe 3
  Sollecitazioni: N=270.47 M_y=-228.44
  Tensioni: σ_N=13.46 $\sigma_{m,d}$=210.22 τ=0.00 σ_{max}=223.69 (sic.=11.709)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=13.46 $\sigma_{m,d}$=210.22 τ=0.00 $\sigma_{ID,max}$=223.69 (sic.=11.709)

- Verifica a taglio Dir. Z [4.2.16] - CC 18 SLU Xl=3.50 - Classe 1
  Sollecitazioni: T_z=-426.94
  V,Ed=-426.94 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=34.206)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.75 - Classe 1

Sollecitazioni: N=1.14 M_y=-501.26
My,Ed=-501.26 My,c,Rd=3255.72
N,Ed=1.14 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.15 (sic.=6.495)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 38 SLU - Classe 1
Sollecitazioni: N,Ed=-10.28 My,Ed=-501.26 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
λ_y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
λ_z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.20=0.20 (sic.=4.895)
Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 132
$f_{z,G}$=0.20 (L/1765) (sic.=5.883)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 142
$f_{z,G}$=0.24 (L/1464) (sic.=5.856)

Asta n. 1009 (122 -9) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.53 - Classe 3
Sollecitazioni: N=276.25 M_y=-155.19
Tensioni: σ_N=13.75 $\sigma_{m,d}$=142.81 τ=0.00 σ_{max}=156.56 (sic.=16.728)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=13.75 $\sigma_{m,d}$=142.81 τ=0.00 $\sigma_{ID,max}$=156.56 (sic.=16.728)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=3.00 - Classe 1
Sollecitazioni: T_z=-462.44
V,Ed=-462.44 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=31.581)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.53 - Classe 1
Sollecitazioni: N=10.44 M_y=-339.89
My,Ed=-339.89 My,c,Rd=3255.72
N,Ed=10.44 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.10 (sic.=9.579)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 101 SLU - Classe 1
Sollecitazioni: N,Ed=-78.08 My,Ed=-339.89 L=3.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4099.15 λ_{LT}=0.91
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.90 β_{LT}=0.75 f=0.97 χ_{LT}=0.77
λ_y=45.61 Ncr,y=200195.00 λ^*_y=0.53 Curva a: Φ_y=0.67 χ_y=0.92
λ_z=162.69 Ncr,z=15732.30 λ^*_z=1.87 Curva b: Φ_z=2.54 χ_z=0.23
Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.00, 0.96
Verifica YY: 0.00+0.13=0.13 (sic.=7.711)
Verifica ZZ: 0.01=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 180
$f_{z,L}$=0.16 (L/1821) (sic.=6.070)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 180
$f_{z,L}$=0.20 (L/1508) (sic.=6.032)

Asta n. 1009 (-9 -10) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.75 - Classe 3
Sollecitazioni: N=27.70 M_y=-225.62
Tensioni: σ_N=1.38 $\sigma_{m,d}$=207.63 τ=0.00 σ_{max}=209.01 (sic.=12.531)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=1.38 $\sigma_{m,d}$=207.63 τ=0.00 $\sigma_{ID,max}$=209.01 (sic.=12.531)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=565.45
V,Ed=565.45 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.04 (sic.=25.827)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.75 - Classe 1
Sollecitazioni: N=6.23 M_y=-494.77
My,Ed=-494.77 My,c,Rd=3255.72
N,Ed=6.23 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.15 (sic.=6.580)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 53 SLU - Classe 1
Sollecitazioni: N,Ed=-82.00 My,Ed=-494.77 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
λ_y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
λ_z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18

Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.00, 0.96
Verifica YY: 0.00+0.20=0.20 (sic.=4.918)
Verifica ZZ: 0.01=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 132
$f_{z,L}$=0.20 (L/1789) (sic.=5.963)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 175
$f_{z,L}$=0.24 (L/1483) (sic.=5.932)

Asta n. 1009 (-10 123) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.71 - Classe 3
Sollecitazioni: N=234.90 M_y=-215.42
Tensioni: σ_N=11.69 $\sigma_{m,d}$=198.25 τ=0.00 σ_{max}=209.94 (sic.=12.476)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=11.69 $\sigma_{m,d}$=198.25 τ=0.00 $\sigma_{ID,max}$=209.94 (sic.=12.476)

- Verifica a taglio Dir. Z [4.2.16] - CC 74 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=411.91
V,Ed=411.91 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=35.454)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.71 - Classe 1
Sollecitazioni: N=5.69 M_y=-472.41
My,Ed=-472.41 My,c,Rd=3255.72
N,Ed=5.69 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.15 (sic.=6.892)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 91 SLU - Classe 1
Sollecitazioni: N,Ed=-74.53 My,Ed=-472.41 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
λ_y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
λ_z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18
Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.00, 0.96
Verifica YY: 0.00+0.19=0.19 (sic.=5.153)
Verifica ZZ: 0.01=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 195
$f_{z,L}$=0.19 (L/1777) (sic.=5.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 195
$f_{z,L}$=0.23 (L/1499) (sic.=5.996)

Asta n. 1011 (-11 -12) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.50 - Classe 3
Sollecitazioni: N=-228.60 M_y=-159.63
Tensioni: σ_N=-11.38 $\sigma_{m,d}$=-146.90 τ=0.00 σ_{max}=-158.28 (sic.=16.547)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=-11.38 $\sigma_{m,d}$=-146.90 τ=0.00 $\sigma_{ID,max}$=158.28 (sic.=16.547)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=465.87
V,Ed=465.87 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=31.348)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.50 - Classe 1
Sollecitazioni: N=-8.57 M_y=-349.40
My,Ed=-349.40 My,c,Rd=3255.72
N,Ed=-8.57 Nc,Rd=-52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.11 (sic.=9.318)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 86 SLU - Classe 1
Sollecitazioni: N,Ed=-259.97 My,Ed=-349.40 L=3.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4099.15 λ_{LT}=0.91
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.90 β_{LT}=0.75 f=0.97 χ_{LT}=0.77
λ_y=45.61 Ncr,y=200195.00 λ^*_y=0.53 Curva a: Φ_y=0.67 χ_y=0.92
λ_z=162.69 Ncr,z=15732.30 λ^*_z=1.87 Curva b: Φ_z=2.54 χ_z=0.23
Kyy, Kyz, Kzy, Kzz=0.95, 0.59, 0.00, 0.98
Verifica YY: 0.01+0.13=0.14 (sic.=7.288)
Verifica ZZ: 0.02=0.02 (sic.=47.559)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 116
$f_{z,L}$=0.10 (L/2964) (sic.=9.880)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 205
$f_{z,G}$=0.12 (L/2450) (sic.=9.800)

Asta n. 1011 (-12 -13) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.75 - Classe 3
  Sollecitazioni: N=93.72 M_y=-222.80
  Tensioni: σ_N=4.66 $\sigma_{m,d}$=205.03 τ=0.00 σ_{max}=209.70 (sic.=12.490)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=4.66 $\sigma_{m,d}$=205.03 τ=0.00 $\sigma_{ID,max}$=209.70 (sic.=12.490)

- Verifica a taglio Dir. Z [4.2.16] - CC 22 SLU Xl=3.50 - Classe 1
  Sollecitazioni: T_z=-416.15
  V,Ed=-416.15 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=35.093)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.75 - Classe 1
  Sollecitazioni: N=17.08 M_y=-488.28
  My,Ed=-488.28 My,c,Rd=3255.72
  N,Ed=17.08 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.15 (sic.=6.668)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 86 SLU - Classe 1
  Sollecitazioni: N,Ed=-259.15 My,Ed=-488.28 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
  λ_Y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
  λ_Z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18
  Kyy, Kyz, Kzy, Kzz=0.95, 0.59, 0.00, 0.99
  Verifica YY: 0.01+0.20=0.20 (sic.=4.883)
  Verifica ZZ: 0.03=0.03 (sic.=36.244)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 185
  $f_{Z,L}$=0.19 (L/1815) (sic.=6.050)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 147
  $f_{Z,L}$=0.23 (L/1503) (sic.=6.012)

Asta n. 1011 (-13 124) - Sez. 11 (Travi terziarie_sottostruttura) - Crit. 9

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=1.71 - Classe 3
  Sollecitazioni: N=320.27 M_y=-212.73
  Tensioni: σ_N=15.94 $\sigma_{m,d}$=195.77 τ=0.00 σ_{max}=211.71 (sic.=12.371)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=15.94 $\sigma_{m,d}$=195.77 τ=0.00 $\sigma_{ID,max}$=211.71 (sic.=12.371)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=406.63
  V,Ed=406.63 Vc,Rd=14604.00 V,Ed/Vc,Rd=0.03 (sic.=35.914)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 17 SLU Xl=1.71 - Classe 1
  Sollecitazioni: N=20.70 M_y=-466.22
  My,Ed=-466.22 My,c,Rd=3255.72
  N,Ed=20.70 Nc,Rd=52621.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=3255.72 My,Ed/MNy,c,Rd=0.14 (sic.=6.983)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 96 SLU - Classe 1
  Sollecitazioni: N,Ed=-234.27 My,Ed=-466.22 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3389.53 λ_{LT}=1.00
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.98 β_{LT}=0.75 f=0.97 χ_{LT}=0.72
  λ_Y=53.21 Ncr,y=147082.00 λ^*_y=0.61 Curva a: Φ_y=0.73 χ_y=0.89
  λ_Z=189.81 Ncr,z=11558.40 λ^*_z=2.19 Curva b: Φ_z=3.23 χ_z=0.18
  Kyy, Kyz, Kzy, Kzz=0.95, 0.59, 0.00, 0.98
  Verifica YY: 0.01+0.19=0.20 (sic.=5.122)
  Verifica ZZ: 0.02=0.02 (sic.=40.093)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 200
  $f_{Z,G}$=0.22 (L/1588) (sic.=5.293)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 200
  $f_{Z,G}$=0.26 (L/1327) (sic.=5.308)

Asta n. 1012 (125 127) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=623.45 T_z=731.76 M_y=973.29 T_y=-179.66 M_z=303.89
  Tensioni: σ_N=13.78 $\sigma_{m,d}$=627.30 τ=0.00 σ_{max}=641.08 (sic.=4.085)
  Tensioni: σ_N=13.78 $\sigma_{m,d}$=-9.86 τ=83.27 τ_{max}=83.27 (sic.=18.159)
  Tensioni: σ_N=13.78 $\sigma_{m,d}$=627.30 τ=0.00 $\sigma_{ID,max}$=641.08 (sic.=4.085)

- Verifica a taglio Dir. Y [4.2.16] - CC 85 SLU Xl=2.16 - Classe 1
  Sollecitazioni: T_y=42.59
  V,Ed=42.59 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 85 SLU Xl=2.16 - Classe 1

Sollecitazioni: T_z=-843.61
V,Ed=-843.61 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.04 (sic.=25.942)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 52 SLU Xl=0.10 - Classe 1
Sollecitazioni: N=-973.22 T_z=770.71 M_y=1038.61 T_y=-53.25 M_z=100.20
N,Ed=-973.22 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=1038.61 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.12 (sic.=8.224)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=100.20 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.02 (sic.=40.946)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.12 (sic.=8.224)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-475.15 My,Ed=973.29 Mz,Ed=303.89 L=2.20
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.10 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.37 M,cr=183927.00 λ_{LT}=0.21
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=14.77 Ncr,y=4299980.00 λ^*_y=0.17 Curva b: Φ_y=0.51 χ_y=1.00
λ_Z=24.34 Ncr,z=1583760.00 λ^*_z=0.28 Curva c: Φ_z=0.56 χ_z=0.96
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.12+0.11=0.23 (sic.=4.316)
Verifica ZZ: 0.00+0.10+0.11=0.21 (sic.=4.813)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 136
$f_{Z,L}$=0.04 (L/5836) (sic.=19.453)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 136
$f_{Z,L}$=0.04 (L/5712) (sic.=22.848)

Asta n. 1012 (127 128) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.36 - Classe 3
Sollecitazioni: N=527.17 T_z=-740.67 M_y=729.72 T_y=174.59 M_z=-138.93
Tensioni: σ_N=11.65 $\sigma_{m,d}$=383.77 τ=0.00 σ_{max}=395.42 (sic.=6.624)
Tensioni: σ_N=11.65 $\sigma_{m,d}$=4.51 τ=84.28 τ_{max}=84.28 (sic.=17.941)
Tensioni: σ_N=11.65 $\sigma_{m,d}$=383.77 τ=0.00 $\sigma_{ID,max}$=395.42 (sic.=6.624)

- Verifica a taglio Dir. Y [4.2.16] - CC 36 SLU Xl=0.36 - Classe 1
Sollecitazioni: T_y=53.34
V,Ed=53.34 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 36 SLU Xl=0.36 - Classe 1
Sollecitazioni: T_z=-600.56
V,Ed=-600.56 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.03 (sic.=36.441)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 85 SLU Xl=0.36 - Classe 1
Sollecitazioni: N=1083.62 T_z=-586.11 M_y=621.37 T_y=42.60 M_z=12.27
N,Ed=1083.62 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=621.37 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.07 (sic.=13.746)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=12.27 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.07 (sic.=13.746)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-495.07 My,Ed=729.72 Mz,Ed=-138.93 L=0.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=4550130.00 λ_{LT}=0.04
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=2.69 Ncr,y=130075000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=4.42 Ncr,z=47908800.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.09+0.05=0.14 (sic.=6.974)
Verifica ZZ: 0.00+0.07+0.05=0.13 (sic.=7.977)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
$f_{Z,L}$=0.00 (L/33817) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
$f_{Z,G}$=0.00 (L/26919) (sic. >100)

Asta n. 1012 (128 129) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.30 - Classe 3
Sollecitazioni: N=522.74 T_z=-1279.00 M_y=1138.73 T_y=178.94 M_z=-194.90
Tensioni: σ_N=11.55 $\sigma_{m,d}$=577.55 τ=0.00 σ_{max}=589.10 (sic.=4.446)
Tensioni: σ_N=11.55 $\sigma_{m,d}$=6.32 τ=145.53 τ_{max}=145.53 (sic.=10.390)

Tensioni: σ_N=11.55 $\sigma_{m,d}$=577.55 τ=0.00 $\sigma_{ID,max}$=589.10 (sic.=4.446)

- Verifica a taglio Dir. Y [4.2.16] - CC 36 SLU Xl=0.30 - Classe 1
  Sollecitazioni: T_y=53.32
  V,Ed=53.32 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 36 SLU Xl=0.30 - Classe 1
  Sollecitazioni: T_z=-856.33
  V,Ed=-856.33 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.04 (sic.=25.557)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 84 SLU Xl=0.30 - Classe 1
  Sollecitazioni: N=485.30 T_z=-830.08 M_y=887.14 T_y=46.54 M_z=35.57
  N,Ed=485.30 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=887.14 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.10 (sic.=9.628)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=35.57 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.10 (sic.=9.628)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-503.83 My,Ed=1138.73 Mz,Ed=-194.90 L=0.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.15 M,cr=4469870.00 λ_{LT}=0.04
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=2.69 Ncr,y=130074000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=4.42 Ncr,z=47908700.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.14+0.07=0.21 (sic.=4.678)
  Verifica ZZ: 0.00+0.11+0.07=0.19 (sic.=5.387)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
  $f_{Z,L}$=0.00 (L/15631) (sic.=52.103)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
  $f_{Z,L}$=0.00 (L/13168) (sic.=52.672)

Asta n. 1012 (129 130) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-641.99 T_z=1564.17 M_y=865.69 T_y=44.14 M_z=-68.39
  Tensioni: σ_N=-14.19 $\sigma_{m,d}$=-361.41 τ=0.00 σ_{max}=-375.60 (sic.=6.973)
  Tensioni: σ_N=-14.19 $\sigma_{m,d}$=2.22 τ=177.98 τ_{max}=177.98 (sic.=8.496)
  Tensioni: σ_N=-14.19 $\sigma_{m,d}$=-361.41 τ=0.00 $\sigma_{ID,max}$=375.60 (sic.=6.973)

- Verifica a taglio Dir. Y [4.2.16] - CC 99 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=4.30
  V,Ed=4.30 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 99 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=1775.13
  V,Ed=1775.13 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.08 (sic.=12.329)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 99 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=-1400.56 T_z=1775.13 M_y=661.26 T_y=4.30 M_z=-8.81
  N,Ed=-1400.56 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=661.26 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.08 (sic.=12.917)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-8.81 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=12.917)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-641.99 My,Ed=865.69 Mz,Ed=-68.39 L=0.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.41 M,cr=9316700.00 λ_{LT}=0.03
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.01 χ_{LT}=1.00
  λ_Y=2.69 Ncr,y=130074000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=4.42 Ncr,z=47908700.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.11+0.02=0.14 (sic.=7.325)
  Verifica ZZ: 0.01+0.09+0.02=0.12 (sic.=8.686)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 198
  $f_{Z,L}$=0.00 (L/20279) (sic.=67.597)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 198
  $f_{Z,L}$=0.00 (L/10476) (sic.=41.904)

Asta n. 1012 (130 135) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=3.00 - Classe 3
  Sollecitazioni: N=-696.12 T_z=-545.70 M_y=652.98 T_y=45.19 M_z=79.40
  Tensioni: σ_N=-15.38 $\sigma_{m,d}$=-299.69 τ=0.00 σ_{max}=-315.07 (sic.=8.313)
  Tensioni: σ_N=-15.38 $\sigma_{m,d}$=-2.58 τ=62.09 τ_{max}=62.09 (sic.=24.352)
  Tensioni: σ_N=-15.38 $\sigma_{m,d}$=-299.69 τ=0.00 $\sigma_{ID,max}$=315.07 (sic.=8.313)

- Verifica a taglio Dir. Y [4.2.16] - CC 76 SLU Xl=3.00 - Classe 1
  Sollecitazioni: T_y=13.84
  V,Ed=13.84 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 76 SLU Xl=3.00 - Classe 1
  Sollecitazioni: T_z=-510.58
  V,Ed=-510.58 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.02 (sic.=42.863)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 79 SLU Xl=3.00 - Classe 1
  Sollecitazioni: N=-1875.76 T_z=-508.54 M_y=530.41 T_y=12.14 M_z=19.42
  N,Ed=-1875.76 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.02
  Pressoflessione retta YY [4.2.33]:
  My,Ed=530.41 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.06 (sic.=16.103)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=19.42 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.103)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-696.12 My,Ed=652.98 Mz,Ed=79.40 L=3.10
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.55 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.79 M,cr=197124.00 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=20.81 Ncr,y=2165650.00 λ^*_y=0.24 Curva b: Φ_y=0.54 χ_y=0.99
  λ_z=34.29 Ncr,z=797649.00 λ^*_z=0.39 Curva c: Φ_z=0.63 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.08+0.03=0.11 (sic.=8.713)
  Verifica ZZ: 0.01+0.06+0.03=0.10 (sic.=10.081)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 204
  $f_{Z,L}$=0.02 (L/18259) (sic.=60.863)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 184
  $f_{Z,L}$=0.02 (L/12533) (sic.=50.132)

Asta n. 1012 (135 142) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=3.40 - Classe 3
  Sollecitazioni: N=-604.39 T_z=-581.34 M_y=861.51 T_y=-138.00 M_z=-273.60
  Tensioni: σ_N=-13.36 $\sigma_{m,d}$=-559.74 τ=0.00 σ_{max}=-573.10 (sic.=4.570)
  Tensioni: σ_N=-13.36 $\sigma_{m,d}$=8.88 τ=66.15 τ_{max}=66.15 (sic.=22.858)
  Tensioni: σ_N=-13.36 $\sigma_{m,d}$=-559.74 τ=0.00 $\sigma_{ID,max}$=573.10 (sic.=4.570)

- Verifica a taglio Dir. Y [4.2.16] - CC 105 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=-72.18
  V,Ed=-72.18 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 105 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=743.00
  V,Ed=743.00 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.03 (sic.=29.455)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 32 SLU Xl=3.40 - Classe 1
  Sollecitazioni: N=-1743.67 T_z=-707.64 M_y=1022.02 T_y=43.57 M_z=90.63
  N,Ed=-1743.67 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=1022.02 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.12 (sic.=8.357)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=90.63 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.02 (sic.=45.269)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.12 (sic.=8.357)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-604.39 My,Ed=861.51 Mz,Ed=-273.60 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.13 M,cr=64076.90 λ_{LT}=0.35
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=23.50 Ncr,y=1698930.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.97
  λ_z=38.72 Ncr,z=625747.00 λ^*_z=0.45 Curva c: Φ_z=0.66 χ_z=0.87
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.11+0.10=0.21 (sic.=4.796)
  Verifica ZZ: 0.01+0.09+0.10=0.19 (sic.=5.324)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 204
  $f_{Z,L}$=0.05 (L/7328) (sic.=24.427)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 204
  $f_{Z,L}$=0.05 (L/7009) (sic.=28.036)

Asta n. 1013 (101 -1) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-357.44 T_z=1148.19 M_y=1303.27 T_y=-186.78 M_z=-135.45 M_x=12.99
  Tensioni: σ_N=-7.90 $\sigma_{m,d}$=-575.73 τ=92.23 σ_{max}=-583.63 (sic.=4.488)
  Tensioni: σ_N=-7.90 $\sigma_{m,d}$=4.39 τ=160.46 τ_{max}=160.46 (sic.=9.423)
  Tensioni: σ_N=-7.90 $\sigma_{m,d}$=-575.73 τ=92.23 $\sigma_{ID,max}$=605.10 (sic.=4.328)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 58 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=-264.63 M_x=28.31
  V,Ed=-264.63 Vc,Rd,Red=54223.70 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 58 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=1567.21 M_x=28.31
  V,Ed=1567.21 Vc,Rd,Red=20688.30 V,Ed/Vc,Rd,Red=0.08 (sic.=13.201)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=-1029.08 T_z=1520.15 M_y=1573.28 T_y=-335.52 M_z=139.63 M_x=21.13
  N,Ed=-1029.08 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=1573.28 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.18 (sic.=5.429)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=139.63 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.03 (sic.=29.383)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.18 (sic.=5.429)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-357.44 My,Ed=1303.27 Mz,Ed=-135.45 L=0.72
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.36 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.33 M,cr=1570100.00 λ_{LT}=0.07
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=4.87 Ncr,y=39594600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=8.02 Ncr,z=14583400.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.16+0.05=0.21 (sic.=4.720)
  Verifica ZZ: 0.00+0.13+0.05=0.18 (sic.=5.566)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 160
  $f_{Z,L}$=0.01 (L/6347) (sic.=21.157)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 160
  $f_{Z,L}$=0.01 (L/5232) (sic.=20.928)

Asta n. 1013 (-1 117) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.67 - Classe 3
  Sollecitazioni: N=-318.04 T_z=304.46 M_y=-212.34 T_y=491.27 M_z=-274.09 M_x=12.99
  Tensioni: σ_N=-7.03 $\sigma_{m,d}$=-339.12 τ=92.29 σ_{max}=-346.15 (sic.=7.566)
  Tensioni: σ_N=-7.03 $\sigma_{m,d}$=42.70 τ=105.89 τ_{max}=105.89 (sic.=14.280)
  Tensioni: σ_N=-7.03 $\sigma_{m,d}$=-339.12 τ=92.29 $\sigma_{ID,max}$=381.27 (sic.=6.869)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 61 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=83.38 M_x=21.13
  V,Ed=83.38 Vc,Rd,Red=55036.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 61 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=1072.94 M_x=21.13
  V,Ed=1072.94 Vc,Rd,Red=20998.20 V,Ed/Vc,Rd,Red=0.05 (sic.=19.571)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-1029.08 T_z=1072.94 M_y=654.20 T_y=83.38 M_z=-70.07 M_x=21.13
  N,Ed=-1029.08 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=654.20 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.08 (sic.=13.056)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-70.07 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.02 (sic.=58.551)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=13.056)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-343.73 My,Ed=285.70 Mz,Ed=-271.69 L=0.72
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.36 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.41 M,cr=2850780.00 λ_{LT}=0.05

$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=4.87 Ncr,y=39594600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=8.02 Ncr,z=14583400.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.10=0.13 (sic.=7.455)
Verifica ZZ: 0.00+0.03+0.10=0.13 (sic.=7.869)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
$f_{Z,L}$=0.00 (L/17351) (sic.=57.837)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
$f_{Z,L}$=0.00 (L/17112) (sic.=68.448)

Asta n. 1013 (117 -6) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.75 - Classe 3
Sollecitazioni: N=-314.15 T_z=194.07 M_y=-258.98 T_y=-112.90 M_z=-361.34
Tensioni: σ_N=-6.94 $\sigma_{m,d}$=-439.93 τ=0.00 σ_{max}=-446.87 (sic.=5.861)
Tensioni: σ_N=-6.94 $\sigma_{m,d}$=11.72 τ=22.09 τ_{max}=22.09 (sic.=68.454)
Tensioni: σ_N=-6.94 $\sigma_{m,d}$=-439.93 τ=0.00 $\sigma_{ID,max}$=446.87 (sic.=5.861)

- Verifica a taglio Dir. Y [4.2.16] - CC 58 SLU Xl=0.06 - Classe 1
Sollecitazioni: T_y=3.33
V,Ed=3.33 Vc,Rd=57359.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 58 SLU Xl=0.06 - Classe 1
Sollecitazioni: T_z=477.45
V,Ed=477.45 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.02 (sic.=45.837)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 111 SLU Xl=0.75 - Classe 1
Sollecitazioni: N=496.25 T_z=325.34 M_y=-512.46 T_y=15.59 M_z=3.80
N,Ed=496.25 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-512.46 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.06 (sic.=16.668)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=3.80 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.668)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-314.15 My,Ed=-258.98 Mz,Ed=-361.34 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.38 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.18 M,cr=1302950.00 λ_{LT}=0.08
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=5.03 Ncr,y=36999000.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=8.30 Ncr,z=13627400.00 λ^*_z=0.10 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.13=0.16 (sic.=6.163)
Verifica ZZ: 0.00+0.03+0.13=0.16 (sic.=6.417)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 190
$f_{Z,L}$=0.00 (L/27303) (sic.=91.010)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 190
$f_{Z,L}$=0.00 (L/17948) (sic.=71.792)

Asta n. 1013 (-6 122) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-305.44 T_z=-133.22 M_y=-258.98 T_y=114.00 M_z=-361.34
Tensioni: σ_N=-6.75 $\sigma_{m,d}$=-439.93 τ=0.00 σ_{max}=-446.68 (sic.=5.863)
Tensioni: σ_N=-6.75 $\sigma_{m,d}$=11.72 τ=15.17 τ_{max}=15.17 (sic.=99.686)
Tensioni: σ_N=-6.75 $\sigma_{m,d}$=-439.93 τ=0.00 $\sigma_{ID,max}$=446.68 (sic.=5.863)

- Verifica a taglio Dir. Z [4.2.16] - CC 91 SLU Xl=0.69 - Classe 1
Sollecitazioni: T_z=-482.58
V,Ed=-482.58 Vc,Rd=21884.80 V,Ed/Vc,Rd=0.02 (sic.=45.350)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 111 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=496.25 T_z=-152.54 M_y=-512.47 T_y=-1.84 M_z=3.80
N,Ed=496.25 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-512.47 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.06 (sic.=16.667)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=3.80 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.667)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-305.44 My,Ed=-258.98 Mz,Ed=-361.34 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.38 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.08 M,cr=1195790.00 λ_{LT}=0.08
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=5.03 Ncr,y=36999000.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=8.30 Ncr,z=13627400.00 λ^*_z=0.10 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.13=0.16 (sic.=6.166)
Verifica ZZ: 0.00+0.03+0.13=0.16 (sic.=6.420)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 210
$f_{Z,G}$=0.00 (L/24630) (sic.=82.100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 210
$f_{Z,L}$=0.00 (L/16213) (sic.=64.852)

Asta n. 1013 (122 -11) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.06 - Classe 3
Sollecitazioni: N=-310.87 T_z=-308.20 M_y=-211.16 T_y=485.44 M_z=-264.57 M_x=-13.00
Tensioni: σ_N=-6.87 $\sigma_{m,d}$=-329.45 τ=92.33 σ_{max}=-336.32 (sic.=7.787)
Tensioni: σ_N=-6.87 $\sigma_{m,d}$=-42.73 τ=105.96 τ_{max}=105.96 (sic.=14.271)
Tensioni: σ_N=-6.87 $\sigma_{m,d}$=-329.45 τ=92.33 $\sigma_{ID,max}$=372.40 (sic.=7.033)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 89 SLU Xl=0.72 - Classe 1
Sollecitazioni: T_y=-70.96 M_x=-21.18
V,Ed=-70.96 Vc,Rd,Red=55030.30 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 89 SLU Xl=0.72 - Classe 1
Sollecitazioni: T_z=-1072.47 M_x=-21.18
V,Ed=-1072.47 Vc,Rd,Red=20996.00 V,Ed/Vc,Rd,Red=0.05 (sic.=19.577)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.72 - Classe 1
Sollecitazioni: N=-1096.35 T_z=-1072.47 M_y=649.63 T_y=-70.96 M_z=-44.55 M_x=-21.18
N,Ed=-1096.35 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=649.63 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.08 (sic.=13.148)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-44.55 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.01 (sic.=92.102)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=13.148)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-349.10 My,Ed=289.53 Mz,Ed=267.54 L=0.72
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.36 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.39 M,cr=2830240.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=4.87 Ncr,y=39594600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=8.02 Ncr,z=14583400.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.09=0.13 (sic.=7.508)
Verifica ZZ: 0.00+0.03+0.09=0.13 (sic.=7.934)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
$f_{Z,L}$=0.00 (L/23538) (sic.=78.460)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 165
$f_{Z,G}$=0.00 (L/19505) (sic.=78.020)

Asta n. 1013 (-11 125) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.62 - Classe 3
Sollecitazioni: N=-366.13 T_z=-1151.13 M_y=1308.96 T_y=182.52 M_z=137.69 M_x=-12.99
Tensioni: σ_N=-8.09 $\sigma_{m,d}$=-579.85 τ=92.28 σ_{max}=-587.94 (sic.=4.455)
Tensioni: σ_N=-8.09 $\sigma_{m,d}$=-4.47 τ=160.75 τ_{max}=160.75 (sic.=9.407)
Tensioni: σ_N=-8.09 $\sigma_{m,d}$=-579.85 τ=92.28 $\sigma_{ID,max}$=609.28 (sic.=4.299)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 86 SLU Xl=0.62 - Classe 1
Sollecitazioni: T_y=185.68 M_x=-28.36
V,Ed=185.68 Vc,Rd,Red=54218.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 86 SLU Xl=0.62 - Classe 1
Sollecitazioni: T_z=-1568.53 M_x=-28.36
V,Ed=-1568.53 Vc,Rd,Red=20686.10 V,Ed/Vc,Rd,Red=0.08 (sic.=13.188)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.62 - Classe 1
Sollecitazioni: N=-1096.35 T_z=-1519.67 M_y=1568.42 T_y=228.53 M_z=98.28 M_x=-21.18
N,Ed=-1096.35 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=1568.42 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.18 (sic.=5.446)

Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=98.28 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.02 (sic.=41.743)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.18 (sic.=5.446)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-366.13 My,Ed=1308.96 Mz,Ed=137.69 L=0.72
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.36 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.33 M,cr=1569260.00 λ_{LT}=0.07
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=4.87 Ncr,y=39594600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=8.02 Ncr,z=14583400.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.16+0.05=0.21 (sic.=4.685)
Verifica ZZ: 0.00+0.13+0.05=0.18 (sic.=5.522)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 188
$f_{z,L}$=0.01 (L/7790) (sic.=25.967)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 188
$f_{z,L}$=0.01 (L/6587) (sic.=26.348)

Asta n. 1017 (105 -2) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.10 - Classe 3
Sollecitazioni: N=-983.68 T_z=1652.81 M_y=1428.53 T_y=-373.87 M_z=198.29
Tensioni: σ_N=-34.53 $\sigma_{m,d}$=-1431.52 τ=0.00 σ_{max}=-1466.05 (sic.=1.786)
Tensioni: σ_N=-34.53 $\sigma_{m,d}$=-39.00 τ=178.38 τ_{max}=178.38 (sic.=8.477)
Tensioni: σ_N=-34.53 $\sigma_{m,d}$=-1431.52 τ=0.00 $\sigma_{ID,max}$=1466.05 (sic.=1.786)

- Verifica a taglio Dir. Y [4.2.16] - CC 58 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_y=-48.84
V,Ed=-48.84 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 58 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_z=3510.60
V,Ed=3510.60 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.17 (sic.=6.031)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 58 SLU Xl=0.10 - Classe 1
Sollecitazioni: N=-2340.04 T_z=3510.60 M_y=2977.85 T_y=-48.84 M_z=21.90
N,Ed=-2340.04 Nc,Rd=74603.30 n=N,Ed/Nc,Rd=0.03
Pressoflessione retta YY [4.2.33]:
My,Ed=2977.85 My,V,c,Rd=5804.95 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.51 (sic.=1.949)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=21.90 Mz,V,c,Rd=1170.59 MNz,c,Rd=1170.59 Mz,Ed/MNz,c,Rd=0.02 (sic.=53.458)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.51 (sic.=1.949)

Asta n. 1017 (-2 -4) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-976.79 T_z=1383.22 M_y=855.13 T_y=15.25 M_z=-20.06
Tensioni: σ_N=-34.29 $\sigma_{m,d}$=-510.50 τ=0.00 σ_{max}=-544.79 (sic.=4.807)
Tensioni: σ_N=-34.29 $\sigma_{m,d}$=3.94 τ=149.26 τ_{max}=149.26 (sic.=10.130)
Tensioni: σ_N=-34.29 $\sigma_{m,d}$=-510.50 τ=0.00 $\sigma_{ID,max}$=544.79 (sic.=4.807)

- Verifica a taglio Dir. Y [4.2.16] - CC 58 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=10.98
V,Ed=10.98 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 58 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=2284.63
V,Ed=2284.63 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.11 (sic.=9.267)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 91 SLU Xl=0.72 - Classe 1
Sollecitazioni: N=-1104.35 T_z=1537.10 M_y=-1240.02 T_y=-2.75
My,Ed=-1240.02 My,V,c,Rd=5804.95
N,Ed=-1104.35 Nc,Rd=-74603.30 YY n=N,Ed/Nc,Rd=0.01 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.21
(sic.=4.681)

Asta n. 1017 (-4 -7) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.75 - Classe 3
Sollecitazioni: N=-919.09 T_z=398.08 M_y=-669.68 T_y=-42.02 M_z=-60.68
Tensioni: σ_N=-32.27 $\sigma_{m,d}$=-557.75 τ=0.00 σ_{max}=-590.01 (sic.=4.439)
Tensioni: σ_N=-32.27 $\sigma_{m,d}$=11.94 τ=42.96 τ_{max}=42.96 (sic.=35.199)
Tensioni: σ_N=-32.27 $\sigma_{m,d}$=-557.75 τ=0.00 $\sigma_{ID,max}$=590.01 (sic.=4.439)

- Verifica a taglio Dir. Y [4.2.16] - CC 58 SLU Xl=0.00 - Classe 1

  Sollecitazioni: T_y=1.78
  V,Ed=1.78 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 58 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=1022.36
  V,Ed=1022.36 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.05 (sic.=20.709)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 63 SLU Xl=0.75 - Classe 1
  Sollecitazioni: N=-1109.58 T_z=767.02 M_y=-1531.13 T_y=-1.84
  My,Ed=-1531.13 My,V,c,Rd=5804.95
  N,Ed=-1109.58 Nc,Rd=-74603.30 YY n=N,Ed/Nc,Rd=0.01 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.26 (sic.=3.791)

Asta n. 1017 (-7 -9) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-913.43 T_z=-360.98 M_y=-669.70 T_y=43.20 M_z=-60.68
  Tensioni: σ_N=-32.07 $\sigma_{m,d}$=-557.76 τ=0.00 σ_{max}=-589.82 (sic.=4.440)
  Tensioni: σ_N=-32.07 $\sigma_{m,d}$=11.94 τ=38.96 τ_{max}=38.96 (sic.=38.817)
  Tensioni: σ_N=-32.07 $\sigma_{m,d}$=-557.76 τ=0.00 $\sigma_{ID,max}$=589.82 (sic.=4.440)

- Verifica a taglio Dir. Y [4.2.16] - CC 91 SLU Xl=0.75 - Classe 1
  Sollecitazioni: T_y=1.58
  V,Ed=1.58 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 91 SLU Xl=0.75 - Classe 1
  Sollecitazioni: T_z=-1038.82
  V,Ed=-1038.82 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.05 (sic.=20.380)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 63 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-1109.58 T_z=-283.72 M_y=-1531.12 T_y=2.34
  My,Ed=-1531.12 My,V,c,Rd=5804.95
  N,Ed=-1109.58 Nc,Rd=-74603.30 YY n=N,Ed/Nc,Rd=0.01 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.26 (sic.=3.791)

Asta n. 1017 (-9 -12) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.72 - Classe 3
  Sollecitazioni: N=-970.18 T_z=-1390.84 M_y=865.82 T_y=15.29 M_z=20.89
  Tensioni: σ_N=-34.06 $\sigma_{m,d}$=-518.91 τ=0.00 σ_{max}=-552.97 (sic.=4.736)
  Tensioni: σ_N=-34.06 $\sigma_{m,d}$=-4.11 τ=150.09 τ_{max}=150.09 (sic.=10.075)
  Tensioni: σ_N=-34.06 $\sigma_{m,d}$=-518.91 τ=0.00 $\sigma_{ID,max}$=552.97 (sic.=4.736)

- Verifica a taglio Dir. Y [4.2.16] - CC 91 SLU Xl=0.72 - Classe 1
  Sollecitazioni: T_y=14.57
  V,Ed=14.57 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 91 SLU Xl=0.72 - Classe 1
  Sollecitazioni: T_z=-2301.09
  V,Ed=-2301.09 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.11 (sic.=9.201)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 63 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-1109.58 T_z=-1560.25 M_y=-1225.22 T_y=6.93
  My,Ed=-1225.22 My,V,c,Rd=5804.95
  N,Ed=-1109.58 Nc,Rd=-74603.30 YY n=N,Ed/Nc,Rd=0.01 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.21 (sic.=4.738)

Asta n. 1017 (-12 129) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.62 - Classe 3
  Sollecitazioni: N=-995.69 T_z=-1660.44 M_y=1443.69 T_y=-383.37 M_z=-202.74
  Tensioni: σ_N=-34.96 $\sigma_{m,d}$=-1454.94 τ=0.00 σ_{max}=-1489.90 (sic.=1.758)
  Tensioni: σ_N=-34.96 $\sigma_{m,d}$=39.87 τ=179.21 τ_{max}=179.21 (sic.=8.438)
  Tensioni: σ_N=-34.96 $\sigma_{m,d}$=-1454.94 τ=0.00 $\sigma_{ID,max}$=1489.90 (sic.=1.758)

- Verifica a taglio Dir. Y [4.2.16] - CC 91 SLU Xl=0.62 - Classe 1
  Sollecitazioni: T_y=-71.04
  V,Ed=-71.04 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 91 SLU Xl=0.62 - Classe 1
  Sollecitazioni: T_z=-3527.06
  V,Ed=-3527.06 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.17 (sic.=6.003)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 86 SLU Xl=0.62 - Classe 1
  Sollecitazioni: N=-2334.80 T_z=-3520.37 M_y=3000.91
  My,Ed=3000.91 My,V,c,Rd=5804.95
  N,Ed=-2334.80 Nc,Rd=-74603.30 YY n=N,Ed/Nc,Rd=0.03 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.52 (sic.=1.934)

Asta n. 1022 (110 -3) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-1541.45 T_z=1752.04 M_y=1489.90 T_y=-381.64 M_z=201.50
  Tensioni: σ_N=-54.11 $\sigma_{m,d}$=-1474.37 τ=0.00 σ_{max}=-1528.48 (sic.=1.714)
  Tensioni: σ_N=-54.11 $\sigma_{m,d}$=-39.63 τ=189.09 τ_{max}=189.09 (sic.=7.997)
  Tensioni: σ_N=-54.11 $\sigma_{m,d}$=-1474.37 τ=0.00 $\sigma_{ID,max}$=1528.48 (sic.=1.714)

- Verifica a taglio Dir. Y [4.2.16] - CC 63 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=-30.84
  V,Ed=-30.84 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 63 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=3787.60
  V,Ed=3787.60 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.18 (sic.=5.590)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 63 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=-2103.04 T_z=3787.60 M_y=3086.91 T_y=-30.84 M_z=10.71
  N,Ed=-2103.04 Nc,Rd=74603.30 n=N,Ed/Nc,Rd=0.03
  Pressoflessione retta YY [4.2.33]:
  My,Ed=3086.91 My,V,c,Rd=5804.95 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.53 (sic.=1.881)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=10.71 Mz,V,c,Rd=1170.59 MNz,c,Rd=1170.59 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.53 (sic.=1.881)

Asta n. 1022 (-3 -5) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-1894.51 T_z=1387.01 M_y=779.38 T_y=19.68 M_z=-22.77
  Tensioni: σ_N=-66.51 $\sigma_{m,d}$=-481.04 τ=0.00 σ_{max}=-547.55 (sic.=4.783)
  Tensioni: σ_N=-66.51 $\sigma_{m,d}$=4.48 τ=149.67 τ_{max}=149.67 (sic.=10.103)
  Tensioni: σ_N=-66.51 $\sigma_{m,d}$=-481.04 τ=0.00 $\sigma_{ID,max}$=547.55 (sic.=4.783)

- Verifica a taglio Dir. Y [4.2.16] - CC 63 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=11.97
  V,Ed=11.97 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 63 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=2479.63
  V,Ed=2479.63 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.12 (sic.=8.538)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 91 SLU Xl=0.72 - Classe 1
  Sollecitazioni: N=-2824.60 T_z=1886.90 M_y=-1214.29 T_y=18.21
  My,Ed=-1214.29 My,V,c,Rd=5804.95
  N,Ed=-2824.60 Nc,Rd=-74603.30 YY n=N,Ed/Nc,Rd=0.04 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.21 (sic.=4.781)

Asta n. 1022 (-5 -8) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.75 - Classe 3
  Sollecitazioni: N=-1510.44 T_z=389.35 M_y=-741.31 T_y=-37.27 M_z=-58.53
  Tensioni: σ_N=-53.03 $\sigma_{m,d}$=-587.03 τ=0.00 σ_{max}=-640.06 (sic.=4.092)
  Tensioni: σ_N=-53.03 $\sigma_{m,d}$=11.51 τ=42.02 τ_{max}=42.02 (sic.=35.989)
  Tensioni: σ_N=-53.03 $\sigma_{m,d}$=-587.03 τ=0.00 $\sigma_{ID,max}$=640.06 (sic.=4.092)

- Verifica a taglio Dir. Z [4.2.16] - CC 63 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=1124.26
  V,Ed=1124.26 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.05 (sic.=18.831)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 91 SLU Xl=0.75 - Classe 1
  Sollecitazioni: N=-2824.60 T_z=516.99 M_y=-1696.31 T_y=1.03
  My,Ed=-1696.31 My,V,c,Rd=5804.95
  N,Ed=-2824.60 Nc,Rd=-74603.30 YY n=N,Ed/Nc,Rd=0.04 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.29 (sic.=3.422)

Asta n. 1022 (-8 -10) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-1500.97 T_z=-343.10 M_y=-741.30 T_y=38.81 M_z=-58.53
  Tensioni: σ_N=-52.69 $\sigma_{m,d}$=-587.03 τ=0.00 σ_{max}=-639.72 (sic.=4.094)
  Tensioni: σ_N=-52.69 $\sigma_{m,d}$=11.51 τ=37.03 τ_{max}=37.03 (sic.=40.840)
  Tensioni: σ_N=-52.69 $\sigma_{m,d}$=-587.03 τ=0.00 $\sigma_{ID,max}$=639.72 (sic.=4.094)

- Verifica a taglio Dir. Z [4.2.16] - CC 86 SLU Xl=0.75 - Classe 1
  Sollecitazioni: T_z=-966.68
  V,Ed=-966.68 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.05 (sic.=21.901)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 91 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-2824.60 T_z=-628.74 M_y=-1696.28
  My,Ed=-1696.28 My,V,c,Rd=5804.95

N,Ed=-2824.60 Nc,Rd=-74603.30 YY n=N,Ed/Nc,Rd=0.04 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.29 (sic.=3.422)

Asta n. 1022 (-10 -13) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-1770.70 T_z=-1175.88 M_y=-770.73 T_y=15.70 M_z=12.77
  Tensioni: σ_N=-62.16 $\sigma_{m,d}$=-441.47 τ=0.00 σ_{max}=-503.63 (sic.=5.200)
  Tensioni: σ_N=-62.16 $\sigma_{m,d}$=-2.51 τ=126.89 τ_{max}=126.89 (sic.=11.917)
  Tensioni: σ_N=-62.16 $\sigma_{m,d}$=-441.47 τ=0.00 $\sigma_{ID,max}$=503.63 (sic.=5.200)

- Verifica a taglio Dir. Y [4.2.16] - CC 86 SLU Xl=0.72 - Classe 1
  Sollecitazioni: T_y=18.22
  V,Ed=18.22 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 86 SLU Xl=0.72 - Classe 1
  Sollecitazioni: T_z=-2322.05
  V,Ed=-2322.05 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.11 (sic.=9.118)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 63 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-2103.04 T_z=-1643.32 M_y=-1376.96 T_y=-16.02 M_z=1.32
  N,Ed=-2103.04 Nc,Rd=74603.30 n=N,Ed/Nc,Rd=0.03
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-1376.96 My,V,c,Rd=5804.95 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.24 (sic.=4.216)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=1.32 Mz,V,c,Rd=1170.59 MNz,c,Rd=1170.59 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.24 (sic.=4.216)

Asta n. 1022 (-13 135) - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.62 - Classe 3
  Sollecitazioni: N=-1529.71 T_z=-1678.48 M_y=1324.85 T_y=358.06 M_z=190.49
  Tensioni: σ_N=-53.70 $\sigma_{m,d}$=-1350.78 τ=0.00 σ_{max}=-1404.48 (sic.=1.865)
  Tensioni: σ_N=-53.70 $\sigma_{m,d}$=-37.46 τ=181.15 τ_{max}=181.15 (sic.=8.347)
  Tensioni: σ_N=-53.70 $\sigma_{m,d}$=-1350.78 τ=0.00 $\sigma_{ID,max}$=1404.48 (sic.=1.865)

- Verifica a taglio Dir. Y [4.2.16] - CC 86 SLU Xl=0.62 - Classe 1
  Sollecitazioni: T_y=-64.99
  V,Ed=-64.99 Vc,Rd=29609.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 86 SLU Xl=0.62 - Classe 1
  Sollecitazioni: T_z=-3630.02
  V,Ed=-3630.02 Vc,Rd=21171.50 V,Ed/Vc,Rd=0.17 (sic.=5.832)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 86 SLU Xl=0.62 - Classe 1
  Sollecitazioni: N=-3240.16 T_z=-3630.02 M_y=2901.45 T_y=-64.99 M_z=-27.68
  N,Ed=-3240.16 Nc,Rd=74603.30 n=N,Ed/Nc,Rd=0.04
  Pressoflessione retta YY [4.2.33]:
  My,Ed=2901.45 My,V,c,Rd=5804.95 MNy,c,Rd=5804.95 My,Ed/MNy,c,Rd=0.50 (sic.=2.001)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-27.68 Mz,V,c,Rd=1170.59 MNz,c,Rd=1170.59 Mz,Ed/MNz,c,Rd=0.02 (sic.=42.296)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.50 (sic.=2.001)

Asta n. 1026 (115 116) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-446.16 T_z=2441.78 M_y=2132.05 T_y=161.18 M_z=-129.41 M_x=-13.19
  Tensioni: σ_N=-9.86 $\sigma_{m,d}$=-852.12 τ=93.65 σ_{max}=-861.98 (sic.=3.038)
  Tensioni: σ_N=-9.86 $\sigma_{m,d}$=4.20 τ=293.45 τ_{max}=293.45 (sic.=5.153)
  Tensioni: σ_N=-9.86 $\sigma_{m,d}$=-852.12 τ=93.65 $\sigma_{ID,max}$=877.11 (sic.=2.986)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 61 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=307.65 M_x=-21.48
  V,Ed=307.65 Vc,Rd,Red=54996.30 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 61 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=2473.63 M_x=-21.48
  V,Ed=2473.63 Vc,Rd,Red=20983.00 V,Ed/Vc,Rd,Red=0.12 (sic.=8.483)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=-1038.84 T_z=2473.63 M_y=2000.81 T_y=307.65 M_z=-120.64 M_x=-21.48
  N,Ed=-1038.84 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=2000.81 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.23 (sic.=4.269)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-120.64 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.03 (sic.=34.008)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.23 (sic.=4.269)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-446.16 My,Ed=2132.05 Mz,Ed=-129.41 L=0.72
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.36 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.43 M,cr=1690360.00 λ_{LT}=0.07
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=4.87 Ncr,y=39594600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=8.02 Ncr,z=14583400.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.26+0.05=0.31 (sic.=3.196)
  Verifica ZZ: 0.00+0.21+0.05=0.26 (sic.=3.843)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 160
  $f_{Z,G}$=0.01 (L/4789) (sic.=15.963)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 160
  $f_{Z,L}$=0.01 (L/4062) (sic.=16.248)

Asta n. 1026 (116 118) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.68 - Classe 3
  Sollecitazioni: N=-308.97 T_z=267.29 M_y=-202.84 T_y=546.15 M_z=308.76 M_x=8.39
  Tensioni: σ_N=-6.83 $\sigma_{m,d}$=-369.62 τ=59.61 σ_{max}=-376.45 (sic.=6.957)
  Tensioni: σ_N=-6.83 $\sigma_{m,d}$=59.31 τ=74.72 τ_{max}=74.72 (sic.=20.237)
  Tensioni: σ_N=-6.83 $\sigma_{m,d}$=-369.62 τ=59.61 $\sigma_{ID,max}$=390.36 (sic.=6.709)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 61 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-83.92 M_x=11.81
  V,Ed=-83.92 Vc,Rd,Red=56072.90 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 61 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=777.27 M_x=11.81
  V,Ed=777.27 Vc,Rd,Red=21393.80 V,Ed/Vc,Rd,Red=0.04 (sic.=27.524)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-1038.84 T_z=777.27 M_y=452.94 T_y=-83.92 M_z=68.21 M_x=11.81
  N,Ed=-1038.84 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=452.94 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.05 (sic.=18.858)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=68.21 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.02 (sic.=60.151)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.05 (sic.=18.858)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-341.56 My,Ed=241.65 Mz,Ed=-313.12 L=0.72
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.36 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.56 M,cr=3028870.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=4.87 Ncr,y=39594600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=8.02 Ncr,z=14583400.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.03+0.11=0.14 (sic.=6.978)
  Verifica ZZ: 0.00+0.02+0.11=0.14 (sic.=7.281)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.00 (L/20866) (sic.=69.553)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.00 (L/19195) (sic.=76.780)

Asta n. 1026 (118 144) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.75 - Classe 3
  Sollecitazioni: N=-208.69 T_z=174.29 M_y=-262.21 T_y=-135.76 M_z=-349.47
  Tensioni: σ_N=-4.61 $\sigma_{m,d}$=-429.48 τ=0.00 σ_{max}=-434.09 (sic.=6.033)
  Tensioni: σ_N=-4.61 $\sigma_{m,d}$=11.34 τ=19.84 τ_{max}=19.84 (sic.=76.201)
  Tensioni: σ_N=-4.61 $\sigma_{m,d}$=-429.48 τ=0.00 $\sigma_{ID,max}$=434.09 (sic.=6.033)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 58 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-4.49 M_x=1.19
  V,Ed=-4.49 Vc,Rd,Red=57232.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 58 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=518.97 M_x=1.19
  V,Ed=518.97 Vc,Rd,Red=21836.00 V,Ed/Vc,Rd,Red=0.02 (sic.=42.075)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 91 SLU Xl=0.75 - Classe 1
  Sollecitazioni: N=494.37 T_z=183.19 M_y=-539.05 T_y=9.84 M_z=-2.87 M_x=1.20
  N,Ed=494.37 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.00

Pressoflessione retta YY [4.2.33]:
My,Ed=-539.05 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.06 (sic.=15.845)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-2.87 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.06 (sic.=15.845)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-208.69 My,Ed=-262.21 Mz,Ed=-349.47 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.38 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.09 M,cr=1202020.00 λ_{LT}=0.08
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=5.03 Ncr,y=36999000.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=8.30 Ncr,z=13627400.00 λ^*_z=0.10 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.12=0.16 (sic.=6.347)
Verifica ZZ: 0.00+0.03+0.12=0.15 (sic.=6.619)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 190
$f_{Z,G}$=0.00 (L/27345) (sic.=91.150)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 190
$f_{Z,L}$=0.00 (L/18357) (sic.=73.428)

Asta n. 1026 (144 123) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-208.69 T_z=-234.52 M_y=-262.23 T_y=159.02 M_z=-349.47
Tensioni: σ_N=-4.61 $\sigma_{m,d}$=-429.48 τ=0.00 σ_{max}=-434.09 (sic.=6.033)
Tensioni: σ_N=-4.61 $\sigma_{m,d}$=11.34 τ=26.70 τ_{max}=26.70 (sic.=56.641)
Tensioni: σ_N=-4.61 $\sigma_{m,d}$=-429.48 τ=0.00 $\sigma_{ID,max}$=434.09 (sic.=6.033)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 91 SLU Xl=0.71 - Classe 1
Sollecitazioni: T_y=17.32 M_x=1.20
V,Ed=17.32 Vc,Rd,Red=57231.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 91 SLU Xl=0.71 - Classe 1
Sollecitazioni: T_z=-531.20 M_x=1.20
V,Ed=-531.20 Vc,Rd,Red=21835.60 V,Ed/Vc,Rd,Red=0.02 (sic.=41.107)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 91 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=494.37 T_z=-389.68 M_y=-539.06 T_y=17.32 M_z=-2.87 M_x=1.20
N,Ed=494.37 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-539.06 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.06 (sic.=15.845)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-2.87 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.06 (sic.=15.845)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-208.69 My,Ed=-262.23 Mz,Ed=-349.47 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.38 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.18 M,cr=1309010.00 λ_{LT}=0.08
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=5.03 Ncr,y=36999000.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=8.30 Ncr,z=13627400.00 λ^*_z=0.10 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.12=0.16 (sic.=6.347)
Verifica ZZ: 0.00+0.03+0.12=0.15 (sic.=6.619)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 210
$f_{Z,L}$=0.00 (L/24177) (sic.=80.590)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 210
$f_{Z,G}$=0.00 (L/16250) (sic.=65.000)

Asta n. 1026 (123 124) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.04 - Classe 3
Sollecitazioni: N=-296.42 T_z=-282.66 M_y=-197.97 T_y=-529.01 M_z=306.28 M_x=-9.05
Tensioni: σ_N=-6.55 $\sigma_{m,d}$=-365.56 τ=64.30 σ_{max}=-372.11 (sic.=7.038)
Tensioni: σ_N=-6.55 $\sigma_{m,d}$=58.04 τ=79.40 τ_{max}=79.40 (sic.=19.044)
Tensioni: σ_N=-6.55 $\sigma_{m,d}$=-365.56 τ=64.30 $\sigma_{ID,max}$=388.42 (sic.=6.743)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 89 SLU Xl=0.68 - Classe 1
Sollecitazioni: T_y=63.70 M_x=-12.72
V,Ed=63.70 Vc,Rd,Red=55972.30 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 89 SLU Xl=0.68 - Classe 1

Sollecitazioni: T_z=-770.75 M_x=-12.72
V,Ed=-770.75 Vc,Rd,Red=21355.40 V,Ed/Vc,Rd,Red=0.04 (sic.=27.707)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.68 - Classe 1
Sollecitazioni: N=-1085.97 T_z=-770.75 M_y=437.69 T_y=63.70 M_z=55.37 M_x=-12.72
N,Ed=-1085.97 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=437.69 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.05 (sic.=19.515)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=55.37 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.01 (sic.=74.098)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.05 (sic.=19.515)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-355.20 My,Ed=256.84 Mz,Ed=-304.65 L=0.72
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.36 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.48 M,cr=2931210.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=4.87 Ncr,y=39594600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=8.02 Ncr,z=14583400.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.11=0.14 (sic.=7.027)
Verifica ZZ: 0.00+0.03+0.11=0.14 (sic.=7.355)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
$f_{Z,L}$=0.00 (L/28539) (sic.=95.130)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 165
$f_{Z,L}$=0.00 (L/22855) (sic.=91.420)

Asta n. 1026 (124 142) - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.62 - Classe 3
Sollecitazioni: N=-454.27 T_z=-2500.49 M_y=2183.96 T_y=151.56 M_z=123.75 M_x=12.54
Tensioni: σ_N=-10.04 $\sigma_{m,d}$=-864.29 τ=89.05 σ_{max}=-874.33 (sic.=2.995)
Tensioni: σ_N=-10.04 $\sigma_{m,d}$=4.02 τ=298.36 τ_{max}=298.36 (sic.=5.068)
Tensioni: σ_N=-10.04 $\sigma_{m,d}$=-864.29 τ=89.05 $\sigma_{ID,max}$=887.83 (sic.=2.950)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 89 SLU Xl=0.62 - Classe 1
Sollecitazioni: T_y=-127.20 M_x=20.57
V,Ed=-127.20 Vc,Rd,Red=55098.70 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 89 SLU Xl=0.62 - Classe 1
Sollecitazioni: T_z=-2643.38 M_x=20.57
V,Ed=-2643.38 Vc,Rd,Red=21022.10 V,Ed/Vc,Rd,Red=0.13 (sic.=7.953)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.62 - Classe 1
Sollecitazioni: N=-1085.97 T_z=-2643.38 M_y=2091.40 T_y=-127.20 M_z=-21.54 M_x=20.57
N,Ed=-1085.97 Nc,Rd=118519.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=2091.40 My,V,c,Rd=8541.33 MNy,c,Rd=8541.33 My,Ed/MNy,c,Rd=0.24 (sic.=4.084)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-21.54 Mz,V,c,Rd=4102.68 MNz,c,Rd=4102.68 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.24 (sic.=4.084)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-454.27 My,Ed=2183.96 Mz,Ed=123.75 L=0.72
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.36 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.43 M,cr=1690340.00 λ_{LT}=0.07
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=4.87 Ncr,y=39594600.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=8.02 Ncr,z=14583400.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.27+0.04=0.32 (sic.=3.151)
Verifica ZZ: 0.00+0.22+0.04=0.26 (sic.=3.796)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 188
$f_{Z,G}$=0.01 (L/6116) (sic.=20.387)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 188
$f_{Z,L}$=0.01 (L/5141) (sic.=20.564)

Asta n. 1027 (118 143) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.09 - Classe 3
Sollecitazioni: N=-184.98 T_z=47.79 M_y=27.19 T_y=135.65 M_z=-62.70 M_x=-1.60
Tensioni: σ_N=-11.26 $\sigma_{m,d}$=-544.66 τ=50.67 σ_{max}=-555.92 (sic.=4.711)
Tensioni: σ_N=-11.26 $\sigma_{m,d}$=60.98 τ=61.29 τ_{max}=61.29 (sic.=24.671)

Tensioni: σ_N=-11.26 $\sigma_{m,d}$=-544.66 τ=50.67 $\sigma_{ID,max}$=562.80 (sic.=4.654)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 33 SLU Xl=0.09 - Classe 1
  Sollecitazioni: T_z=97.31 M_x=-3.68
  V,Ed=97.31 Vc,Rd,Red=11194.40 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 33 SLU Xl=0.09 - Classe 1
  Sollecitazioni: N=30.53 T_z=97.31 M_y=58.47 M_z=2.41 M_x=-3.68
  N,Ed=30.53 Nc,Rd=43021.20 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=58.47 My,V,c,Rd=2320.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.03 (sic.=39.678)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=2.41 Mz,c,Rd=504.58 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=39.678)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-184.98 My,Ed=27.19 Mz,Ed=-62.70 L=0.54
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.54 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.49 M,cr=34116.90 λ_{LT}=0.25
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=9.33 Ncr,y=3907760.00 λ^*_y=0.11 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=32.40 Ncr,z=324311.00 λ^*_z=0.37 Curva b: Φ_z=0.60 χ_z=0.94
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.01+0.18=0.20 (sic.=4.949)
  Verifica ZZ: 0.00+0.01+0.18=0.20 (sic.=5.005)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 175
  $f_{Z,G}$=0.00 (L/51272) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 175
  $f_{Z,G}$=0.00 (L/43521) (sic. >100)

Asta n. 1028 (143 119) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.52 - Classe 3
  Sollecitazioni: N=-157.00 T_z=28.96 M_y=-10.61 T_y=-73.17 M_z=21.92 M_x=4.12
  Tensioni: σ_N=-9.56 $\sigma_{m,d}$=-191.87 τ=130.70 σ_{max}=-201.43 (sic.=13.002)
  Tensioni: σ_N=-9.56 $\sigma_{m,d}$=-22.46 τ=136.26 τ_{max}=136.26 (sic.=11.097)
  Tensioni: σ_N=-9.56 $\sigma_{m,d}$=-191.87 τ=130.70 $\sigma_{ID,max}$=303.01 (sic.=8.643)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 33 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-2.86 M_x=9.69
  V,Ed=-2.86 Vc,Rd,Red=15434.20 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 33 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=80.19 M_x=9.69
  V,Ed=80.19 Vc,Rd,Red=10576.40 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 81 SLU Xl=0.52 - Classe 1
  Sollecitazioni: N=31.67 T_z=71.54 M_y=-25.01 T_y=-2.86 M_x=9.69
  My,Ed=-25.01 My,V,c,Rd=2320.00
  N,Ed=31.67 Nc,Rd=43021.20 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.01 (sic.=92.762)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-157.00 My,Ed=-10.61 Mz,Ed=21.92 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.45 M,cr=47752.90 λ_{LT}=0.21
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=10.14 Ncr,y=3308890.00 λ^*_y=0.12 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=35.21 Ncr,z=274610.00 λ^*_z=0.41 Curva b: Φ_z=0.62 χ_z=0.92
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.00+0.06=0.07 (sic.=13.641)
  Verifica ZZ: 0.00+0.00+0.06=0.07 (sic.=13.771)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 157
  $f_{Z,G}$=0.00 (L/188091) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 157
  $f_{Z,G}$=0.00 (L/188091) (sic. >100)

Asta n. 1030 (119 145) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.06 - Classe 3
  Sollecitazioni: N=-168.65 T_z=-28.55 M_y=-10.90 T_y=44.69 M_z=24.71 M_x=-3.85
  Tensioni: σ_N=-10.27 $\sigma_{m,d}$=-214.88 τ=122.17 σ_{max}=-225.15 (sic.=11.633)
  Tensioni: σ_N=-10.27 $\sigma_{m,d}$=-24.23 τ=125.60 τ_{max}=125.60 (sic.=12.039)
  Tensioni: σ_N=-10.27 $\sigma_{m,d}$=-214.88 τ=122.17 $\sigma_{ID,max}$=308.97 (sic.=8.477)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 17 SLU Xl=0.42 - Classe 1

Sollecitazioni: T_z=-75.77 M_x=-9.08
V,Ed=-75.77 Vc,Rd,Red=10641.30 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 17 SLU Xl=0.42 - Classe 1
Sollecitazioni: T_z=-75.77 M_x=-9.08
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=288.25 τ_{max}=288.25 (sic.=5.246)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=288.25 $\sigma_{ID,max}$=499.26 (sic.=5.246)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-168.65 My,Ed=-10.90 Mz,Ed=24.71 L=0.53
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.53 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.19 M,cr=50251.10 λ_{LT}=0.21
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=9.30 Ncr,y=3937390.00 λ^*_y=0.11 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=32.28 Ncr,z=326771.00 λ^*_z=0.37 Curva b: Φ_z=0.60 χ_z=0.94
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.07=0.08 (sic.=12.205)
Verifica ZZ: 0.00+0.00+0.07=0.08 (sic.=12.320)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 132
$f_{z,G}$=0.00 (L/118681) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 190
$f_{z,G}$=0.00 (L/111994) (sic. >100)

Asta n. 1031 (145 123) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.52 - Classe 3
Sollecitazioni: N=-114.97 T_z=-47.98 M_y=28.84 T_y=-158.98 M_z=-72.00
Tensioni: σ_N=-7.00 $\sigma_{m,d}$=-622.40 τ=0.00 σ_{max}=-629.40 (sic.=4.161)
Tensioni: σ_N=-7.00 $\sigma_{m,d}$=183.51 τ=22.09 τ_{max}=22.09 (sic.=68.464)
Tensioni: σ_N=-7.00 $\sigma_{m,d}$=-622.40 τ=0.00 $\sigma_{ID,max}$=629.40 (sic.=4.161)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 33 SLU Xl=0.52 - Classe 1
Sollecitazioni: T_y=30.47 M_x=2.29
V,Ed=30.47 Vc,Rd,Red=16537.70 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 33 SLU Xl=0.52 - Classe 1
Sollecitazioni: T_z=-97.48 M_x=2.29
V,Ed=-97.48 Vc,Rd,Red=11332.60 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 56 SLU Xl=0.52 - Classe 1
Sollecitazioni: N=-70.31 T_z=-74.30 M_y=45.61 T_y=-57.37 M_z=-21.27 M_x=1.54
N,Ed=-70.31 Nc,Rd=43021.20 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=45.61 My,V,c,Rd=2320.00 MNy,c,Rd=2320.00 My,Ed/MNy,c,Rd=0.02 (sic.=50.864)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-21.27 Mz,V,c,Rd=504.58 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.04 (sic.=23.719)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=23.503)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-114.97 My,Ed=28.84 Mz,Ed=-72.00 L=0.61
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.61 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.56 M,cr=27735.00 λ_{LT}=0.28
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=10.66 Ncr,y=2995410.00 λ^*_y=0.12 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=37.01 Ncr,z=248594.00 λ^*_z=0.43 Curva b: Φ_z=0.63 χ_z=0.92
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.21=0.23 (sic.=4.375)
Verifica ZZ: 0.00+0.01+0.21=0.23 (sic.=4.422)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 132
$f_{z,G}$=0.00 (L/54098) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 132
$f_{z,G}$=0.00 (L/46126) (sic. >100)

Asta n. 2001 (201 202) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.10 - Classe 3
Sollecitazioni: N=278.54 T_z=487.68 M_y=886.78 T_y=212.03 M_z=-242.32
Tensioni: σ_N=3.57 $\sigma_{m,d}$=276.63 τ=0.00 σ_{max}=280.20 (sic.=9.347)
Tensioni: σ_N=3.57 $\sigma_{m,d}$=5.44 τ=31.94 τ_{max}=31.94 (sic.=47.349)
Tensioni: σ_N=3.57 $\sigma_{m,d}$=276.63 τ=0.00 $\sigma_{ID,max}$=280.20 (sic.=9.347)

- Verifica a taglio Dir. Y [4.2.16] - CC 57 SLU Xl=0.10 - Classe 1

Sollecitazioni: T_y=73.27
V,Ed=73.27 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 57 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_z=770.70
V,Ed=770.70 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=48.723)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.10 - Classe 1
Sollecitazioni: N=450.51 T_z=-66.54 M_y=64.05 T_y=413.55 M_z=-425.03 M_x=-25.61
N,Ed=450.51 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=64.05 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.00 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-425.03 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.05 (sic.=18.862)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.05 (sic.=18.857)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-194.26 My,Ed=886.78 Mz,Ed=-242.32 L=0.95
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.47 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.74 M,cr=4726240.00 λ_{LT}=0.06
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=5.56 Ncr,y=52326700.00 λ^*_y=0.06 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=9.38 Ncr,z=18403200.00 λ^*_z=0.11 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.06+0.04=0.10 (sic.=9.872)
Verifica ZZ: 0.00+0.05+0.04=0.09 (sic.=11.111)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 155
$f_{Z,L}$=0.00 (L/41380) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 155
$f_{Z,L}$=0.00 (L/40395) (sic. >100)

Asta n. 2001 (202 -24) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
Sollecitazioni: N=218.64 T_z=-895.81 M_y=-638.50 T_y=186.91 M_z=-55.52
Tensioni: σ_N=2.80 $\sigma_{m,d}$=139.80 τ=0.00 σ_{max}=142.60 (sic.=18.366)
Tensioni: σ_N=2.80 $\sigma_{m,d}$=1.25 τ=58.65 τ_{max}=58.65 (sic.=25.783)
Tensioni: σ_N=2.80 $\sigma_{m,d}$=139.80 τ=0.00 $\sigma_{ID,max}$=142.60 (sic.=18.366)

- Verifica a taglio Dir. Y [4.2.16] - CC 100 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=153.65
V,Ed=153.65 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 100 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_z=640.50
V,Ed=640.50 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=58.628)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 85 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-397.11 T_z=-536.06 M_y=-502.31 T_y=-93.03 M_z=72.75
N,Ed=-397.11 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-502.31 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=33.608)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=72.75 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=33.608)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-147.13 My,Ed=-638.50 Mz,Ed=-55.52 L=0.55
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.28 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.49 M,cr=7570500.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=3.22 Ncr,y=156115000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=5.43 Ncr,z=54905400.00 λ^*_z=0.06 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.01=0.05 (sic.=19.444)
Verifica ZZ: 0.00+0.03+0.01=0.04 (sic.=23.095)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 136
$f_{Z,G}$=0.00 (L/50831) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 184
$f_{Z,L}$=0.00 (L/44477) (sic. >100)

Asta n. 2001 (-24 203) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.31 - Classe 3

Sollecitazioni: N=182.32 T_z=-947.41 M_y=-224.90 T_y=81.85 M_z=66.80
Tensioni: σ_N=2.33 $\sigma_{m,d}$=72.82 τ=0.00 σ_{max}=75.16 (sic.=34.847)
Tensioni: σ_N=2.33 $\sigma_{m,d}$=-1.50 τ=62.02 τ_{max}=62.02 (sic.=24.380)
Tensioni: σ_N=2.33 $\sigma_{m,d}$=1.50 τ=62.02 $\sigma_{ID,max}$=107.49 (sic.=24.365)

- Verifica a taglio Dir. Y [4.2.16] - CC 85 SLU Xl=0.31 - Classe 1
Sollecitazioni: T_y=-77.97
V,Ed=-77.97 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 85 SLU Xl=0.31 - Classe 1
Sollecitazioni: T_z=-626.37
V,Ed=-626.37 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=59.951)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.31 - Classe 1
Sollecitazioni: N=449.46 T_z=243.52 M_y=-110.06 T_y=166.65 M_z=129.84
N,Ed=449.46 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-110.06 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=129.84 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=61.746)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=61.585)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-181.23 My,Ed=-130.82 Mz,Ed=108.20 L=0.35
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.17 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.05 M,cr=13131000.00 λ_{LT}=0.03
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.01 χ_{LT}=1.00
λ_Y=2.05 Ncr,y=385509000.00 λ^*_y=0.02 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=3.45 Ncr,z=135583000.00 λ^*_z=0.04 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.02=0.03 (sic.=34.712)
Verifica ZZ: 0.00+0.01+0.02=0.03 (sic.=36.843)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 184
$f_{Z,L}$=0.00 (L/129604) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 184
$f_{Z,G}$=0.00 (L/108003) (sic. >100)

Asta n. 2001 (203 204) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.36 - Classe 3
Sollecitazioni: N=141.34 T_z=-934.77 M_y=484.53 T_y=-70.12 M_z=90.31
Tensioni: σ_N=1.81 $\sigma_{m,d}$=130.14 τ=0.00 σ_{max}=131.95 (sic.=19.849)
Tensioni: σ_N=1.81 $\sigma_{m,d}$=-2.03 τ=61.19 τ_{max}=61.19 (sic.=24.710)
Tensioni: σ_N=1.81 $\sigma_{m,d}$=130.14 τ=0.00 $\sigma_{ID,max}$=131.95 (sic.=19.849)

- Verifica a taglio Dir. Y [4.2.16] - CC 84 SLU Xl=0.36 - Classe 1
Sollecitazioni: T_y=-112.11
V,Ed=-112.11 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 84 SLU Xl=0.36 - Classe 1
Sollecitazioni: T_z=-628.13
V,Ed=-628.13 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=59.783)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.36 - Classe 1
Sollecitazioni: N=448.70 T_z=-28.61 M_y=-114.68 T_y=77.55 M_z=164.46 M_x=17.32
N,Ed=448.70 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-114.68 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=164.46 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=48.746)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=48.636)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-95.76 My,Ed=484.53 Mz,Ed=90.31 L=0.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.46 M,cr=23656100.00 λ_{LT}=0.03
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.01 χ_{LT}=1.00
λ_Y=2.34 Ncr,y=295156000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=3.95 Ncr,z=103806000.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.02=0.05 (sic.=20.976)
Verifica ZZ: 0.00+0.02+0.02=0.04 (sic.=24.094)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 135
$f_{Z,L}$=0.00 (L/133379) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 135
  $f_{Z,L}$=0.00 (L/133379) (sic. >100)

Asta n. 2001 (204 205) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.65 - Classe 3
  Sollecitazioni: N=108.93 T_z=-541.32 M_y=854.75 T_y=-134.90 M_z=152.29
  Tensioni: σ_N=1.40 $\sigma_{m,d}$=226.07 τ=0.00 σ_{max}=227.46 (sic.=11.514)
  Tensioni: σ_N=1.40 $\sigma_{m,d}$=-3.42 τ=35.44 τ_{max}=35.44 (sic.=42.666)
  Tensioni: σ_N=1.40 $\sigma_{m,d}$=226.07 τ=0.00 $\sigma_{ID,max}$=227.46 (sic.=11.514)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 84 SLU Xl=0.65 - Classe 1
  Sollecitazioni: T_y=-195.65 M_x=4.00
  V,Ed=-195.65 Vc,Rd,Red=99538.20 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 84 SLU Xl=0.65 - Classe 1
  Sollecitazioni: T_z=-473.15 M_x=4.00
  V,Ed=-473.15 Vc,Rd,Red=37439.00 V,Ed/Vc,Rd,Red=0.01 (sic.=79.128)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 84 SLU Xl=0.65 - Classe 1
  Sollecitazioni: N=-319.89 T_z=-473.15 M_y=554.62 T_y=-195.65 M_z=-183.50 M_x=4.00
  N,Ed=-319.89 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=554.62 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=30.439)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-183.50 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=43.688)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=30.439)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-77.35 My,Ed=854.75 Mz,Ed=152.29 L=0.75
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.38 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.20 M,cr=3312440.00 λ_{LT}=0.07
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=4.39 Ncr,y=83955300.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=7.40 Ncr,z=29526900.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.05+0.03=0.08 (sic.=12.139)
  Verifica ZZ: 0.00+0.04+0.03=0.07 (sic.=13.987)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
  $f_{Z,L}$=0.00 (L/47302) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 135
  $f_{Z,L}$=0.00 (L/39911) (sic. >100)

Asta n. 2001 (205 206) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-709.06 T_z=261.11 M_y=359.51 T_y=372.60 M_z=-309.32 M_x=-4.51
  Tensioni: σ_N=-9.08 $\sigma_{m,d}$=-217.51 τ=12.73 σ_{max}=-226.59 (sic.=11.558)
  Tensioni: σ_N=-9.08 $\sigma_{m,d}$=49.23 τ=23.42 τ_{max}=23.42 (sic.=64.564)
  Tensioni: σ_N=-9.08 $\sigma_{m,d}$=-217.51 τ=12.73 $\sigma_{ID,max}$=227.66 (sic.=11.504)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 85 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=-29.93 M_x=-7.31
  V,Ed=-29.93 Vc,Rd,Red=99291.10 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 85 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=620.76 M_x=-7.31
  V,Ed=620.76 Vc,Rd,Red=37346.00 V,Ed/Vc,Rd,Red=0.02 (sic.=60.162)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=1013.41 T_z=130.73 M_y=144.63 T_y=393.73 M_z=-259.28 M_x=-19.33
  N,Ed=1013.41 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=144.63 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-259.28 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.03 (sic.=30.920)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=30.850)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-709.06 My,Ed=359.51 Mz,Ed=-309.32 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.14 M,cr=3606020.00 λ_{LT}=0.07
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=4.10 Ncr,y=96377300.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=6.91 Ncr,z=33895700.00 λ^*_z=0.08 Curva c: Φ_z=0.00 χ_z=1.00

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.06=0.08 (sic.=12.139)
Verifica ZZ: 0.00+0.02+0.06=0.08 (sic.=12.854)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
$f_{z,L}$=0.00 (L/53287) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 203
$f_{z,L}$=0.00 (L/36635) (sic. >100)

Asta n. 2001 (206 207) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.04 - Classe 3
Sollecitazioni: N=-269.82 T_z=608.58 M_y=495.75 T_y=86.00 M_z=-67.93 M_x=-1.63
Tensioni: σ_N=-3.46 $\sigma_{m,d}$=-120.94 τ=4.59 σ_{max}=-124.39 (sic.=21.055)
Tensioni: σ_N=-3.46 $\sigma_{m,d}$=1.53 τ=40.14 τ_{max}=40.14 (sic.=37.669)
Tensioni: σ_N=-3.46 $\sigma_{m,d}$=-120.94 τ=4.59 $\sigma_{ID,max}$=124.65 (sic.=21.012)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 104 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=-21.92 M_x=-4.85
V,Ed=-21.92 Vc,Rd,Red=99474.60 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 104 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_z=479.86 M_x=-4.85
V,Ed=479.86 Vc,Rd,Red=37415.10 V,Ed/Vc,Rd,Red=0.01 (sic.=77.971)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.66 - Classe 1
Sollecitazioni: N=-324.76 T_z=145.33 M_y=-111.43 T_y=-182.27 M_z=-141.56 M_x=5.01
N,Ed=-324.76 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-111.43 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-141.56 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=56.633)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=56.493)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-269.82 My,Ed=495.75 Mz,Ed=-73.31 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.42 M,cr=7652720.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=4.10 Ncr,y=96377300.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=6.91 Ncr,z=33895700.00 λ^*_z=0.08 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.01=0.05 (sic.=21.662)
Verifica ZZ: 0.00+0.03+0.01=0.04 (sic.=25.094)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 135
$f_{z,L}$=0.00 (L/86403) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 135
$f_{z,L}$=0.00 (L/86403) (sic. >100)

Asta n. 2001 (207 208) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.66 - Classe 3
Sollecitazioni: N=-689.59 T_z=243.99 M_y=-166.07 T_y=184.18 M_z=-236.24 M_x=3.09
Tensioni: σ_N=-8.83 $\sigma_{m,d}$=-147.07 τ=8.70 σ_{max}=-155.91 (sic.=16.799)
Tensioni: σ_N=-8.83 $\sigma_{m,d}$=-5.31 τ=18.54 τ_{max}=18.54 (sic.=81.573)
Tensioni: σ_N=-8.83 $\sigma_{m,d}$=-147.07 τ=8.70 $\sigma_{ID,max}$=156.63 (sic.=16.721)

- Verifica a taglio Dir. Y [4.2.16] - CC 84 SLU Xl=0.66 - Classe 1
Sollecitazioni: T_y=-29.37
V,Ed=-29.37 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 84 SLU Xl=0.66 - Classe 1
Sollecitazioni: T_z=-265.90
V,Ed=-265.90 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.66 - Classe 1
Sollecitazioni: N=-1011.87 T_z=-78.58 M_y=-173.95 T_y=-128.12 M_z=-227.61 M_x=-1.88
N,Ed=-1011.87 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-173.95 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic.=97.050)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-227.61 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.03 (sic.=35.221)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=35.090)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-689.59 My,Ed=-166.07 Mz,Ed=-236.24 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.03 M,cr=3246050.00 λ_{LT}=0.07
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=4.10 Ncr,y=96377400.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=6.91 Ncr,z=33895700.00 λ^*_z=0.08 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.01+0.04=0.06 (sic.=17.628)
  Verifica ZZ: 0.00+0.01+0.04=0.05 (sic.=18.311)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
  $f_{Z,G}$=0.00 (L/129604) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{Z,G}$=0.00 (L/76238) (sic. >100)

Asta n. 2001 (208 209) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.66 - Classe 3
  Sollecitazioni: N=718.89 T_z=-383.68 M_y=249.63 T_y=-97.56 M_z=-285.53 M_x=3.70
  Tensioni: σ_N=9.21 $\sigma_{m,d}$=186.35 τ=10.42 σ_{max}=195.56 (sic.=13.393)
  Tensioni: σ_N=9.21 $\sigma_{m,d}$=6.41 τ=27.34 τ_{max}=27.34 (sic.=55.310)
  Tensioni: σ_N=9.21 $\sigma_{m,d}$=186.35 τ=10.42 $\sigma_{ID,max}$=196.39 (sic.=13.336)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 84 SLU Xl=0.66 - Classe 1
  Sollecitazioni: T_y=-23.28 M_x=4.51
  V,Ed=-23.28 Vc,Rd,Red=99500.20 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 84 SLU Xl=0.66 - Classe 1
  Sollecitazioni: T_z=-485.67 M_x=4.51
  V,Ed=-485.67 Vc,Rd,Red=37424.70 V,Ed/Vc,Rd,Red=0.01 (sic.=77.058)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.66 - Classe 1
  Sollecitazioni: N=-1011.48 T_z=-342.11 M_y=37.51 T_y=-21.79 M_z=-247.19 M_x=-8.62
  N,Ed=-1011.48 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=37.51 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.00 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-247.19 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.03 (sic.=32.432)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=32.427)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-681.60 My,Ed=249.63 Mz,Ed=-285.53 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.54 M,cr=8011890.00 λ_{LT}=0.04
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=4.10 Ncr,y=96377200.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=6.91 Ncr,z=33895700.00 λ^*_z=0.08 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.02+0.05=0.07 (sic.=14.097)
  Verifica ZZ: 0.00+0.01+0.05=0.07 (sic.=14.758)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
  $f_{Z,L}$=0.00 (L/99695) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 203
  $f_{Z,L}$=0.00 (L/72002) (sic. >100)

Asta n. 2001 (209 210) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.60 - Classe 3
  Sollecitazioni: N=743.91 T_z=-281.84 M_y=388.44 T_y=-98.66 M_z=-331.60 M_x=4.57
  Tensioni: σ_N=9.53 $\sigma_{m,d}$=233.71 τ=12.89 σ_{max}=243.24 (sic.=10.767)
  Tensioni: σ_N=9.53 $\sigma_{m,d}$=7.45 τ=22.72 τ_{max}=22.72 (sic.=66.543)
  Tensioni: σ_N=9.53 $\sigma_{m,d}$=233.71 τ=12.89 $\sigma_{ID,max}$=244.26 (sic.=10.722)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 105 SLU Xl=0.60 - Classe 1
  Sollecitazioni: T_y=-55.21 M_x=6.92
  V,Ed=-55.21 Vc,Rd,Red=99319.90 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 105 SLU Xl=0.60 - Classe 1
  Sollecitazioni: T_z=-642.65 M_x=6.92
  V,Ed=-642.65 Vc,Rd,Red=37356.90 V,Ed/Vc,Rd,Red=0.02 (sic.=58.129)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-1010.81 T_z=-497.33 M_y=72.01 T_y=14.31 M_z=-247.49 M_x=-15.37
  N,Ed=-1010.81 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:

My,Ed=72.01 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.00 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-247.49 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.03 (sic.=32.393)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=32.374)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-720.32 My,Ed=388.44 Mz,Ed=-331.60 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.16 M,cr=3661410.00 λ_{LT}=0.07
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=4.10 Ncr,y=96377400.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=6.91 Ncr,z=33895700.00 λ^*_z=0.08 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.06=0.09 (sic.=11.324)
Verifica ZZ: 0.00+0.02+0.06=0.08 (sic.=11.996)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
$f_{z,L}$=0.00 (L/65128) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
$f_{z,L}$=0.00 (L/43419) (sic. >100)

Asta n. 2001 (210 211) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.10 - Classe 3
Sollecitazioni: N=-562.97 T_z=317.03 M_y=461.73 T_y=177.69 M_z=-324.56 M_x=-3.69
Tensioni: σ_N=-7.21 $\sigma_{m,d}$=-243.06 τ=10.40 σ_{max}=-250.27 (sic.=10.465)
Tensioni: σ_N=-7.21 $\sigma_{m,d}$=7.29 τ=23.52 τ_{max}=23.52 (sic.=64.277)
Tensioni: σ_N=-7.21 $\sigma_{m,d}$=-243.06 τ=10.40 $\sigma_{ID,max}$=250.92 (sic.=10.438)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 86 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_y=33.47 M_x=17.41
V,Ed=33.47 Vc,Rd,Red=98531.50 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 86 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_z=472.27 M_x=17.41
V,Ed=472.27 Vc,Rd,Red=37060.30 V,Ed/Vc,Rd,Red=0.01 (sic.=78.472)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 104 SLU Xl=0.10 - Classe 1
Sollecitazioni: N=-399.62 T_z=357.35 M_y=568.18 T_y=129.68 M_z=-88.77 M_x=-3.94
N,Ed=-399.62 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=568.18 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=29.712)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-88.77 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic.=90.309)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=29.712)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-562.97 My,Ed=461.73 Mz,Ed=-324.56 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.35 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=3691450.00 λ_{LT}=0.07
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=4.10 Ncr,y=96377400.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=6.91 Ncr,z=33895700.00 λ^*_z=0.08 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.06=0.09 (sic.=10.998)
Verifica ZZ: 0.00+0.02+0.06=0.09 (sic.=11.758)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
$f_{z,L}$=0.00 (L/45089) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 203
$f_{z,L}$=0.00 (L/30059) (sic. >100)

Asta n. 2001 (211 212) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.04 - Classe 3
Sollecitazioni: N=-550.39 T_z=472.70 M_y=288.06 T_y=177.91 M_z=246.17 M_x=-2.70
Tensioni: σ_N=-7.05 $\sigma_{m,d}$=-173.45 τ=7.61 σ_{max}=-180.50 (sic.=14.510)
Tensioni: σ_N=-7.05 $\sigma_{m,d}$=-5.53 τ=32.04 τ_{max}=32.04 (sic.=47.199)
Tensioni: σ_N=-7.05 $\sigma_{m,d}$=-173.45 τ=7.61 $\sigma_{ID,max}$=180.98 (sic.=14.472)

- Verifica a taglio Dir. Y [4.2.16] - CC 104 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=81.70
V,Ed=81.70 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 104 SLU Xl=0.04 - Classe 1

Sollecitazioni: T_z=596.87
V,Ed=596.87 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=62.914)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-778.81 T_z=380.40 M_y=96.28 T_y=102.04 M_z=-171.65 M_x=27.17
N,Ed=-778.81 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=96.28 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-171.65 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=46.706)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=46.635)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-550.39 My,Ed=288.06 Mz,Ed=246.17 L=0.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.63 M,cr=25309300.00 λ_{LT}=0.02
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.01 χ_{LT}=1.00
λ_Y=2.34 Ncr,y=295156000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=3.95 Ncr,z=103806000.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.04=0.07 (sic.=15.242)
Verifica ZZ: 0.00+0.01+0.04=0.06 (sic.=16.145)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
$f_{Z,G}$=0.00 (L/74099) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 155
$f_{Z,L}$=0.00 (L/66689) (sic. >100)

Asta n. 2001 (212 -25) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.04 - Classe 3
Sollecitazioni: N=-558.84 T_z=458.44 M_y=-195.62 T_y=219.67 M_z=190.74 M_x=-2.70
Tensioni: σ_N=-7.16 $\sigma_{m,d}$=-129.55 τ=7.61 σ_{max}=-136.71 (sic.=19.158)
Tensioni: σ_N=-7.16 $\sigma_{m,d}$=-4.28 τ=31.18 τ_{max}=31.18 (sic.=48.501)
Tensioni: σ_N=-7.16 $\sigma_{m,d}$=-129.55 τ=7.61 $\sigma_{ID,max}$=137.34 (sic.=19.070)

- Verifica a taglio Dir. Y [4.2.16] - CC 105 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=78.49
V,Ed=78.49 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 105 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_z=730.67
V,Ed=730.67 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=51.393)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=750.31 T_z=-41.44 M_y=-122.43 T_y=-145.14 M_z=141.01 M_x=-11.53
N,Ed=750.31 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-122.43 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=141.01 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=56.855)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=56.686)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-558.84 My,Ed=-195.62 Mz,Ed=190.74 L=0.30
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.11 M,cr=18986100.00 λ_{LT}=0.03
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.01 χ_{LT}=1.00
λ_Y=1.76 Ncr,y=524719000.00 λ^*_y=0.02 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=2.96 Ncr,z=184542000.00 λ^*_z=0.03 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.03=0.05 (sic.=20.110)
Verifica ZZ: 0.00+0.01+0.03=0.05 (sic.=21.171)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 130
$f_{Z,L}$=0.00 (L/90527) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 130
$f_{Z,G}$=0.00 (L/90527) (sic. >100)

Asta n. 2001 (-25 213) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-563.32 T_z=439.41 M_y=-153.32 T_y=238.61 M_z=142.87 M_x=-2.70
Tensioni: σ_N=-7.21 $\sigma_{m,d}$=-98.23 τ=7.61 σ_{max}=-105.44 (sic.=24.838)
Tensioni: σ_N=-7.21 $\sigma_{m,d}$=-3.21 τ=30.00 τ_{max}=30.00 (sic.=50.403)
Tensioni: σ_N=-7.21 $\sigma_{m,d}$=-98.23 τ=7.61 $\sigma_{ID,max}$=106.27 (sic.=24.646)

- Verifica a taglio Dir. Y [4.2.16] - CC 105 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=77.99
  V,Ed=77.99 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 105 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=688.68
  V,Ed=688.68 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=54.527)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 105 SLU Xl=0.46 - Classe 1
  Sollecitazioni: N=-521.64 T_z=652.10 M_y=-402.06 T_y=77.99 M_z=68.35
  N,Ed=-521.64 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-402.06 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=41.988)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=68.35 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.02 (sic.=41.988)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-563.32 My,Ed=-208.37 Mz,Ed=142.87 L=0.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.25 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.14 M,cr=7025180.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=2.93 Ncr,y=188900000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=4.94 Ncr,z=66435700.00 λ^*_z=0.06 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.01+0.03=0.04 (sic.=23.869)
  Verifica ZZ: 0.00+0.01+0.03=0.04 (sic.=25.484)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 156
  $f_{Z,G}$=0.00 (L/137513) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 156
  $f_{Z,L}$=0.00 (L/96259) (sic. >100)

Asta n. 2001 (213 -26) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.20 - Classe 3
  Sollecitazioni: N=278.98 T_z=-673.31 M_y=-479.08 T_y=-91.49 M_z=75.27
  Tensioni: σ_N=3.57 $\sigma_{m,d}$=121.68 τ=0.00 σ_{max}=125.25 (sic.=20.911)
  Tensioni: σ_N=3.57 $\sigma_{m,d}$=-1.69 τ=44.08 τ_{max}=44.08 (sic.=34.305)
  Tensioni: σ_N=3.57 $\sigma_{m,d}$=121.68 τ=0.00 $\sigma_{ID,max}$=125.25 (sic.=20.911)

- Verifica a taglio Dir. Y [4.2.16] - CC 31 SLU Xl=0.20 - Classe 1
  Sollecitazioni: T_y=-52.99
  V,Ed=-52.99 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 31 SLU Xl=0.20 - Classe 1
  Sollecitazioni: T_z=-399.64
  V,Ed=-399.64 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=93.963)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 105 SLU Xl=0.20 - Classe 1
  Sollecitazioni: N=-521.64 T_z=205.54 M_y=-471.44 T_y=77.99 M_z=87.13
  N,Ed=-521.64 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-471.44 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=35.810)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=87.13 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic.=92.012)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=35.810)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-274.51 My,Ed=-479.08 Mz,Ed=75.27 L=0.20
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.10 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.11 M,cr=42476100.00 λ_{LT}=0.02
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.01 χ_{LT}=1.00
  λ_Y=1.17 Ncr,y=1180610000.00 λ^*_y=0.01 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=1.97 Ncr,z=415219000.00 λ^*_z=0.02 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.03+0.01=0.05 (sic.=21.988)
  Verifica ZZ: 0.00+0.02+0.01=0.04 (sic.=25.396)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 133
  $f_{Z,L}$=0.00 (L/166724) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 119
  $f_{Z,L}$=0.00 (L/111149) (sic. >100)

Asta n. 2001 (-26 214) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.56 - Classe 3
  Sollecitazioni: N=601.69 T_z=-342.84 M_y=-383.12 T_y=-415.18 M_z=287.05 M_x=-2.70
  Tensioni: σ_N=7.71 $\sigma_{m,d}$=210.54 τ=7.61 σ_{max}=218.25 (sic.=12.000)
  Tensioni: σ_N=7.71 $\sigma_{m,d}$=51.51 τ=24.47 τ_{max}=24.47 (sic.=61.782)
  Tensioni: σ_N=7.71 $\sigma_{m,d}$=210.54 τ=7.61 $\sigma_{ID,max}$=218.65 (sic.=11.979)

- Verifica a taglio Dir. Y [4.2.16] - CC 79 SLU Xl=0.56 - Classe 1
  Sollecitazioni: T_y=-93.55
  V,Ed=-93.55 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 79 SLU Xl=0.56 - Classe 1
  Sollecitazioni: T_z=-503.97
  V,Ed=-503.97 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=74.511)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 105 SLU Xl=0.56 - Classe 1
  Sollecitazioni: N=-496.88 T_z=129.22 M_y=-555.95 T_y=93.75 M_z=139.59
  N,Ed=-496.88 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-555.95 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=30.366)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=139.59 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=57.433)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=30.366)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-588.08 My,Ed=-383.12 Mz,Ed=287.05 L=0.60
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.30 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.15 M,cr=4935120.00 λ_{LT}=0.06
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.51 Ncr,y=131180000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=5.92 Ncr,z=46135900.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.02+0.05=0.08 (sic.=12.618)
  Verifica ZZ: 0.00+0.02+0.05=0.07 (sic.=13.446)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 156
  $f_{Z,L}$=0.00 (L/55824) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 204
  $f_{Z,G}$=0.00 (L/41868) (sic. >100)

Asta n. 2001 (214 215) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=-646.36 T_z=-269.73 M_y=361.19 T_y=436.98 M_z=609.05 M_x=-2.67
  Tensioni: σ_N=-8.28 $\sigma_{m,d}$=-367.42 τ=7.52 σ_{max}=-375.70 (sic.=6.971)
  Tensioni: σ_N=-8.28 $\sigma_{m,d}$=28.80 τ=20.82 τ_{max}=20.82 (sic.=72.618)
  Tensioni: σ_N=-8.28 $\sigma_{m,d}$=-367.42 τ=7.52 $\sigma_{ID,max}$=375.92 (sic.=6.967)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 67 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_y=-206.51 M_x=20.08
  V,Ed=-206.51 Vc,Rd,Red=98329.90 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 67 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-909.28 M_x=20.08
  V,Ed=-909.28 Vc,Rd,Red=36984.50 V,Ed/Vc,Rd,Red=0.02 (sic.=40.674)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=730.98 T_z=124.49 M_y=-23.18 T_y=-483.34 M_z=-583.86 M_x=33.59
  N,Ed=730.98 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-23.18 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.00 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-583.86 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.07 (sic.=13.731)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.07 (sic.=13.730)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-600.05 My,Ed=-385.62 Mz,Ed=-621.10 L=0.80
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.10 M,cr=2669170.00 λ_{LT}=0.08
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=4.68 Ncr,y=73788800.00 λ^*_y=0.05 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=7.90 Ncr,z=25951400.00 λ^*_z=0.09 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.02+0.11=0.14 (sic.=7.145)
  Verifica ZZ: 0.00+0.02+0.11=0.14 (sic.=7.404)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 155
  $f_{z,L}$=0.00 (L/41879) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 155
  $f_{z,L}$=0.00 (L/36369) (sic. >100)

Asta n. 2012 (225 226) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-267.51 T_z=690.94 M_y=1010.04 T_y=128.40 M_z=-198.00
  Tensioni: σ_N=-3.43 $\sigma_{m,d}$=-276.15 τ=0.00 σ_{max}=-279.57 (sic.=9.368)
  Tensioni: σ_N=-3.43 $\sigma_{m,d}$=4.45 τ=45.23 τ_{max}=45.23 (sic.=33.429)
  Tensioni: σ_N=-3.43 $\sigma_{m,d}$=-276.15 τ=0.00 $\sigma_{ID,max}$=279.57 (sic.=9.368)

- Verifica a taglio Dir. Y [4.2.16] - CC 79 SLU Xl=1.96 - Classe 1
  Sollecitazioni: T_y=26.83
  V,Ed=26.83 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 79 SLU Xl=1.96 - Classe 1
  Sollecitazioni: T_z=-482.72
  V,Ed=-482.72 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=77.792)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=345.22 T_z=18.02 M_y=68.16 T_y=-245.98 M_z=334.70 M_x=2.79
  N,Ed=345.22 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=68.16 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.00 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=334.70 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.04 (sic.=23.952)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=23.943)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-267.51 My,Ed=1010.04 Mz,Ed=-198.00 L=2.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.37 M,cr=555255.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.71 Ncr,y=11806200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=19.74 Ncr,z=4152220.00 λ^*_z=0.23 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.06+0.04=0.10 (sic.=9.853)
  Verifica ZZ: 0.00+0.05+0.04=0.09 (sic.=11.281)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
  $f_{z,L}$=0.01 (L/28115) (sic.=93.717)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 203
  $f_{z,L}$=0.01 (L/21711) (sic.=86.844)

Asta n. 2012 (226 228) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.56 - Classe 3
  Sollecitazioni: N=240.96 T_z=-1004.11 M_y=1031.90 T_y=-143.28 M_z=-149.95
  Tensioni: σ_N=3.09 $\sigma_{m,d}$=256.00 τ=0.00 σ_{max}=259.09 (sic.=10.109)
  Tensioni: σ_N=3.09 $\sigma_{m,d}$=3.37 τ=65.73 τ_{max}=65.73 (sic.=23.003)
  Tensioni: σ_N=3.09 $\sigma_{m,d}$=256.00 τ=0.00 $\sigma_{ID,max}$=259.09 (sic.=10.109)

- Verifica a taglio Dir. Y [4.2.16] - CC 84 SLU Xl=0.56 - Classe 1
  Sollecitazioni: T_y=61.33
  V,Ed=61.33 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 84 SLU Xl=0.56 - Classe 1
  Sollecitazioni: T_z=-766.84
  V,Ed=-766.84 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=48.969)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 84 SLU Xl=0.56 - Classe 1
  Sollecitazioni: N=-217.35 T_z=-766.84 M_y=810.64 T_y=61.33 M_z=26.49
  N,Ed=-217.35 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=810.64 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.05 (sic.=20.825)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=26.49 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.05 (sic.=20.825)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-200.98 My,Ed=1031.90 Mz,Ed=-149.95 L=0.60
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.30 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.30 M,cr=5573390.00 λ_{LT}=0.05

$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=3.51 Ncr,y=131180000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=5.92 Ncr,z=46135800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.07+0.03=0.09 (sic.=10.656)
Verifica ZZ: 0.00+0.05+0.03=0.08 (sic.=12.391)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 150
$f_{Z,L}$=0.00 (L/78269) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
$f_{Z,L}$=0.00 (L/35347) (sic. >100)

Asta n. 2012 (228 229) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.30 - Classe 3
Sollecitazioni: N=242.24 T_z=-696.79 M_y=1263.81 T_y=-143.28 M_z=-198.75
Tensioni: σ_N=3.10 $\sigma_{m,d}$=321.07 τ=0.00 σ_{max}=324.17 (sic.=8.079)
Tensioni: σ_N=3.10 $\sigma_{m,d}$=4.46 τ=45.62 τ_{max}=45.62 (sic.=33.147)
Tensioni: σ_N=3.10 $\sigma_{m,d}$=321.07 τ=0.00 $\sigma_{ID,max}$=324.17 (sic.=8.079)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 114 SLU Xl=0.30 - Classe 1
Sollecitazioni: T_y=84.42 M_x=14.48
V,Ed=84.42 Vc,Rd,Red=98752.20 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 114 SLU Xl=0.30 - Classe 1
Sollecitazioni: T_z=-838.44 M_x=14.48
V,Ed=-838.44 Vc,Rd,Red=37143.30 V,Ed/Vc,Rd,Red=0.02 (sic.=44.300)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 84 SLU Xl=0.30 - Classe 1
Sollecitazioni: N=-219.52 T_z=-785.22 M_y=1074.56 T_y=61.32 M_z=47.41
N,Ed=-219.52 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=1074.56 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=15.710)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=47.41 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.06 (sic.=15.710)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-202.69 My,Ed=1263.81 Mz,Ed=-198.75 L=0.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.06 M,cr=10232700.00 λ_{LT}=0.04
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=2.34 Ncr,y=295155000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=3.95 Ncr,z=103806000.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.08+0.04=0.12 (sic.=8.514)
Verifica ZZ: 0.00+0.06+0.04=0.10 (sic.=9.866)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 150
$f_{Z,L}$=0.00 (L/60351) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
$f_{Z,L}$=0.00 (L/24689) (sic.=98.756)

Asta n. 2012 (229 230) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.10 - Classe 3
Sollecitazioni: N=-808.40 T_z=408.50 M_y=1080.93 T_y=-247.38 M_z=258.24 M_x=7.30
Tensioni: σ_N=-10.35 $\sigma_{m,d}$=-318.66 τ=20.59 σ_{max}=-329.02 (sic.=7.960)
Tensioni: σ_N=-10.35 $\sigma_{m,d}$=121.34 τ=34.37 τ_{max}=34.37 (sic.=43.989)
Tensioni: σ_N=-10.35 $\sigma_{m,d}$=-318.66 τ=20.59 $\sigma_{ID,max}$=330.94 (sic.=7.914)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 31 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_y=-16.80 M_x=7.96
V,Ed=-16.80 Vc,Rd,Red=99241.90 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 31 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_z=517.12 M_x=7.96
V,Ed=517.12 Vc,Rd,Red=37327.60 V,Ed/Vc,Rd,Red=0.01 (sic.=72.184)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 99 SLU Xl=0.10 - Classe 1
Sollecitazioni: N=-164.66 T_z=104.47 M_y=1516.21 T_y=-22.01 M_z=28.66 M_x=9.26
N,Ed=-164.66 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=1516.21 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.09 (sic.=11.134)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=28.66 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.09 (sic.=11.134)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-808.40 My,Ed=1086.45 Mz,Ed=258.24 L=0.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.00 M,cr=9639200.00 λ_{LT}=0.04
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=2.34 Ncr,y=295155000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=3.95 Ncr,z=103806000.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.07+0.05=0.12 (sic.=8.340)
  Verifica ZZ: 0.00+0.06+0.05=0.11 (sic.=9.428)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 198
  $f_{Z,L}$=0.00 (L/61400) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 196
  $f_{Z,L}$=0.00 (L/15350) (sic.=61.400)

Asta n. 2012 (230 231) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-664.46 T_z=1114.93 M_y=1358.03 T_y=-90.86 M_z=115.40 M_x=6.65
  Tensioni: σ_N=-8.51 $\sigma_{m,d}$=-296.01 τ=18.75 σ_{max}=-304.52 (sic.=8.601)
  Tensioni: σ_N=-8.51 $\sigma_{m,d}$=-2.59 τ=75.44 τ_{max}=75.44 (sic.=20.043)
  Tensioni: σ_N=-8.51 $\sigma_{m,d}$=-296.01 τ=18.75 $\sigma_{ID,max}$=306.25 (sic.=8.552)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 104 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-32.47 M_x=9.50
  V,Ed=-32.47 Vc,Rd,Red=99127.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 104 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=1247.08 M_x=9.50
  V,Ed=1247.08 Vc,Rd,Red=37284.30 V,Ed/Vc,Rd,Red=0.03 (sic.=29.897)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 99 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-164.66 T_z=1195.73 M_y=1444.75 T_y=-22.01 M_z=21.26 M_x=9.26
  N,Ed=-164.66 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=1444.75 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.09 (sic.=11.685)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=21.26 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.09 (sic.=11.685)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-664.46 My,Ed=1358.03 Mz,Ed=115.40 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.26 M,cr=5050050.00 λ_{LT}=0.06
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=3.63 Ncr,y=122854000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.09+0.02=0.11 (sic.=9.039)
  Verifica ZZ: 0.00+0.07+0.02=0.09 (sic.=10.714)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 198
  $f_{Z,G}$=0.00 (L/47798) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 198
  $f_{Z,L}$=0.00 (L/13656) (sic.=54.624)

Asta n. 2012 (231 232) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-629.86 T_z=812.15 M_y=689.10 T_y=-90.36 M_z=73.73 M_x=6.65
  Tensioni: σ_N=-8.07 $\sigma_{m,d}$=-157.77 τ=18.75 σ_{max}=-165.84 (sic.=15.793)
  Tensioni: σ_N=-8.07 $\sigma_{m,d}$=-1.66 τ=56.49 τ_{max}=56.49 (sic.=26.767)
  Tensioni: σ_N=-8.07 $\sigma_{m,d}$=-157.77 τ=18.75 $\sigma_{ID,max}$=168.99 (sic.=15.498)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 97 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-22.77 M_x=9.69
  V,Ed=-22.77 Vc,Rd,Red=99112.30 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 97 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=1097.33 M_x=9.69
  V,Ed=1097.33 Vc,Rd,Red=37278.80 V,Ed/Vc,Rd,Red=0.03 (sic.=33.972)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 99 SLU Xl=0.04 - Classe 1

Sollecitazioni: N=-164.66 T_z=1067.08 M_y=721.61 T_y=-22.01 M_z=7.62 M_x=9.26
N,Ed=-164.66 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=721.61 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.04 (sic.=23.395)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=7.62 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=23.395)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-784.15 My,Ed=513.90 Mz,Ed=138.21 L=0.62
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.51 M,cr=6049130.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=3.63 Ncr,y=122854000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.03=0.06 (sic.=16.237)
Verifica ZZ: 0.00+0.03+0.03=0.06 (sic.=18.167)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 198
$f_{Z,L}$=0.00 (L/76476) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 198
$f_{Z,L}$=0.00 (L/27313) (sic. >100)

Asta n. 2012 (232 233) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.58 - Classe 3
Sollecitazioni: N=-677.20 T_z=569.99 M_y=-404.38 T_y=-175.99 M_z=-233.88 M_x=7.46
Tensioni: σ_N=-8.67 $\sigma_{m,d}$=-187.73 τ=21.05 σ_{max}=-196.40 (sic.=13.335)
Tensioni: σ_N=-8.67 $\sigma_{m,d}$=5.25 τ=43.18 τ_{max}=43.18 (sic.=35.020)
Tensioni: σ_N=-8.67 $\sigma_{m,d}$=-187.73 τ=21.05 $\sigma_{ID,max}$=199.76 (sic.=13.111)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 97 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=-22.77 M_x=9.69
V,Ed=-22.77 Vc,Rd,Red=99112.30 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 97 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_z=953.88 M_x=9.69
V,Ed=953.88 Vc,Rd,Red=37278.80 V,Ed/Vc,Rd,Red=0.03 (sic.=39.081)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 82 SLU Xl=0.58 - Classe 1
Sollecitazioni: N=-335.14 T_z=813.59 M_y=-588.84 T_y=-41.28 M_z=-33.83 M_x=9.99
N,Ed=-335.14 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-588.84 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=28.670)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-33.83 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=28.670)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-677.20 My,Ed=-404.38 Mz,Ed=-233.88 L=0.62
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.38 M,cr=5529900.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=3.63 Ncr,y=122853000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.04=0.07 (sic.=14.003)
Verifica ZZ: 0.00+0.02+0.04=0.07 (sic.=15.091)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 135
$f_{Z,L}$=0.00 (L/163878) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 167
$f_{Z,L}$=0.00 (L/57357) (sic. >100)

Asta n. 2012 (233 234) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
Sollecitazioni: N=-759.58 T_z=504.37 M_y=-625.22 T_y=-161.22 M_z=-316.85 M_x=7.30
Tensioni: σ_N=-9.73 $\sigma_{m,d}$=-267.92 τ=20.59 σ_{max}=-277.64 (sic.=9.433)
Tensioni: σ_N=-9.73 $\sigma_{m,d}$=7.12 τ=39.24 τ_{max}=39.24 (sic.=38.535)
Tensioni: σ_N=-9.73 $\sigma_{m,d}$=-267.92 τ=20.59 $\sigma_{ID,max}$=279.93 (sic.=9.356)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 97 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=-22.77 M_x=9.69
V,Ed=-22.77 Vc,Rd,Red=99112.30 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 97 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=841.24 M_x=9.69
  V,Ed=841.24 Vc,Rd,Red=37278.80 V,Ed/Vc,Rd,Red=0.02 (sic.=44.314)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 82 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-335.14 T_z=697.03 M_y=-1038.76 T_y=-41.28 M_z=-59.42 M_x=9.99
  N,Ed=-335.14 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-1038.76 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=16.252)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-59.42 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.252)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-759.58 My,Ed=-625.22 Mz,Ed=-316.85 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.18 M,cr=4738420.00 λ_{LT}=0.06
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=3.63 Ncr,y=122854000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.04+0.06=0.10 (sic.=9.910)
  Verifica ZZ: 0.00+0.03+0.06=0.09 (sic.=10.759)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 181
  $f_{z,L}$=0.00 (L/114714) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{z,L}$=0.00 (L/25492) (sic. >100)

Asta n. 2012 (234 236) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-747.41 T_z=412.22 M_y=-854.96 T_y=-128.77 M_z=-391.11 M_x=7.30
  Tensioni: σ_N=-9.57 $\sigma_{m,d}$=-345.32 τ=20.59 σ_{max}=-354.89 (sic.=7.380)
  Tensioni: σ_N=-9.57 $\sigma_{m,d}$=8.79 τ=34.24 τ_{max}=34.24 (sic.=44.159)
  Tensioni: σ_N=-9.57 $\sigma_{m,d}$=-345.32 τ=20.59 $\sigma_{ID,max}$=356.68 (sic.=7.343)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 97 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-22.77 M_x=9.69
  V,Ed=-22.77 Vc,Rd,Red=99112.30 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 97 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=710.57 M_x=9.69
  V,Ed=710.57 Vc,Rd,Red=37278.80 V,Ed/Vc,Rd,Red=0.02 (sic.=52.464)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 102 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-394.24 T_z=660.85 M_y=-1440.61 T_y=-33.23 M_z=-53.27 M_x=9.93
  N,Ed=-394.24 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-1440.61 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.09 (sic.=11.719)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-53.27 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.09 (sic.=11.719)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-747.41 My,Ed=-854.96 Mz,Ed=-391.11 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.13 M,cr=4519530.00 λ_{LT}=0.06
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=3.63 Ncr,y=122854000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.05+0.07=0.13 (sic.=7.756)
  Verifica ZZ: 0.00+0.04+0.07=0.12 (sic.=8.472)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
  $f_{z,L}$=0.00 (L/71696) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{z,L}$=0.00 (L/16157) (sic.=64.628)

Asta n. 2012 (236 237) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-700.14 T_z=-208.35 M_y=-864.62 T_y=210.77 M_z=-388.20 M_x=-6.93

Tensioni: σ_N=-8.97 $\sigma_{m,d}$=-345.56 τ=19.56 σ_{max}=-354.53 (sic.=7.387)
Tensioni: σ_N=-8.97 $\sigma_{m,d}$=-92.98 τ=25.46 τ_{max}=25.46 (sic.=59.390)
Tensioni: σ_N=-8.97 $\sigma_{m,d}$=-345.56 τ=19.56 $\sigma_{ID,max}$=356.14 (sic.=7.354)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 82 SLU Xl=0.36 - Classe 1
Sollecitazioni: T_y=73.77 M_x=-9.48
V,Ed=73.77 Vc,Rd,Red=99128.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 82 SLU Xl=0.36 - Classe 1
Sollecitazioni: T_z=-405.95 M_x=-9.48
V,Ed=-405.95 Vc,Rd,Red=37284.70 V,Ed/Vc,Rd,Red=0.01 (sic.=91.845)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 102 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-366.12 T_z=-294.87 M_y=-1451.42 T_y=32.15 M_z=-52.06 M_x=-9.51
N,Ed=-366.12 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-1451.42 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.09 (sic.=11.631)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-52.06 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.09 (sic.=11.631)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-700.14 My,Ed=-864.62 Mz,Ed=-388.20 L=0.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.01 M,cr=9749450.00 λ_{LT}=0.04
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=2.34 Ncr,y=295155000.00 λ^*_y=0.03 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=3.95 Ncr,z=103806000.00 λ^*_z=0.05 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.06+0.07=0.13 (sic.=7.765)
Verifica ZZ: 0.00+0.04+0.07=0.12 (sic.=8.491)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 196
$f_{z,L}$=0.00 (L/76197) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 211
$f_{z,L}$=0.00 (L/18047) (sic.=72.188)

Asta n. 2012 (237 238) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.04 - Classe 3
Sollecitazioni: N=-702.79 T_z=-277.44 M_y=-830.77 T_y=241.86 M_z=-305.83 M_x=-6.93
Tensioni: σ_N=-9.00 $\sigma_{m,d}$=-298.50 τ=19.56 σ_{max}=-307.50 (sic.=8.517)
Tensioni: σ_N=-9.00 $\sigma_{m,d}$=-90.85 τ=28.13 τ_{max}=28.13 (sic.=53.756)
Tensioni: σ_N=-9.00 $\sigma_{m,d}$=-298.50 τ=19.56 $\sigma_{ID,max}$=309.36 (sic.=8.466)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 82 SLU Xl=0.58 - Classe 1
Sollecitazioni: T_y=73.77 M_x=-9.48
V,Ed=73.77 Vc,Rd,Red=99128.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 82 SLU Xl=0.58 - Classe 1
Sollecitazioni: T_z=-510.43 M_x=-9.48
V,Ed=-510.43 Vc,Rd,Red=37284.70 V,Ed/Vc,Rd,Red=0.01 (sic.=73.046)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 102 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-366.12 T_z=-382.11 M_y=-1325.07 T_y=32.15 M_z=-39.21 M_x=-9.51
N,Ed=-366.12 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-1325.07 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.08 (sic.=12.740)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-39.21 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=12.740)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-702.79 My,Ed=-830.77 Mz,Ed=-305.83 L=0.62
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.05 M,cr=4203460.00 λ_{LT}=0.06
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=3.63 Ncr,y=122854000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.05+0.06=0.11 (sic.=8.951)
Verifica ZZ: 0.00+0.04+0.06=0.10 (sic.=9.887)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
$f_{z,L}$=0.00 (L/63730) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201

$f_{Z,L}$=0.00 (L/14162) (sic.=56.648)

Asta n. 2012 (238 239) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-707.91 T_z=-364.99 M_y=-736.12 T_y=279.19 M_z=-164.27 M_x=-6.93
  Tensioni: σ_N=-9.07 $\sigma_{m,d}$=-211.23 τ=19.56 σ_{max}=-220.29 (sic.=11.889)
  Tensioni: σ_N=-9.07 $\sigma_{m,d}$=-82.89 τ=31.99 τ_{max}=31.99 (sic.=47.261)
  Tensioni: σ_N=-9.07 $\sigma_{m,d}$=-211.23 τ=19.56 $\sigma_{ID,max}$=222.88 (sic.=11.751)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 82 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=73.77 M_x=-9.48
  V,Ed=73.77 Vc,Rd,Red=99128.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 82 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-629.73 M_x=-9.48
  V,Ed=-629.73 Vc,Rd,Red=37284.70 V,Ed/Vc,Rd,Red=0.02 (sic.=59.208)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 102 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-366.12 T_z=-502.33 M_y=-1070.26 T_y=32.15 M_z=-19.29 M_x=-9.51
  N,Ed=-366.12 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-1070.26 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=15.774)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-19.29 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=15.774)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-707.91 My,Ed=-736.12 Mz,Ed=-164.27 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.09 M,cr=4368790.00 λ_{LT}=0.06
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.63 Ncr,y=122853000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.05+0.03=0.08 (sic.=12.486)
  Verifica ZZ: 0.00+0.04+0.03=0.07 (sic.=14.142)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 196
  $f_{Z,L}$=0.00 (L/76476) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
  $f_{Z,G}$=0.00 (L/17924) (sic.=71.696)

Asta n. 2012 (239 240) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-443.74 T_z=-567.07 M_y=-675.61 T_y=143.06 M_z=126.11 M_x=-6.48
  Tensioni: σ_N=-5.68 $\sigma_{m,d}$=-181.55 τ=18.28 σ_{max}=-187.24 (sic.=13.988)
  Tensioni: σ_N=-5.68 $\sigma_{m,d}$=-2.83 τ=41.63 τ_{max}=41.63 (sic.=36.326)
  Tensioni: σ_N=-5.68 $\sigma_{m,d}$=-181.55 τ=18.28 $\sigma_{ID,max}$=189.89 (sic.=13.792)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 82 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=73.77 M_x=-9.48
  V,Ed=73.77 Vc,Rd,Red=99128.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 82 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-731.91 M_x=-9.48
  V,Ed=-731.91 Vc,Rd,Red=37284.70 V,Ed/Vc,Rd,Red=0.02 (sic.=50.942)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 99 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-152.28 T_z=-532.99 M_y=-766.41 T_y=43.52 M_z=26.92 M_x=-9.14
  N,Ed=-152.28 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-766.41 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.05 (sic.=22.027)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=26.92 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.05 (sic.=22.027)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-713.19 My,Ed=-587.33 Mz,Ed=199.62 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.16 M,cr=4663090.00 λ_{LT}=0.06
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.63 Ncr,y=122854000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95

Verifica YY: 0.00+0.04+0.04=0.08 (sic.=12.980)
Verifica ZZ: 0.00+0.03+0.04=0.07 (sic.=14.377)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 169
$f_{Z,L}$=0.00 (L/95595) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 169
$f_{Z,L}$=0.00 (L/25492) (sic. >100)

Asta n. 2012 (240 241) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.58 - Classe 3
Sollecitazioni: N=-751.71 T_z=-710.71 M_y=437.21 T_y=318.54 M_z=406.12 M_x=-6.86
Tensioni: σ_N=-9.63 $\sigma_{m,d}$=-279.47 τ=19.35 σ_{max}=-289.10 (sic.=9.059)
Tensioni: σ_N=-9.63 $\sigma_{m,d}$=-9.12 τ=50.87 τ_{max}=50.87 (sic.=29.724)
Tensioni: σ_N=-9.63 $\sigma_{m,d}$=-279.47 τ=19.35 $\sigma_{ID,max}$=291.04 (sic.=8.999)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 84 SLU Xl=0.58 - Classe 1
Sollecitazioni: T_y=94.29 M_x=-9.04
V,Ed=94.29 Vc,Rd,Red=99160.80 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 84 SLU Xl=0.58 - Classe 1
Sollecitazioni: T_z=-1011.23 M_x=-9.04
V,Ed=-1011.23 Vc,Rd,Red=37297.00 V,Ed/Vc,Rd,Red=0.03 (sic.=36.883)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.58 - Classe 1
Sollecitazioni: N=319.77 T_z=-817.38 M_y=198.40 T_y=327.05 M_z=395.45 M_x=-39.34
N,Ed=319.77 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=198.40 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic.=85.090)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=395.45 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.05 (sic.=20.273)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.05 (sic.=20.216)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-751.71 My,Ed=437.21 Mz,Ed=406.12 L=0.62
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.73 M,cr=10958100.00 λ_{LT}=0.04
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=3.63 Ncr,y=122854000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.03+0.07=0.11 (sic.=9.518)
Verifica ZZ: 0.00+0.02+0.07=0.10 (sic.=10.051)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 167
$f_{Z,L}$=0.00 (L/88242) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 150
$f_{Z,L}$=0.00 (L/52143) (sic. >100)

Asta n. 2012 (241 242) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.52 - Classe 3
Sollecitazioni: N=-724.02 T_z=-632.20 M_y=713.53 T_y=391.43 M_z=631.63 M_x=-6.93
Tensioni: σ_N=-9.27 $\sigma_{m,d}$=-440.55 τ=19.56 σ_{max}=-449.82 (sic.=5.822)
Tensioni: σ_N=-9.27 $\sigma_{m,d}$=-14.19 τ=46.43 τ_{max}=46.43 (sic.=32.565)
Tensioni: σ_N=-9.27 $\sigma_{m,d}$=-440.55 τ=19.56 $\sigma_{ID,max}$=451.09 (sic.=5.806)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 77 SLU Xl=0.52 - Classe 1
Sollecitazioni: T_y=92.39 M_x=-9.53
V,Ed=92.39 Vc,Rd,Red=99124.20 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 77 SLU Xl=0.52 - Classe 1
Sollecitazioni: T_z=-955.34 M_x=-9.53
V,Ed=-955.34 Vc,Rd,Red=37283.30 V,Ed/Vc,Rd,Red=0.03 (sic.=39.026)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.52 - Classe 1
Sollecitazioni: N=319.77 T_z=-892.75 M_y=681.74 T_y=377.97 M_z=604.25 M_x=-48.59
N,Ed=319.77 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=681.74 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.04 (sic.=24.763)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=604.25 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.08 (sic.=13.268)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=12.986)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-724.02 My,Ed=713.53 Mz,Ed=631.63 L=0.62

αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.24 M,cr=4978740.00 λ_{LT}=0.06
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=3.63 Ncr,y=122854000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=6.12 Ncr,z=43207300.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.05+0.11=0.16 (sic.=6.121)
Verifica ZZ: 0.00+0.04+0.11=0.15 (sic.=6.482)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
$f_{z,L}$=0.00 (L/50699) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 167
$f_{z,L}$=0.00 (L/22043) (sic.=88.172)

Asta n. 2013 (201 220) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.10 - Classe 3
Sollecitazioni: N=764.63 T_z=669.92 M_y=772.05 T_y=-104.38 M_z=172.07
Tensioni: σ_N=9.79 $\sigma_{m,d}$=221.42 τ=0.00 σ_{max}=231.22 (sic.=11.327)
Tensioni: σ_N=9.79 $\sigma_{m,d}$=-3.86 τ=43.86 τ_{max}=43.86 (sic.=34.478)
Tensioni: σ_N=9.79 $\sigma_{m,d}$=221.42 τ=0.00 $\sigma_{ID,max}$=231.22 (sic.=11.327)

- Verifica a taglio Dir. Y [4.2.16] - CC 63 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_y=-37.19
V,Ed=-37.19 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 63 SLU Xl=0.10 - Classe 1
Sollecitazioni: T_z=1067.91
V,Ed=1067.91 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.03 (sic.=35.163)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 63 SLU Xl=2.14 - Classe 1
Sollecitazioni: N=906.88 T_z=864.40 M_y=-999.92 T_y=-37.19 M_z=15.62
N,Ed=906.88 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-999.92 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=16.883)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=15.62 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.883)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
$f_{z,L}$=0.01 (L/26573) (sic.=88.577)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
$f_{z,L}$=0.01 (L/19358) (sic.=77.432)

Asta n. 2013 (220 225) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=2.10 - Classe 3
Sollecitazioni: N=726.60 T_z=-671.21 M_y=775.64 T_y=106.06 M_z=163.86
Tensioni: σ_N=9.31 $\sigma_{m,d}$=217.96 τ=0.00 σ_{max}=227.26 (sic.=11.524)
Tensioni: σ_N=9.31 $\sigma_{m,d}$=-3.68 τ=43.94 τ_{max}=43.94 (sic.=34.412)
Tensioni: σ_N=9.31 $\sigma_{m,d}$=217.96 τ=0.00 $\sigma_{ID,max}$=227.26 (sic.=11.524)

- Verifica a taglio Dir. Y [4.2.16] - CC 91 SLU Xl=2.10 - Classe 1
Sollecitazioni: T_y=45.23
V,Ed=45.23 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 91 SLU Xl=2.10 - Classe 1
Sollecitazioni: T_z=-1072.66
V,Ed=-1072.66 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.03 (sic.=35.008)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 43 SLU Xl=0.06 - Classe 1
Sollecitazioni: N=775.76 T_z=-863.70 M_y=-1000.27 T_y=38.43 M_z=9.41
N,Ed=775.76 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-1000.27 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=16.878)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=9.41 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.878)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
$f_{z,L}$=0.01 (L/24171) (sic.=80.570)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 165
$f_{z,L}$=0.01 (L/17045) (sic.=68.180)

Asta n. 2017 (205 229) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=4.30 - Classe 3
  Sollecitazioni: N=505.55 T_z=-410.79 M_y=675.99 T_y=-89.38 M_z=-195.33
  Tensioni: σ_N=6.47 $\sigma_{m,d}$=216.17 τ=0.00 σ_{max}=222.65 (sic.=11.763)
  Tensioni: σ_N=6.47 $\sigma_{m,d}$=4.39 τ=26.89 τ_{max}=26.89 (sic.=56.226)
  Tensioni: σ_N=6.47 $\sigma_{m,d}$=216.17 τ=0.00 $\sigma_{ID,max}$=222.65 (sic.=11.763)

- Verifica a taglio Dir. Y [4.2.16] - CC 94 SLU Xl=4.30 - Classe 1
  Sollecitazioni: T_y=65.24
  V,Ed=65.24 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=4.30 - Classe 1
  Sollecitazioni: T_z=-418.07
  V,Ed=-418.07 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=89.820)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=4.30 - Classe 1
  Sollecitazioni: N=673.76 T_z=-418.07 M_y=652.32 T_y=65.24 M_z=130.75
  N,Ed=673.76 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=652.32 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.04 (sic.=25.880)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=130.75 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=61.314)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=25.880)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 66 SLU - Classe 1
  Sollecitazioni: N,Ed=-17.67 My,Ed=615.79 Mz,Ed=-179.87 L=4.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.31 M,cr=230992.00 λ_{LT}=0.28
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=25.76 Ncr,y=2439300.00 λ^*_y=0.30 Curva b: Φ_y=0.56 χ_y=0.97
  λ_z=43.43 Ncr,z=857898.00 λ^*_z=0.50 Curva c: Φ_z=0.70 χ_z=0.84
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.03+0.01=0.05 (sic.=21.038)
  Verifica ZZ: 0.00+0.02+0.02=0.04 (sic.=23.691)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
  $f_{Z,L}$=0.02 (L/23806) (sic.=79.353)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 188
  $f_{Z,L}$=0.02 (L/22243) (sic.=88.972)

Asta n. 2022 (210 236) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=2.21 - Classe 3
  Sollecitazioni: N=918.62 M_y=-137.09
  Tensioni: σ_N=11.76 $\sigma_{m,d}$=24.07 τ=0.00 σ_{max}=35.83 (sic.=73.093)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=11.76 $\sigma_{m,d}$=24.07 τ=0.00 $\sigma_{ID,max}$=35.83 (sic.=73.093)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=4.33 - Classe 1
  Sollecitazioni: T_z=-168.53
  V,Ed=-168.53 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 87 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=2312.33 T_z=168.53
  Verifica a trazione [4.2.5]
  N,Ed=2312.33 Npl,Rd=204503.00 Nu,Rd=241745.00 N,Ed/Nt,Rd=0.01 (sic.=88.440)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.06 (L/6610) (sic.=22.033)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.10 (L/4230) (sic.=16.920)

Asta n. 2026 (215 216) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=904.36 T_z=1074.83 M_y=1099.20 T_y=176.17 M_z=-274.47 M_x=-1.37
  Tensioni: σ_N=11.58 $\sigma_{m,d}$=329.97 τ=3.87 σ_{max}=341.56 (sic.=7.668)
  Tensioni: σ_N=11.58 $\sigma_{m,d}$=6.17 τ=70.51 τ_{max}=70.51 (sic.=21.446)
  Tensioni: σ_N=11.58 $\sigma_{m,d}$=329.97 τ=3.87 $\sigma_{ID,max}$=341.62 (sic.=7.667)

- Verifica a taglio Dir. Y [4.2.16] - CC 43 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=-35.26
  V,Ed=-35.26 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 43 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=1747.15

V,Ed=1747.15 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.05 (sic.=21.493)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 63 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=824.13 T_z=1217.63 M_y=1141.30 T_y=57.36 M_z=-125.86
  N,Ed=824.13 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=1141.30 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.07 (sic.=14.792)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-125.86 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=63.699)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.07 (sic.=14.792)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
  $f_{Z,L}$=0.00 (L/19137) (sic.=63.790)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 165
  $f_{Z,L}$=0.00 (L/14580) (sic.=58.320)

Asta n. 2026 (216 218) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=872.38 T_z=1192.87 M_y=1050.54 T_y=171.36 M_z=-160.04 M_x=-1.37
  Tensioni: σ_N=11.17 $\sigma_{m,d}$=264.31 τ=3.87 σ_{max}=275.48 (sic.=9.507)
  Tensioni: σ_N=11.17 $\sigma_{m,d}$=3.59 τ=78.22 τ_{max}=78.22 (sic.=19.331)
  Tensioni: σ_N=11.17 $\sigma_{m,d}$=264.31 τ=3.87 $\sigma_{ID,max}$=275.56 (sic.=9.504)

- Verifica a taglio Dir. Y [4.2.16] - CC 63 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=57.36
  V,Ed=57.36 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 63 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=1328.74
  V,Ed=1328.74 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.04 (sic.=28.261)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.68 - Classe 1
  Sollecitazioni: N=990.71 T_z=480.49 M_y=-1009.45 T_y=-70.29 M_z=62.69 M_x=-1.22
  N,Ed=990.71 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-1009.45 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=16.724)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=62.69 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.724)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.00 (L/24518) (sic.=81.727)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.00 (L/22474) (sic.=89.896)

Asta n. 2026 (218 221) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=789.20 T_z=-833.48 M_y=-939.69 T_y=121.32 M_z=117.97
  Tensioni: σ_N=10.11 $\sigma_{m,d}$=223.85 τ=0.00 σ_{max}=233.96 (sic.=11.194)
  Tensioni: σ_N=10.11 $\sigma_{m,d}$=-2.65 τ=54.56 τ_{max}=54.56 (sic.=27.712)
  Tensioni: σ_N=10.11 $\sigma_{m,d}$=223.85 τ=0.00 $\sigma_{ID,max}$=233.96 (sic.=11.194)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 94 SLU Xl=0.71 - Classe 1
  Sollecitazioni: T_y=-83.26 M_x=1.37
  V,Ed=-83.26 Vc,Rd,Red=99734.50 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 94 SLU Xl=0.71 - Classe 1
  Sollecitazioni: T_z=-637.19 M_x=1.37
  V,Ed=-637.19 Vc,Rd,Red=37512.80 V,Ed/Vc,Rd,Red=0.02 (sic.=58.872)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=984.24 T_z=-581.05 M_y=-1004.04 T_y=-83.26 M_z=56.36 M_x=1.37
  N,Ed=984.24 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-1004.04 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=16.814)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=56.36 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.814)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 190
  $f_{Z,G}$=0.00 (L/25471) (sic.=84.903)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 142

$f_{z,L}$=0.00 (L/17733) (sic.=70.932)

Asta n. 2026 (221 223) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.71 - Classe 3
  Sollecitazioni: N=828.82 T_z=800.79 M_y=-919.97 T_y=134.59 M_z=136.75 M_x=-2.18
  Tensioni: σ_N=10.61 $\sigma_{m,d}$=229.76 τ=6.15 σ_{max}=240.38 (sic.=10.896)
  Tensioni: σ_N=10.61 $\sigma_{m,d}$=-3.07 τ=52.84 τ_{max}=52.84 (sic.=28.615)
  Tensioni: σ_N=10.61 $\sigma_{m,d}$=229.76 τ=6.15 $\sigma_{ID,max}$=240.61 (sic.=10.885)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 66 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=105.43 M_x=-2.85
  V,Ed=105.43 Vc,Rd,Red=99624.10 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 66 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=574.53 M_x=-2.85
  V,Ed=574.53 Vc,Rd,Red=37471.30 V,Ed/Vc,Rd,Red=0.02 (sic.=65.221)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 66 SLU Xl=0.71 - Classe 1
  Sollecitazioni: N=581.75 T_z=518.39 M_y=-954.68 T_y=105.43 M_z=63.10 M_x=-2.85
  N,Ed=581.75 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-954.68 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=17.683)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=63.10 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.06 (sic.=17.683)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 162
  $f_{z,L}$=0.00 (L/33355) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 210
  $f_{z,L}$=0.00 (L/21226) (sic.=84.904)

Asta n. 2026 (223 224) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.68 - Classe 3
  Sollecitazioni: N=962.84 T_z=-1218.56 M_y=1088.00 T_y=155.40 M_z=164.43
  Tensioni: σ_N=12.33 $\sigma_{m,d}$=273.08 τ=0.00 σ_{max}=285.41 (sic.=9.176)
  Tensioni: σ_N=12.33 $\sigma_{m,d}$=-3.69 τ=79.77 τ_{max}=79.77 (sic.=18.955)
  Tensioni: σ_N=12.33 $\sigma_{m,d}$=273.08 τ=0.00 $\sigma_{ID,max}$=285.41 (sic.=9.176)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 91 SLU Xl=0.68 - Classe 1
  Sollecitazioni: T_y=-37.76 M_x=-1.36
  V,Ed=-37.76 Vc,Rd,Red=99735.30 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 91 SLU Xl=0.68 - Classe 1
  Sollecitazioni: T_z=-1368.98 M_x=-1.36
  V,Ed=-1368.98 Vc,Rd,Red=37513.10 V,Ed/Vc,Rd,Red=0.04 (sic.=27.402)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 66 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=588.01 T_z=-523.66 M_y=-955.71 T_y=93.29 M_z=71.31
  N,Ed=588.01 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-955.71 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=17.664)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=71.31 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.06 (sic.=17.664)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
  $f_{z,L}$=0.00 (L/24972) (sic.=83.240)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 165
  $f_{z,L}$=0.00 (L/19830) (sic.=79.320)

Asta n. 2026 (224 242) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.62 - Classe 3
  Sollecitazioni: N=995.39 T_z=-1041.05 M_y=1125.89 T_y=168.65 M_z=273.58
  Tensioni: σ_N=12.75 $\sigma_{m,d}$=334.21 τ=0.00 σ_{max}=346.96 (sic.=7.549)
  Tensioni: σ_N=12.75 $\sigma_{m,d}$=-6.15 τ=68.15 τ_{max}=68.15 (sic.=22.187)
  Tensioni: σ_N=12.75 $\sigma_{m,d}$=334.21 τ=0.00 $\sigma_{ID,max}$=346.96 (sic.=7.549)

- Verifica a taglio Dir. Y [4.2.16] - CC 67 SLU Xl=0.62 - Classe 1
  Sollecitazioni: T_y=57.13
  V,Ed=57.13 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 67 SLU Xl=0.62 - Classe 1
  Sollecitazioni: T_z=-1771.56
  V,Ed=-1771.56 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.05 (sic.=21.197)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 43 SLU Xl=0.62 - Classe 1
  Sollecitazioni: N=856.80 T_z=-1194.88 M_y=1192.06 T_y=-30.11 M_z=-63.73 M_x=-1.24
  N,Ed=856.80 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=1192.06 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.07 (sic.=14.162)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-63.73 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.07 (sic.=14.162)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 145
  $f_{z,L}$=0.00 (L/21487) (sic.=71.623)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 145
  $f_{z,L}$=0.00 (L/17250) (sic.=69.000)

Asta n. 3002 (-27 -28) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica a trazione (4.2.4.1.2.1) - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=8.77 T_z=1.62
  Verifica a trazione [4.2.5]
  N,Ed=8.77 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.75 - Classe 1
  Sollecitazioni: T_z=-2.10
  V,Ed=-2.10 Vc,Rd=4355.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 67 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=12.71 T_z=2.10
  Verifica a trazione [4.2.5]
  N,Ed=12.71 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 90 SLU - Classe 3
  Sollecitazioni: N,Ed=-11.51 My,Ed=-0.39 Mz,Ed=0.13 L=0.75
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=50.72 Ncr,y=46408.90 λ^*_y=0.58 Curva a: Φ_y=0.71 χ_y=0.90
  λ_z=50.72 Ncr,z=46408.90 λ^*_z=0.58 Curva a: Φ_z=0.71 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00+0.00+0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 121
  $f_{z,L}$=0.00 (L/524288) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 137
  $f_{z,L}$=0.00 (L/104858) (sic. >100)

Asta n. 3002 (-28 -29) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica a trazione (4.2.4.1.2.1) - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=15.17 T_z=1.62
  Verifica a trazione [4.2.5]
  N,Ed=15.17 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 94 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=2.10 M_x=1.30
  V,Ed=2.10 Vc,Rd,Red=4318.94 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 94 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=2.10 M_x=1.30
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=13.33 τ_{max}=13.33 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=13.33 $\sigma_{ID,max}$=23.10 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 90 SLU - Classe 3
  Sollecitazioni: N,Ed=-20.06 My,Ed=-0.39 Mz,Ed=0.13 L=0.75
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=50.72 Ncr,y=46408.90 λ^*_y=0.58 Curva a: Φ_y=0.71 χ_y=0.90
  λ_z=50.72 Ncr,z=46408.90 λ^*_z=0.58 Curva a: Φ_z=0.71 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00+0.00+0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 129
  $f_{z,L}$=0.00 (L/524288) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 117
  $f_{z,L}$=0.00 (L/104858) (sic. >100)

Asta n. 3002 (-29 -30) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica a trazione (4.2.4.1.2.1) - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=230.90 T_z=1.51 M_x=-1.06
  Verifica a trazione [4.2.5]
  N,Ed=230.90 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.02 (sic.=65.335)

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 18 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=1.96 M_x=-1.86
  V,Ed=1.96 Vc,Rd,Red=4303.44 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 95 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=366.10 T_z=1.96 M_x=-1.73
  Verifica a trazione [4.2.5]
  N,Ed=366.10 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.02 (sic.=41.207)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 62 SLU - Classe 3
  Sollecitazioni: N,Ed=-363.44 My,Ed=-0.34 Mz,Ed=0.11 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=47.34 Ncr,y=53275.60 λ^*_y=0.55 Curva a: Φ_y=0.68 χ_y=0.91
  λ_z=47.34 Ncr,z=53275.60 λ^*_z=0.55 Curva a: Φ_z=0.68 χ_z=0.91
  Kyy, Kyz, Kzy, Kzz=0.96, 0.96, 0.77, 0.96
  Verifica YY: 0.03+0.00+0.00=0.03 (sic.=34.349)
  Verifica ZZ: 0.03+0.00+0.00=0.03 (sic.=34.825)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 128
  $f_{z,L}$=0.00 (L/367002) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 120
  $f_{z,L}$=0.00 (L/133455) (sic. >100)

Asta n. 3002 (-30 -31) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica a trazione (4.2.4.1.2.1) - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=227.74 T_z=1.51
  Verifica a trazione [4.2.5]
  N,Ed=227.74 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.02 (sic.=66.241)

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 87 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-1.96 M_x=-1.48
  V,Ed=-1.96 Vc,Rd,Red=4313.90 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 95 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=364.25 T_z=1.96 M_x=-1.05
  Verifica a trazione [4.2.5]
  N,Ed=364.25 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.02 (sic.=41.416)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 62 SLU - Classe 3
  Sollecitazioni: N,Ed=-360.78 My,Ed=-0.34 Mz,Ed=0.11 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=47.34 Ncr,y=53275.60 λ^*_y=0.55 Curva a: Φ_y=0.68 χ_y=0.91
  λ_z=47.34 Ncr,z=53275.60 λ^*_z=0.55 Curva a: Φ_z=0.68 χ_z=0.91
  Kyy, Kyz, Kzy, Kzz=0.96, 0.96, 0.77, 0.96
  Verifica YY: 0.03+0.00+0.00=0.03 (sic.=34.579)
  Verifica ZZ: 0.03+0.00+0.00=0.03 (sic.=35.062)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 128
  $f_{z,L}$=0.00 (L/367002) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 116
  $f_{z,L}$=0.00 (L/146801) (sic. >100)

Asta n. 3002 (-31 -32) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica a trazione (4.2.4.1.2.1) - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=227.07 T_z=1.51
  Verifica a trazione [4.2.5]
  N,Ed=227.07 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.02 (sic.=66.437)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-1.96
  V,Ed=-1.96 Vc,Rd=4355.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 95 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=363.74 T_z=1.96
  Verifica a trazione [4.2.5]
  N,Ed=363.74 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.02 (sic.=41.474)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 62 SLU - Classe 3
  Sollecitazioni: N,Ed=-359.36 My,Ed=-0.34 Mz,Ed=0.11 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95

λ_y=47.34 Ncr,y=53275.60 λ^*_y=0.55 Curva a: Φ_y=0.68 χ_y=0.91
λ_z=47.34 Ncr,z=53275.60 λ^*_z=0.55 Curva a: Φ_z=0.68 χ_z=0.91
Kyy, Kyz, Kzy, Kzz=0.96, 0.96, 0.77, 0.96
Verifica YY: 0.03+0.00+0.00=0.03 (sic.=34.703)
Verifica ZZ: 0.03+0.00+0.00=0.03 (sic.=35.190)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 142
$f_{z,G}$=0.00 (L/489335) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 189
$f_{z,L}$=0.00 (L/146801) (sic. >100)

Asta n. 3002 (-32 -33) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica a trazione (4.2.4.1.2.1) - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=227.00 T_z=1.51
Verifica a trazione [4.2.5]
N,Ed=227.00 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.02 (sic.=66.456)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.70 - Classe 1
Sollecitazioni: T_z=-1.96
V,Ed=-1.96 Vc,Rd=4355.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 95 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=363.60 T_z=1.96
Verifica a trazione [4.2.5]
N,Ed=363.60 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.02 (sic.=41.490)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 62 SLU - Classe 3
Sollecitazioni: N,Ed=-357.93 My,Ed=-0.34 Mz,Ed=0.11 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
λ_y=47.34 Ncr,y=53275.50 λ^*_y=0.55 Curva a: Φ_y=0.68 χ_y=0.91
λ_z=47.34 Ncr,z=53275.50 λ^*_z=0.55 Curva a: Φ_z=0.68 χ_z=0.91
Kyy, Kyz, Kzy, Kzz=0.96, 0.96, 0.77, 0.96
Verifica YY: 0.03+0.00+0.00=0.03 (sic.=34.829)
Verifica ZZ: 0.03+0.00+0.00=0.03 (sic.=35.319)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 134
$f_{z,L}$=0.00 (L/367002) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 126
$f_{z,L}$=0.00 (L/133455) (sic. >100)

Asta n. 3002 (-33 -34) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica a trazione (4.2.4.1.2.1) - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=226.26 T_z=1.51
Verifica a trazione [4.2.5]
N,Ed=226.26 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.01 (sic.=66.673)

- Verifica a taglio e torsione Dir. Z [4.2.25] - CC 87 SLU Xl=0.70 - Classe 1
Sollecitazioni: T_z=-1.96 M_x=1.81
V,Ed=-1.96 Vc,Rd,Red=4304.65 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 95 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=363.07 T_z=1.96 M_x=1.12
Verifica a trazione [4.2.5]
N,Ed=363.07 Npl,Rd=15085.70 Nu,Rd=17833.00 N,Ed/Nt,Rd=0.02 (sic.=41.550)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 62 SLU - Classe 3
Sollecitazioni: N,Ed=-356.01 My,Ed=-0.34 Mz,Ed=0.11 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
λ_y=47.34 Ncr,y=53275.60 λ^*_y=0.55 Curva a: Φ_y=0.68 χ_y=0.91
λ_z=47.34 Ncr,z=53275.60 λ^*_z=0.55 Curva a: Φ_z=0.68 χ_z=0.91
Kyy, Kyz, Kzy, Kzz=0.96, 0.96, 0.77, 0.96
Verifica YY: 0.03+0.00+0.00=0.03 (sic.=35.000)
Verifica ZZ: 0.03+0.00+0.00=0.03 (sic.=35.495)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 133
$f_{z,L}$=0.00 (L/367002) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 116
$f_{z,L}$=0.00 (L/133455) (sic. >100)

Asta n. 3002 (-34 -35) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica a compressione (4.2.4.1.2.2) - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-24.73 T_z=1.51
Verifica a compressione [4.2.9]
N,Ed=-24.73 Nc,Rd=-15085.70 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 23 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-1.96
  V,Ed=-1.96 Vc,Rd=4355.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a compressione (4.2.4.1.2.2) - CC 100 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-102.29 T_z=1.96
  Verifica a compressione [4.2.9]
  N,Ed=-102.29 Nc,Rd=-15085.70 N,Ed/Nc,Rd=0.01 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 100 SLU - Classe 3
  Sollecitazioni: N,Ed=-102.29 My,Ed=-0.34 Mz,Ed=0.11 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=47.34 Ncr,y=53275.60 λ^*_y=0.55 Curva a: Φ_y=0.68 χ_y=0.91
  λ_z=47.34 Ncr,z=53275.60 λ^*_z=0.55 Curva a: Φ_z=0.68 χ_z=0.91
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.00+0.00=0.01 (sic.=99.349)
  Verifica ZZ: 0.01+0.00+0.00=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 128
  $f_{z,L}$=0.00 (L/489335) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 116
  $f_{z,G}$=0.00 (L/133455) (sic. >100)

Asta n. 3002 (-35 -36) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=-23.61 T_z=1.67 M_y=-2.23 T_y=-1.56 M_z=1.09
  Tensioni: σ_N=-4.10 $\sigma_{m,d}$=-52.69 τ=0.00 σ_{max}=-56.79 (sic.=46.118)
  Tensioni: σ_N=-4.10 $\sigma_{m,d}$=-13.87 τ=0.65 τ_{max}=0.65 (sic. >100)
  Tensioni: σ_N=-4.10 $\sigma_{m,d}$=-52.69 τ=0.00 $\sigma_{ID,max}$=56.79 (sic.=46.118)

- Verifica a taglio Dir. Z [4.2.16] - CC 87 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=21.08
  V,Ed=21.08 Vc,Rd=4355.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 114 SLU Xl=0.70 - Classe 3
  Sollecitazioni: N=40.21 T_z=12.89 M_y=-10.39 M_z=1.01
  Tensioni: σ_N=6.98 $\sigma_{m,d}$=181.11 τ=0.00 σ_{max}=188.09 (sic.=13.924)
  Tensioni: σ_N=6.98 $\sigma_{m,d}$=-16.07 τ=4.99 τ_{max}=4.99 (sic. >100)
  Tensioni: σ_N=6.98 $\sigma_{m,d}$=181.11 τ=0.00 $\sigma_{ID,max}$=188.09 (sic.=13.924)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 3
  Sollecitazioni: N,Ed=-55.99 My,Ed=-13.38 Mz,Ed=-0.42 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=47.34 Ncr,y=53275.50 λ^*_y=0.55 Curva a: Φ_y=0.68 χ_y=0.91
  λ_z=47.34 Ncr,z=53275.50 λ^*_z=0.55 Curva a: Φ_z=0.68 χ_z=0.91
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.08+0.00=0.08 (sic.=11.949)
  Verifica ZZ: 0.00+0.06+0.00=0.07 (sic.=14.652)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 186
  $f_{z,L}$=0.01 (L/8486) (sic.=28.287)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 186
  $f_{z,L}$=0.01 (L/6142) (sic.=24.568)

Asta n. 3002 (-36 -37) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-23.61 T_z=-1.66 M_y=-2.22 T_y=1.56 M_z=1.09
  Tensioni: σ_N=-4.10 $\sigma_{m,d}$=-52.52 τ=0.00 σ_{max}=-56.62 (sic.=46.254)
  Tensioni: σ_N=-4.10 $\sigma_{m,d}$=42.02 τ=0.65 τ_{max}=0.65 (sic. >100)
  Tensioni: σ_N=-4.10 $\sigma_{m,d}$=-52.52 τ=0.00 $\sigma_{ID,max}$=56.62 (sic.=46.254)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_y=-1.69
  V,Ed=-1.69 Vc,Rd=4355.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-21.05
  V,Ed=-21.05 Vc,Rd=4355.00 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 114 SLU Xl=0.00 - Classe 3
  Sollecitazioni: N=40.21 T_z=-13.37 M_y=-10.73 M_z=1.01
  Tensioni: σ_N=6.98 $\sigma_{m,d}$=186.49 τ=0.00 σ_{max}=193.47 (sic.=13.537)
  Tensioni: σ_N=6.98 $\sigma_{m,d}$=-16.07 τ=5.18 τ_{max}=5.18 (sic. >100)
  Tensioni: σ_N=6.98 $\sigma_{m,d}$=186.49 τ=0.00 $\sigma_{ID,max}$=193.47 (sic.=13.537)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 3
  Sollecitazioni: N,Ed=-47.96 My,Ed=-13.32 Mz,Ed=0.47 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=47.34 Ncr,y=53275.50 λ^*_y=0.55 Curva a: Φ_y=0.68 χ_y=0.91
  λ_z=47.34 Ncr,z=53275.50 λ^*_z=0.55 Curva a: Φ_z=0.68 χ_z=0.91
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.08+0.00=0.08 (sic.=12.040)
  Verifica ZZ: 0.00+0.06+0.00=0.07 (sic.=14.774)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{Z,L}$=0.01 (L/8437) (sic.=28.123)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 211
  $f_{Z,L}$=0.01 (L/6142) (sic.=24.568)

Asta n. 3004 (-38 -39) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.75 - Classe 3
  Sollecitazioni: N=-186.48 T_z=26.74 M_y=-25.38 T_y=3.28 M_z=4.15
  Tensioni: σ_N=-7.36 $\sigma_{m,d}$=-34.66 τ=0.00 σ_{max}=-42.02 (sic.=62.328)
  Tensioni: σ_N=-7.36 $\sigma_{m,d}$=-0.45 τ=5.59 τ_{max}=5.59 (sic. >100)
  Tensioni: σ_N=-7.36 $\sigma_{m,d}$=-34.66 τ=0.00 $\sigma_{ID,max}$=42.02 (sic.=62.328)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=10.82
  V,Ed=10.82 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=115.88
  V,Ed=115.88 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.75 - Classe 1
  Sollecitazioni: N=233.60 T_z=97.40 M_y=-79.98 T_y=4.94 M_z=5.91
  N,Ed=233.60 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-79.98 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=39.297)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=5.91 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=39.297)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-291.71 My,Ed=-79.96 Mz,Ed=6.29 L=0.75
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=85658.40 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.02+0.00=0.03 (sic.=32.376)
  Verifica ZZ: 0.00+0.01+0.00=0.02 (sic.=43.533)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 186
  $f_{Z,L}$=0.00 (L/65536) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
  $f_{Z,L}$=0.00 (L/37449) (sic. >100)

Asta n. 3004 (-39 -40) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.75 - Classe 3
  Sollecitazioni: N=-186.48 T_z=7.61 M_y=-36.42 T_y=-25.14 M_z=14.77
  Tensioni: σ_N=-7.36 $\sigma_{m,d}$=-72.63 τ=0.00 σ_{max}=-79.99 (sic.=32.741)
  Tensioni: σ_N=-7.36 $\sigma_{m,d}$=-38.71 τ=1.86 τ_{max}=1.86 (sic. >100)
  Tensioni: σ_N=-7.36 $\sigma_{m,d}$=-72.63 τ=0.00 $\sigma_{ID,max}$=79.99 (sic.=32.741)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=12.07
  V,Ed=12.07 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=59.04
  V,Ed=59.04 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.75 - Classe 1
  Sollecitazioni: N=233.60 T_z=40.56 M_y=-117.33 T_y=6.19 M_z=12.76
  N,Ed=233.60 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-117.33 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=26.787)

Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=12.76 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.04 (sic.=26.787)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
Sollecitazioni: N,Ed=-291.71 My,Ed=-117.30 Mz,Ed=-9.99 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=57446.30 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
λ_Z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.04+0.00=0.04 (sic.=22.968)
Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=31.232)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 181
$f_{Z,G}$=0.00 (L/33465) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
$f_{Z,G}$=0.00 (L/19181) (sic.=76.724)

Asta n. 3004 (-40 -41) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.75 - Classe 3
Sollecitazioni: N=-189.57 T_z=-19.11 M_y=-27.50 T_y=-51.31 M_z=26.26
Tensioni: σ_N=-7.48 $\sigma_{m,d}$=-94.09 τ=0.00 σ_{max}=-101.57 (sic.=25.786)
Tensioni: σ_N=-7.48 $\sigma_{m,d}$=-19.63 τ=4.12 τ_{max}=4.12 (sic. >100)
Tensioni: σ_N=-7.48 $\sigma_{m,d}$=-94.09 τ=0.00 $\sigma_{ID,max}$=101.57 (sic.=25.786)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_y=-45.93
V,Ed=-45.93 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_z=-42.05
V,Ed=-42.05 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=232.74 T_z=-23.57 M_y=-117.32 T_y=-40.05 M_z=12.76
N,Ed=232.74 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-117.32 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=26.790)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=12.76 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.04 (sic.=26.790)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
Sollecitazioni: N,Ed=-291.26 My,Ed=-117.29 Mz,Ed=16.01 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.11 M,cr=54109.50 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
λ_Z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.04+0.01=0.05 (sic.=21.857)
Verifica ZZ: 0.00+0.02+0.01=0.04 (sic.=28.000)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 196
$f_{Z,L}$=0.00 (L/31457) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
$f_{Z,L}$=0.00 (L/17873) (sic.=71.492)

Asta n. 3004 (-41 -42) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-191.71 T_z=-29.58 M_y=-27.52 T_y=-32.75 M_z=26.26
Tensioni: σ_N=-7.57 $\sigma_{m,d}$=-94.10 τ=0.00 σ_{max}=-101.67 (sic.=25.761)
Tensioni: σ_N=-7.57 $\sigma_{m,d}$=-2.84 τ=6.20 τ_{max}=6.20 (sic. >100)
Tensioni: σ_N=-7.57 $\sigma_{m,d}$=-94.10 τ=0.00 $\sigma_{ID,max}$=101.67 (sic.=25.761)

- Verifica a taglio Dir. Y [4.2.16] - CC 107 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_y=-24.29
V,Ed=-24.29 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_z=-133.50
V,Ed=-133.50 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic.=95.793)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-290.90 T_z=-115.02 M_y=-93.19 T_y=-18.41 M_z=16.01
  N,Ed=-290.90 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-93.19 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=33.726)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=16.01 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic.=96.392)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=33.726)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-290.90 My,Ed=-93.19 Mz,Ed=16.01 L=0.75
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=85658.40 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.03+0.01=0.04 (sic.=26.000)
  Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=31.910)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{Z,G}$=0.00 (L/50738) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
  $f_{Z,G}$=0.00 (L/30840) (sic. >100)

Asta n. 3004 (-42 -43) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=-377.54 T_z=40.27 M_y=-32.83 T_y=-32.29 M_z=-21.13
  Tensioni: σ_N=-14.90 $\sigma_{m,d}$=-85.77 τ=0.00 σ_{max}=-100.67 (sic.=26.015)
  Tensioni: σ_N=-14.90 $\sigma_{m,d}$=2.29 τ=8.43 τ_{max}=8.43 (sic. >100)
  Tensioni: σ_N=-14.90 $\sigma_{m,d}$=-85.77 τ=0.00 $\sigma_{ID,max}$=100.67 (sic.=26.015)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-7.10
  V,Ed=-7.10 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=179.93
  V,Ed=179.93 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic.=71.073)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=-48.97 T_z=162.68 M_y=-119.91 T_y=-12.59 M_z=-6.89
  N,Ed=-48.97 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-119.91 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=26.210)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-6.89 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.04 (sic.=26.210)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-348.64 My,Ed=-119.87 Mz,Ed=-11.41 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.60 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976653.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.04+0.00=0.05 (sic.=21.886)
  Verifica ZZ: 0.01+0.02+0.01=0.03 (sic.=29.244)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/44485) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/27185) (sic. >100)

Asta n. 3004 (-43 -44) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=-392.13 T_z=16.83 M_y=-49.18 T_y=40.67 M_z=15.05
  Tensioni: σ_N=-15.48 $\sigma_{m,d}$=-85.36 τ=0.00 σ_{max}=-100.83 (sic.=25.974)
  Tensioni: σ_N=-15.48 $\sigma_{m,d}$=-31.65 τ=3.58 τ_{max}=3.58 (sic. >100)
  Tensioni: σ_N=-15.48 $\sigma_{m,d}$=-85.36 τ=0.00 $\sigma_{ID,max}$=100.83 (sic.=25.974)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=25.83
  V,Ed=25.83 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=94.20
  V,Ed=94.20 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=-49.80 T_z=76.95 M_y=-179.64 T_y=20.34 M_z=9.26
  N,Ed=-49.80 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-179.64 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.06 (sic.=17.496)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=9.26 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.06 (sic.=17.496)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-349.70 My,Ed=-179.55 Mz,Ed=-11.41 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.18 M,cr=65832.40 λ_{LT}=0.22
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976653.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.05+0.00=0.06 (sic.=15.688)
  Verifica ZZ: 0.01+0.03+0.01=0.05 (sic.=22.207)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 196
  $f_{Z,L}$=0.00 (L/23678) (sic.=78.927)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/14535) (sic.=58.140)

Asta n. 3004 (-44 -45) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=-392.76 T_z=-6.70 M_y=-49.18 T_y=-18.59 M_z=23.41
  Tensioni: σ_N=-15.50 $\sigma_{m,d}$=-107.09 τ=0.00 σ_{max}=-122.59 (sic.=21.364)
  Tensioni: σ_N=-15.50 $\sigma_{m,d}$=-32.56 τ=1.45 τ_{max}=1.45 (sic. >100)
  Tensioni: σ_N=-15.50 $\sigma_{m,d}$=-107.09 τ=0.00 $\sigma_{ID,max}$=122.59 (sic.=21.364)

- Verifica a taglio Dir. Y [4.2.16] - CC 104 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=3.49
  V,Ed=3.49 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 104 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=8.76
  V,Ed=8.76 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.35 - Classe 1
  Sollecitazioni: N=-50.36 M_y=-181.08 T_y=3.36 M_z=10.92
  N,Ed=-50.36 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-181.08 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.06 (sic.=17.357)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=10.92 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.06 (sic.=17.357)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-350.29 My,Ed=-179.48 Mz,Ed=12.35 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.00 M,cr=55635.50 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976654.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.05+0.00=0.06 (sic.=15.606)
  Verifica ZZ: 0.01+0.03+0.01=0.05 (sic.=21.926)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 211
  $f_{Z,G}$=0.00 (L/18821) (sic.=62.737)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.01 (L/11559) (sic.=46.236)

Asta n. 3004 (-45 -46) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=-393.21 T_z=-30.07 M_y=-32.81 T_y=-30.57 M_z=-39.73
  Tensioni: σ_N=-15.52 $\sigma_{m,d}$=-134.10 τ=0.00 σ_{max}=-149.62 (sic.=17.504)
  Tensioni: σ_N=-15.52 $\sigma_{m,d}$=4.30 τ=6.30 τ_{max}=6.30 (sic. >100)
  Tensioni: σ_N=-15.52 $\sigma_{m,d}$=-134.10 τ=0.00 $\sigma_{ID,max}$=149.62 (sic.=17.504)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_y=-11.03
  V,Ed=-11.03 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-94.09
  V,Ed=-94.09 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-51.04 T_z=-76.84 M_y=-179.61 T_y=-5.55 M_z=11.62
  N,Ed=-51.04 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-179.61 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.06 (sic.=17.499)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=11.62 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=17.499)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-350.94 My,Ed=-179.51 Mz,Ed=12.35 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.18 M,cr=65823.30 λ_{LT}=0.22
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976652.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.05+0.00=0.06 (sic.=15.602)
  Verifica ZZ: 0.01+0.03+0.01=0.05 (sic.=21.919)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{Z,G}$=0.00 (L/21275) (sic.=70.917)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.01 (L/13225) (sic.=52.900)

Asta n. 3004 (-46 -47) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-394.00 T_z=-40.25 M_y=-32.82 T_y=58.87 M_z=-39.73
  Tensioni: σ_N=-15.55 $\sigma_{m,d}$=-134.11 τ=0.00 σ_{max}=-149.66 (sic.=17.500)
  Tensioni: σ_N=-15.55 $\sigma_{m,d}$=4.30 τ=8.44 τ_{max}=8.44 (sic. >100)
  Tensioni: σ_N=-15.55 $\sigma_{m,d}$=-134.11 τ=0.00 $\sigma_{ID,max}$=149.66 (sic.=17.500)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_y=-11.05
  V,Ed=-11.05 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-179.90
  V,Ed=-179.90 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic.=71.084)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-51.84 T_z=-162.66 M_y=-119.89 T_y=-5.56 M_z=5.82
  N,Ed=-51.84 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-119.89 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=26.215)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=5.82 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=26.215)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-394.00 My,Ed=-32.82 Mz,Ed=-39.73 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.70 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976654.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.01+0.04=0.05 (sic.=18.306)
  Verifica ZZ: 0.01+0.01+0.04=0.05 (sic.=19.013)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206

$f_{Z,G}$=0.00 (L/41943) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/26214) (sic. >100)

Asta n. 3004 (-47 -48) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=503.06 T_z=43.02 M_y=-34.76 T_y=-55.96 M_z=-37.69
  Tensioni: σ_N=19.85 $\sigma_{m,d}$=130.63 τ=0.00 σ_{max}=150.48 (sic.=17.404)
  Tensioni: σ_N=19.85 $\sigma_{m,d}$=4.08 τ=9.02 τ_{max}=9.02 (sic. >100)
  Tensioni: σ_N=19.85 $\sigma_{m,d}$=130.63 τ=0.00 $\sigma_{ID,max}$=150.48 (sic.=17.404)

- Verifica a taglio Dir. Y [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=22.80
  V,Ed=22.80 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=120.71
  V,Ed=120.71 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 107 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=-374.15 T_z=103.46 M_y=-78.46 T_y=17.32 M_z=14.04
  N,Ed=-374.15 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-78.46 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.02 (sic.=40.059)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=14.04 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=40.059)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-481.19 My,Ed=-34.76 Mz,Ed=-37.69 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.70 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_Z=23.19 Ncr,z=976654.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.01+0.04=0.05 (sic.=18.287)
  Verifica ZZ: 0.01+0.01+0.04=0.05 (sic.=19.023)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{Z,G}$=0.00 (L/86353) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
  $f_{Z,G}$=0.00 (L/37641) (sic. >100)

Asta n. 3004 (-48 -49) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=505.40 T_z=33.08 M_y=-34.73 T_y=49.35 M_z=-37.69
  Tensioni: σ_N=19.95 $\sigma_{m,d}$=130.60 τ=0.00 σ_{max}=150.55 (sic.=17.397)
  Tensioni: σ_N=19.95 $\sigma_{m,d}$=4.08 τ=6.94 τ_{max}=6.94 (sic. >100)
  Tensioni: σ_N=19.95 $\sigma_{m,d}$=130.60 τ=0.00 $\sigma_{ID,max}$=150.55 (sic.=17.397)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=36.54
  V,Ed=36.54 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=49.74
  V,Ed=49.74 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=1.40 - Classe 1
  Sollecitazioni: N=-60.30 T_z=15.07 M_y=-123.61 T_y=-4.10 M_z=5.43
  N,Ed=-60.30 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-123.61 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=25.427)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=5.43 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=25.427)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-483.75 My,Ed=-62.25 Mz,Ed=-37.69 L=1.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.26 M,cr=20757.50 λ_{LT}=0.38
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=28.62 Ncr,y=640995.00 λ^*_y=0.33 Curva b: Φ_y=0.58 χ_y=0.95

λ_z=46.38 Ncr,z=244163.00 λ^*_z=0.53 Curva c: Φ_z=0.72 χ_z=0.82
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.02+0.04=0.06 (sic.=15.494)
Verifica ZZ: 0.01+0.02+0.04=0.06 (sic.=16.263)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 211
$f_{Z,G}$=0.00 (L/28231) (sic.=94.103)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
$f_{Z,L}$=0.01 (L/9502) (sic.=38.008)

Asta n. 3004 (-49 -50) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-505.99 T_z=-31.30 M_y=-62.40 T_y=20.28 M_z=27.75
Tensioni: σ_N=-19.97 $\sigma_{m,d}$=-130.78 τ=0.00 σ_{max}=-150.75 (sic.=17.374)
Tensioni: σ_N=-19.97 $\sigma_{m,d}$=-3.00 τ=6.55 τ_{max}=6.55 (sic. >100)
Tensioni: σ_N=-19.97 $\sigma_{m,d}$=-130.78 τ=0.00 $\sigma_{ID,max}$=150.75 (sic.=17.374)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=1.40 - Classe 1
Sollecitazioni: T_y=-9.37
V,Ed=-9.37 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=1.40 - Classe 1
Sollecitazioni: T_z=-105.57
V,Ed=-105.57 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-45.93 T_z=-71.08 M_y=-123.66 T_y=1.61 M_z=5.43
N,Ed=-45.93 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-123.66 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=25.417)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=5.43 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=25.417)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-505.99 My,Ed=-62.40 Mz,Ed=27.75 L=1.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=28885.00 λ_{LT}=0.32
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=28.62 Ncr,y=640996.00 λ^*_y=0.33 Curva b: Φ_y=0.58 χ_y=0.95
λ_z=46.38 Ncr,z=244163.00 λ^*_z=0.53 Curva c: Φ_z=0.72 χ_z=0.82
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.02+0.03=0.06 (sic.=18.003)
Verifica ZZ: 0.01+0.02+0.03=0.05 (sic.=19.033)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 191
$f_{Z,G}$=0.00 (L/37165) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 191
$f_{Z,G}$=0.01 (L/12765) (sic.=51.060)

Asta n. 3006 (-55 -56) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.75 - Classe 3
Sollecitazioni: N=46.02 T_z=27.21 M_y=-25.74 T_y=5.86 M_z=6.09
Tensioni: σ_N=1.82 $\sigma_{m,d}$=40.04 τ=0.00 σ_{max}=41.86 (sic.=62.572)
Tensioni: σ_N=1.82 $\sigma_{m,d}$=-0.66 τ=5.69 τ_{max}=5.69 (sic. >100)
Tensioni: σ_N=1.82 $\sigma_{m,d}$=40.04 τ=0.00 $\sigma_{ID,max}$=41.86 (sic.=62.572)

- Verifica a taglio Dir. Y [4.2.16] - CC 87 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=8.56
V,Ed=8.56 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 87 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=133.78
V,Ed=133.78 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic.=95.594)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 87 SLU Xl=0.75 - Classe 1
Sollecitazioni: N=69.92 T_z=115.30 M_y=-93.40 T_y=2.68 M_z=4.22
N,Ed=69.92 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-93.40 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=33.650)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=4.22 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=33.650)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-19.09 My,Ed=-93.40 Mz,Ed=10.46 L=0.75
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=85658.40 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.03+0.00=0.03 (sic.=30.883)
  Verifica ZZ: 0.00+0.02+0.01=0.02 (sic.=42.239)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 181
  $f_{Z,G}$=0.00 (L/54237) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{Z,G}$=0.00 (L/32768) (sic. >100)

Asta n. 3006 (-56 -57) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.75 - Classe 3
  Sollecitazioni: N=-66.41 T_z=3.17 M_y=-33.45 T_y=-13.37 M_z=-5.05
  Tensioni: σ_N=-2.62 $\sigma_{m,d}$=-44.57 τ=0.00 σ_{max}=-47.19 (sic.=55.502)
  Tensioni: σ_N=-2.62 $\sigma_{m,d}$=-23.87 τ=0.99 τ_{max}=0.99 (sic. >100)
  Tensioni: σ_N=-2.62 $\sigma_{m,d}$=-44.57 τ=0.00 $\sigma_{ID,max}$=47.19 (sic.=55.502)

- Verifica a taglio Dir. Y [4.2.16] - CC 87 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-13.48
  V,Ed=-13.48 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 87 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=38.58
  V,Ed=38.58 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 87 SLU Xl=0.75 - Classe 1
  Sollecitazioni: N=69.92 T_z=20.10 M_y=-115.44 T_y=-19.36 M_z=-8.10
  N,Ed=69.92 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-115.44 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=27.226)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-8.10 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=27.226)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-19.09 My,Ed=-115.44 Mz,Ed=10.46 L=0.75
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.10 M,cr=53680.20 λ_{LT}=0.25
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.03+0.00=0.04 (sic.=25.614)
  Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=36.139)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/32099) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{Z,L}$=0.00 (L/18725) (sic.=74.900)

Asta n. 3006 (-57 -58) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-66.41 T_z=-5.63 M_y=-33.45 T_y=8.07 M_z=-5.05
  Tensioni: σ_N=-2.62 $\sigma_{m,d}$=-44.57 τ=0.00 σ_{max}=-47.19 (sic.=55.501)
  Tensioni: σ_N=-2.62 $\sigma_{m,d}$=0.55 τ=1.18 τ_{max}=1.18 (sic. >100)
  Tensioni: σ_N=-2.62 $\sigma_{m,d}$=-44.57 τ=0.00 $\sigma_{ID,max}$=47.19 (sic.=55.501)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.75 - Classe 1
  Sollecitazioni: T_y=2.73
  V,Ed=2.73 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.75 - Classe 1
  Sollecitazioni: T_z=-57.77
  V,Ed=-57.77 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 87 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=69.92 T_z=-39.29 M_y=-115.45 T_y=16.05 M_z=-8.10
  N,Ed=69.92 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00

Pressoflessione retta YY [4.2.33]:
My,Ed=-115.45 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=27.223)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-8.10 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.04 (sic.=27.223)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
Sollecitazioni: N,Ed=-62.02 My,Ed=-115.45 Mz,Ed=6.96 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=57351.10 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
λ_z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.03+0.00=0.04 (sic.=26.042)
Verifica ZZ: 0.00+0.02+0.00=0.03 (sic.=38.171)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
$f_{z,L}$=0.00 (L/33465) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
$f_{z,L}$=0.00 (L/18950) (sic.=75.800)

Asta n. 3006 (-58 -59) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=67.83 T_z=-24.76 M_y=-23.90 T_y=-2.51 M_z=3.58
Tensioni: σ_N=2.68 $\sigma_{m,d}$=31.78 τ=0.00 σ_{max}=34.45 (sic.=76.016)
Tensioni: σ_N=2.68 $\sigma_{m,d}$=-0.39 τ=5.18 τ_{max}=5.18 (sic. >100)
Tensioni: σ_N=2.68 $\sigma_{m,d}$=31.78 τ=0.00 $\sigma_{ID,max}$=34.45 (sic.=76.016)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_y=-12.22
V,Ed=-12.22 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_z=-114.60
V,Ed=-114.60 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-62.02 T_z=-96.12 M_y=-79.02 T_y=-6.34 M_z=6.96
N,Ed=-62.02 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-79.02 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=39.773)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=6.96 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=39.773)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
Sollecitazioni: N,Ed=-62.02 My,Ed=-79.02 Mz,Ed=6.96 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=85658.40 λ_{LT}=0.20
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
λ_z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.02+0.00=0.03 (sic.=36.510)
Verifica ZZ: 0.00+0.01+0.00=0.02 (sic.=51.041)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
$f_{z,L}$=0.00 (L/68385) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 186
$f_{z,L}$=0.00 (L/36578) (sic. >100)

Asta n. 3006 (-59 -60) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.70 - Classe 3
Sollecitazioni: N=-51.39 T_z=29.44 M_y=-25.25 T_y=5.89 M_z=5.60
Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-38.30 τ=0.00 σ_{max}=-40.33 (sic.=64.948)
Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-0.61 τ=6.15 τ_{max}=6.15 (sic. >100)
Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-38.30 τ=0.00 $\sigma_{ID,max}$=40.33 (sic.=64.948)

- Verifica a taglio Dir. Y [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=20.93
V,Ed=20.93 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=115.18
  V,Ed=115.18 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 107 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=-2.85 T_z=97.93 M_y=-74.59 T_y=15.44 M_z=12.73
  N,Ed=-2.85 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-74.59 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.02 (sic.=42.136)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=12.73 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=42.136)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
  Sollecitazioni: N,Ed=-58.15 My,Ed=-74.59 Mz,Ed=12.63 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.60 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976653.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.02+0.00=0.03 (sic.=35.606)
  Verifica ZZ: 0.00+0.01+0.01=0.02 (sic.=45.031)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 211
  $f_{Z,L}$=0.00 (L/77264) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{Z,G}$=0.00 (L/39676) (sic. >100)

Asta n. 3006 (-60 -61) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=-51.39 T_z=11.39 M_y=-37.88 T_y=1.61 M_z=8.16
  Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-56.83 τ=0.00 σ_{max}=-58.86 (sic.=44.496)
  Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-0.88 τ=2.38 τ_{max}=2.38 (sic. >100)
  Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-56.83 τ=0.00 $\sigma_{ID,max}$=58.86 (sic.=44.496)

- Verifica a taglio Dir. Y [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=10.71
  V,Ed=10.71 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=61.89
  V,Ed=61.89 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 107 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=-2.85 T_z=44.64 M_y=-111.90 T_y=5.22 M_z=18.30
  N,Ed=-2.85 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-111.90 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=28.088)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=18.30 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic.=84.337)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=28.088)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
  Sollecitazioni: N,Ed=-58.15 My,Ed=-111.90 Mz,Ed=18.32 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.18 M,cr=65826.80 λ_{LT}=0.22
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976653.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.03+0.01=0.04 (sic.=24.117)
  Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=30.790)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
  $f_{Z,G}$=0.00 (L/41943) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,G}$=0.00 (L/20972) (sic.=83.888)

Asta n. 3006 (-61 -62) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.34 - Classe 3
  Sollecitazioni: N=-51.39 M_y=-39.05 M_z=8.51
  Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-58.84 τ=0.00 σ_{max}=-60.87 (sic.=43.026)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)

Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-58.84 τ=0.00 $\sigma_{ID,max}$=60.87 (sic.=43.026)

- Verifica a taglio Dir. Y [4.2.16] - CC 94 SLU Xl=0.70 - Classe 1
Sollecitazioni: T_y=-2.88
V,Ed=-2.88 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=0.70 - Classe 1
Sollecitazioni: T_z=-8.66
V,Ed=-8.66 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 77 SLU Xl=0.35 - Classe 1
Sollecitazioni: N=30.06 M_y=-113.42 M_z=18.77
N,Ed=30.06 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-113.42 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=27.710)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=18.77 Mz,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic.=82.234)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=27.710)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
Sollecitazioni: N,Ed=-58.15 My,Ed=-111.92 Mz,Ed=18.32 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.00 M,cr=55637.20 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
λ_z=23.19 Ncr,z=976654.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.03+0.01=0.04 (sic.=24.113)
Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=30.786)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
$f_{Z,G}$=0.00 (L/34953) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
$f_{Z,G}$=0.00 (L/17070) (sic.=68.280)

Asta n. 3006 (-62 -63) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-51.39 T_z=-11.44 M_y=-37.90 T_y=-1.45 M_z=8.14
Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-56.79 τ=0.00 σ_{max}=-58.82 (sic.=44.529)
Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-0.88 τ=2.39 τ_{max}=2.39 (sic. >100)
Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-56.79 τ=0.00 $\sigma_{ID,max}$=58.82 (sic.=44.529)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.70 - Classe 1
Sollecitazioni: T_y=-10.36
V,Ed=-10.36 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.70 - Classe 1
Sollecitazioni: T_z=-61.96
V,Ed=-61.96 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=-44.71 M_y=-111.94 T_y=-4.87 M_z=18.25
N,Ed=0.00 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
My,Ed=-111.94 My,V,c,Rd=3142.99 My,Ed/My,V,c,Rd=0.04 (sic.=28.079) My,Ed/My,V,c,Rd=0.04 (sic.=28.079)
Mz,Ed=18.25 Mz,V,c,Rd=1543.47 Mz,Ed/Mz,V,c,Rd=0.01 (sic.=84.575) Mz,Ed/Mz,V,c,Rd=0.01 (sic.=84.575)
α=2.00 β=1.00 $(My,Ed/My,V,c,Rd)^2+(Mz,Ed/Mz,V,c,Rd)^1$=0.04 (sic.=28.079)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
Sollecitazioni: N,Ed=-58.15 My,Ed=-111.93 Mz,Ed=18.29 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.18 M,cr=65837.20 λ_{LT}=0.22
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
λ_z=23.19 Ncr,z=976652.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.03+0.01=0.04 (sic.=24.120)
Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=30.808)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 181
$f_{Z,G}$=0.00 (L/40778) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
$f_{Z,G}$=0.00 (L/19573) (sic.=78.292)

Asta n. 3006 (-63 -64) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-51.39 T_z=-29.48 M_y=-25.28 T_y=-6.01 M_z=5.69
  Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-38.55 τ=0.00 σ_{max}=-40.58 (sic.=64.541)
  Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-0.62 τ=6.16 τ_{max}=6.16 (sic. >100)
  Tensioni: σ_N=-2.03 $\sigma_{m,d}$=-38.55 τ=0.00 $\sigma_{ID,max}$=40.58 (sic.=64.541)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.70
  Sollecitazioni: T_y=-21.20
  V,Ed=-21.20 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.70
  Sollecitazioni: T_z=-115.25
  V,Ed=-115.25 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=-98.00 M_y=-74.64 T_y=-15.72 M_z=12.92
  N,Ed=0.00 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  My,Ed=-74.64 My,V,c,Rd=3142.99 My,Ed/My,V,c,Rd=0.02 (sic.=42.109) My,Ed/My,V,c,Rd=0.02 (sic.=42.109)
  Mz,Ed=12.92 Mz,V,c,Rd=1543.47 Mz,Ed/Mz,V,c,Rd=0.01 (sic. >100) Mz,Ed/Mz,V,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/My,V,c,Rd)^2+(Mz,Ed/Mz,V,c,Rd)^1$=0.02 (sic.=42.109)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
  Sollecitazioni: N,Ed=-58.15 My,Ed=-74.63 Mz,Ed=12.77 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.70 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976654.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.02+0.00=0.03 (sic.=35.523)
  Verifica ZZ: 0.00+0.01+0.01=0.02 (sic.=44.838)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 191
  $f_{Z,G}$=0.00 (L/81556) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{Z,G}$=0.00 (L/39676) (sic. >100)

Asta n. 3006 (-64 -65) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=19.02 T_z=11.43 M_y=-12.65 T_y=4.80 M_z=4.84
  Tensioni: σ_N=0.75 $\sigma_{m,d}$=24.47 τ=0.00 σ_{max}=25.22 (sic. >100)
  Tensioni: σ_N=0.75 $\sigma_{m,d}$=-0.52 τ=2.39 τ_{max}=2.39 (sic. >100)
  Tensioni: σ_N=0.75 $\sigma_{m,d}$=24.47 τ=0.00 $\sigma_{ID,max}$=25.22 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=16.98
  V,Ed=16.98 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=61.90
  V,Ed=61.90 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=12.30 T_z=44.65 M_y=-37.29 T_y=11.49 M_z=9.96
  N,Ed=12.30 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-37.29 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.01 (sic.=84.275)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=9.96 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=84.275)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
  Sollecitazioni: N,Ed=-9.77 My,Ed=-37.29 Mz,Ed=9.35 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.70 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976654.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=67.254)
  Verifica ZZ: 0.00+0.01+0.01=0.01 (sic.=78.944)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 191
  $f_{z,G}$=0.00 (L/146801) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{z,G}$=0.00 (L/81556) (sic. >100)

Asta n. 3006 (-65 -66) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=7.37 T_z=-6.63 M_y=-12.66 T_y=-7.40 M_z=8.84
  Tensioni: σ_N=0.29 $\sigma_{m,d}$=34.88 τ=0.00 σ_{max}=35.17 (sic.=74.460)
  Tensioni: σ_N=0.29 $\sigma_{m,d}$=-0.96 τ=1.39 τ_{max}=1.39 (sic. >100)
  Tensioni: σ_N=0.29 $\sigma_{m,d}$=34.88 τ=0.00 $\sigma_{ID,max}$=35.17 (sic.=74.460)

- Verifica a taglio Dir. Y [4.2.16] - CC 21 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=3.37
  V,Ed=3.37 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=8.67
  V,Ed=8.67 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 77 SLU Xl=0.35 - Classe 1
  Sollecitazioni: N=-1.97 M_y=-38.89 T_y=-7.74 M_z=4.95
  N,Ed=-1.97 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-38.89 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.01 (sic.=80.822)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=4.95 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=80.822)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
  Sollecitazioni: N,Ed=-9.77 My,Ed=-37.39 Mz,Ed=9.35 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.00 M,cr=55645.10 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_Z=23.19 Ncr,z=976652.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=67.117)
  Verifica ZZ: 0.00+0.01+0.01=0.01 (sic.=78.831)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
  $f_{z,G}$=0.00 (L/81556) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
  $f_{z,G}$=0.00 (L/45875) (sic. >100)

Asta n. 3006 (-66 -67) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=7.37 T_z=-11.40 M_y=-12.63 T_y=-10.52 M_z=8.84
  Tensioni: σ_N=0.29 $\sigma_{m,d}$=34.85 τ=0.00 σ_{max}=35.15 (sic.=74.520)
  Tensioni: σ_N=0.29 $\sigma_{m,d}$=-0.96 τ=2.39 τ_{max}=2.39 (sic. >100)
  Tensioni: σ_N=0.29 $\sigma_{m,d}$=34.85 τ=0.00 $\sigma_{ID,max}$=35.15 (sic.=74.520)

- Verifica a taglio Dir. Z [4.2.16] - CC 79 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-54.23
  V,Ed=-54.23 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-14.01 T_z=-44.70 M_y=-37.33 T_y=-2.92 M_z=3.96
  N,Ed=-14.01 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-37.33 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.01 (sic.=84.205)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=3.96 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=84.205)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
  Sollecitazioni: N,Ed=-9.77 My,Ed=-37.33 Mz,Ed=8.91 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.60 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_Z=23.19 Ncr,z=976652.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95

Verifica YY: 0.00+0.01+0.00=0.01 (sic.=67.929)
Verifica ZZ: 0.00+0.01+0.01=0.01 (sic.=80.591)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
$f_{z,G}$=0.00 (L/122334) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
$f_{z,G}$=0.00 (L/66728) (sic. >100)

Asta n. 3007 (-72 -73) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.75 - Classe 3
Sollecitazioni: N=14.72 T_z=25.67 M_y=-25.66 T_y=-7.29 M_z=-5.47
Tensioni: σ_N=0.58 $\sigma_{m,d}$=38.34 τ=0.00 σ_{max}=38.92 (sic.=67.285)
Tensioni: σ_N=0.58 $\sigma_{m,d}$=0.59 τ=5.37 τ_{max}=5.37 (sic. >100)
Tensioni: σ_N=0.58 $\sigma_{m,d}$=38.34 τ=0.00 $\sigma_{ID,max}$=38.92 (sic.=67.285)

- Verifica a taglio Dir. Y [4.2.16] - CC 82 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-3.23
V,Ed=-3.23 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 82 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=167.10
V,Ed=167.10 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic.=76.530)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 82 SLU Xl=0.75 - Classe 1
Sollecitazioni: N=-55.72 T_z=112.29 M_y=-104.77 T_y=-6.18 M_z=-3.53
N,Ed=-55.72 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-104.77 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=29.999)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-3.53 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=29.999)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 102 SLU - Classe 1
Sollecitazioni: N,Ed=-49.47 My,Ed=-103.48 Mz,Ed=-7.59 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=85658.40 λ_{LT}=0.20
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
λ_z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.03+0.00=0.03 (sic.=28.716)
Verifica ZZ: 0.00+0.02+0.00=0.02 (sic.=41.297)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 181
$f_{z,G}$=0.00 (L/42510) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
$f_{z,L}$=0.00 (L/28087) (sic. >100)

Asta n. 3007 (-73 -74) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.75 - Classe 3
Sollecitazioni: N=14.56 T_z=2.97 M_y=-32.58 T_y=-11.32 M_z=-8.58
Tensioni: σ_N=0.57 $\sigma_{m,d}$=52.94 τ=0.00 σ_{max}=53.51 (sic.=48.944)
Tensioni: σ_N=0.57 $\sigma_{m,d}$=-20.95 τ=0.84 τ_{max}=0.84 (sic. >100)
Tensioni: σ_N=0.57 $\sigma_{m,d}$=52.94 τ=0.00 $\sigma_{ID,max}$=53.51 (sic.=48.944)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-9.00
V,Ed=-9.00 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=71.14
V,Ed=71.14 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.75 - Classe 1
Sollecitazioni: N=-47.36 T_z=16.33 M_y=-136.81 T_y=-11.95 M_z=-13.68
N,Ed=-47.36 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-136.81 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=22.974)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-13.68 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=22.974)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
Sollecitazioni: N,Ed=-57.82 My,Ed=-134.93 Mz,Ed=-19.58 L=0.75

αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.12 M,cr=54729.10 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
λ_Z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.04+0.01=0.05 (sic.=20.456)
Verifica ZZ: 0.00+0.02+0.01=0.04 (sic.=26.715)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 211
$f_{Z,L}$=0.00 (L/24198) (sic.=80.660)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
$f_{Z,L}$=0.00 (L/16050) (sic.=64.200)

Asta n. 3007 (-74 -75) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=14.56 T_z=-1.86 M_y=-32.58 T_y=6.29 M_z=-8.58
Tensioni: σ_N=0.57 $\sigma_{m,d}$=52.93 τ=0.00 σ_{max}=53.51 (sic.=48.947)
Tensioni: σ_N=0.57 $\sigma_{m,d}$=-20.94 τ=0.46 τ_{max}=0.46 (sic. >100)
Tensioni: σ_N=0.57 $\sigma_{m,d}$=52.93 τ=0.00 $\sigma_{ID,max}$=53.51 (sic.=48.947)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_y=7.66
V,Ed=7.66 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_z=-71.56
V,Ed=-71.56 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-47.36 T_z=-16.75 M_y=-136.80 T_y=10.62 M_z=-13.68
N,Ed=-47.36 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-136.80 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=22.974)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-13.68 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=22.974)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
Sollecitazioni: N,Ed=-57.82 My,Ed=-134.92 Mz,Ed=-19.58 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.12 M,cr=55040.20 λ_{LT}=0.24
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
λ_Z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.04+0.01=0.05 (sic.=20.457)
Verifica ZZ: 0.00+0.02+0.01=0.04 (sic.=26.715)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 181
$f_{Z,G}$=0.00 (L/23476) (sic.=78.253)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 211
$f_{Z,G}$=0.00 (L/15271) (sic.=61.084)

Asta n. 3007 (-75 -76) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=14.56 T_z=-24.50 M_y=-24.78 T_y=5.16 M_z=-3.87
Tensioni: σ_N=0.57 $\sigma_{m,d}$=33.35 τ=0.00 σ_{max}=33.92 (sic.=77.213)
Tensioni: σ_N=0.57 $\sigma_{m,d}$=0.42 τ=5.12 τ_{max}=5.12 (sic. >100)
Tensioni: σ_N=0.57 $\sigma_{m,d}$=33.35 τ=0.00 $\sigma_{ID,max}$=33.92 (sic.=77.213)

- Verifica a taglio Dir. Y [4.2.16] - CC 112 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_y=7.63
V,Ed=7.63 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.75 - Classe 1
Sollecitazioni: T_z=-165.70
V,Ed=-165.70 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic.=77.178)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 112 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-47.36 T_z=-110.88 M_y=-103.72 T_y=10.58 M_z=-6.83
N,Ed=-47.36 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-103.72 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=30.304)

Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-6.83 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=30.304)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
Sollecitazioni: N,Ed=-57.82 My,Ed=-102.76 Mz,Ed=-9.85 L=0.75
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=85658.30 λ_{LT}=0.20
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=15.33 Ncr,y=2233510.00 λ^*_y=0.18 Curva b: Φ_y=0.51 χ_y=1.00
λ_Z=24.84 Ncr,z=850774.00 λ^*_z=0.29 Curva c: Φ_z=0.56 χ_z=0.96
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.03+0.00=0.04 (sic.=28.115)
Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=39.049)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 196
$f_{Z,G}$=0.00 (L/42510) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
$f_{Z,L}$=0.00 (L/27594) (sic. >100)

Asta n. 3007 (-76 -77) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.70 - Classe 3
Sollecitazioni: N=36.46 T_z=32.00 M_y=-27.27 T_y=3.35 M_z=2.35
Tensioni: σ_N=1.44 $\sigma_{m,d}$=31.75 τ=0.00 σ_{max}=33.19 (sic.=78.916)
Tensioni: σ_N=1.44 $\sigma_{m,d}$=-0.25 τ=6.69 τ_{max}=6.69 (sic. >100)
Tensioni: σ_N=1.44 $\sigma_{m,d}$=31.75 τ=0.00 $\sigma_{ID,max}$=33.19 (sic.=78.916)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=4.10
V,Ed=4.10 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=122.25
V,Ed=122.25 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.70 - Classe 1
Sollecitazioni: N=-99.59 T_z=104.15 M_y=-79.24 T_y=4.10 M_z=2.87
N,Ed=-99.59 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-79.24 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=39.664)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=2.87 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=39.664)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
Sollecitazioni: N,Ed=-100.41 My,Ed=-79.24 Mz,Ed=2.87 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.60 λ_{LT}=0.18
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
λ_Z=23.19 Ncr,z=976653.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.02+0.00=0.03 (sic.=37.706)
Verifica ZZ: 0.00+0.01+0.00=0.02 (sic.=56.494)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
$f_{Z,L}$=0.00 (L/73400) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
$f_{Z,G}$=0.00 (L/38632) (sic. >100)

Asta n. 3007 (-77 -78) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.70 - Classe 3
Sollecitazioni: N=36.46 T_z=12.62 M_y=-40.96 T_y=1.97 M_z=3.72
Tensioni: σ_N=1.44 $\sigma_{m,d}$=48.17 τ=0.00 σ_{max}=49.61 (sic.=52.791)
Tensioni: σ_N=1.44 $\sigma_{m,d}$=-0.40 τ=2.64 τ_{max}=2.64 (sic. >100)
Tensioni: σ_N=1.44 $\sigma_{m,d}$=48.17 τ=0.00 $\sigma_{ID,max}$=49.61 (sic.=52.791)

- Verifica a taglio Dir. Y [4.2.16] - CC 97 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=3.04
V,Ed=3.04 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 97 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=65.98
V,Ed=65.98 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 87 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=113.60 T_z=47.88 M_y=-119.03 T_y=3.02 M_z=4.90
  N,Ed=113.60 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-119.03 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=26.405)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=4.90 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.04 (sic.=26.405)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-100.41 My,Ed=-119.02 Mz,Ed=4.88 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.18 M,cr=65873.80 λ_{LT}=0.22
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976653.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.04+0.00=0.04 (sic.=25.451)
  Verifica ZZ: 0.00+0.02+0.00=0.03 (sic.=38.230)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{Z,L}$=0.00 (L/40778) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/20972) (sic.=83.888)

Asta n. 3007 (-78 -79) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.35 - Classe 3
  Sollecitazioni: N=36.46 M_y=-42.17 M_z=3.73
  Tensioni: σ_N=1.44 $\sigma_{m,d}$=49.34 τ=0.00 σ_{max}=50.78 (sic.=51.574)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=1.44 $\sigma_{m,d}$=49.34 τ=0.00 $\sigma_{ID,max}$=50.78 (sic.=51.574)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=9.13
  V,Ed=9.13 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 87 SLU Xl=0.35 - Classe 1
  Sollecitazioni: N=113.60 M_y=-120.61 M_z=4.93
  N,Ed=113.60 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-120.61 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=26.060)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=4.93 Mz,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.04 (sic.=26.060)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-100.41 My,Ed=-119.04 Mz,Ed=4.94 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.00 M,cr=55641.20 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976654.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.04+0.00=0.04 (sic.=25.434)
  Verifica ZZ: 0.00+0.02+0.00=0.03 (sic.=38.172)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 191
  $f_{Z,L}$=0.00 (L/33364) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 191
  $f_{Z,G}$=0.00 (L/17070) (sic.=68.280)

Asta n. 3007 (-79 -80) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=36.46 T_z=-12.63 M_y=-40.95 T_y=-2.13 M_z=3.75
  Tensioni: σ_N=1.44 $\sigma_{m,d}$=48.24 τ=0.00 σ_{max}=49.68 (sic.=52.722)
  Tensioni: σ_N=1.44 $\sigma_{m,d}$=-0.41 τ=2.64 τ_{max}=2.64 (sic. >100)
  Tensioni: σ_N=1.44 $\sigma_{m,d}$=48.24 τ=0.00 $\sigma_{ID,max}$=49.68 (sic.=52.722)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_y=-3.41
  V,Ed=-3.41 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-66.02
  V,Ed=-66.02 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-99.59 T_z=-47.92 M_y=-119.01 T_y=-3.41 M_z=4.97
  N,Ed=-99.59 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-119.01 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=26.409)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=4.97 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=26.409)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-100.41 My,Ed=-119.01 Mz,Ed=4.95 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.18 M,cr=65887.50 λ_{LT}=0.22
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976652.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.04+0.00=0.04 (sic.=25.438)
  Verifica ZZ: 0.00+0.02+0.00=0.03 (sic.=38.172)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
  $f_{Z,L}$=0.00 (L/37641) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{Z,L}$=0.00 (L/19573) (sic.=78.292)

Asta n. 3007 (-80 -81) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=36.46 T_z=-31.92 M_y=-27.22 T_y=-3.24 M_z=2.27
  Tensioni: σ_N=1.44 $\sigma_{m,d}$=31.50 τ=0.00 σ_{max}=32.94 (sic.=79.517)
  Tensioni: σ_N=1.44 $\sigma_{m,d}$=-0.25 τ=6.67 τ_{max}=6.67 (sic. >100)
  Tensioni: σ_N=1.44 $\sigma_{m,d}$=31.50 τ=0.00 $\sigma_{ID,max}$=32.94 (sic.=79.517)

- Verifica a taglio Dir. Y [4.2.16] - CC 107 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_y=-3.92
  V,Ed=-3.92 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.70 - Classe 1
  Sollecitazioni: T_z=-122.12
  V,Ed=-122.12 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=133.61 T_z=-104.02 M_y=-79.15 T_y=-3.92 M_z=2.74
  N,Ed=133.61 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-79.15 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=39.711)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=2.74 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=39.711)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-100.41 My,Ed=-79.12 Mz,Ed=2.67 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.70 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976654.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.02+0.00=0.03 (sic.=37.859)
  Verifica ZZ: 0.00+0.01+0.00=0.02 (sic.=56.950)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 186
  $f_{Z,L}$=0.00 (L/73400) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/37641) (sic. >100)

Asta n. 3007 (-81 -82) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=36.62 T_z=41.60 M_y=-34.70 T_y=-5.80 M_z=-4.06
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=43.19 τ=0.00 σ_{max}=44.63 (sic.=58.680)
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=0.44 τ=8.70 τ_{max}=8.70 (sic. >100)

Tensioni: σ_N=1.45 $\sigma_{m,d}$=43.19 τ=0.00 $\sigma_{ID,max}$=44.63 (sic.=58.680)

- Verifica a taglio Dir. Y [4.2.16] - CC 102 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-6.60
  V,Ed=-6.60 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 102 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=205.66
  V,Ed=205.66 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.02 (sic.=62.181)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 102 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=-61.44 T_z=154.50 M_y=-126.06 T_y=-9.36 M_z=-5.59
  N,Ed=-61.44 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-126.06 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=24.933)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-5.59 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=24.933)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-81.44 My,Ed=-125.26 Mz,Ed=-8.09 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=97356.70 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976654.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.04+0.00=0.04 (sic.=23.768)
  Verifica ZZ: 0.00+0.02+0.00=0.03 (sic.=34.526)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 186
  $f_{Z,G}$=0.00 (L/39676) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.00 (L/24066) (sic.=96.264)

Asta n. 3007 (-82 -83) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=36.62 T_z=19.58 M_y=-53.99 T_y=-3.58 M_z=-6.57
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=67.84 τ=0.00 σ_{max}=69.28 (sic.=37.802)
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=0.71 τ=4.09 τ_{max}=4.09 (sic. >100)
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=67.84 τ=0.00 $\sigma_{ID,max}$=69.28 (sic.=37.802)

- Verifica a taglio Dir. Y [4.2.16] - CC 102 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-8.33
  V,Ed=-8.33 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 102 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=117.00
  V,Ed=117.00 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 102 SLU Xl=0.70 - Classe 1
  Sollecitazioni: N=-61.44 T_z=65.84 M_y=-189.96 T_y=-11.08 M_z=-12.35
  N,Ed=-61.44 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-189.96 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.06 (sic.=16.545)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-12.35 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.545)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-81.44 My,Ed=-189.03 Mz,Ed=-15.28 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.19 M,cr=65994.60 λ_{LT}=0.22
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.49 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976652.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.06+0.01=0.06 (sic.=15.625)
  Verifica ZZ: 0.00+0.03+0.01=0.04 (sic.=22.246)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 186
  $f_{Z,L}$=0.00 (L/22243) (sic.=74.143)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,L}$=0.01 (L/13346) (sic.=53.384)

Asta n. 3007 (-83 -84) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.70 - Classe 3
  Sollecitazioni: N=36.62 T_z=-7.04 M_y=-60.60 T_y=-20.22 M_z=-20.74
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=110.87 τ=0.00 σ_{max}=112.31 (sic.=23.319)
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=-34.75 τ=1.54 τ_{max}=1.54 (sic. >100)
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=110.87 τ=0.00 $\sigma_{ID,max}$=112.31 (sic.=23.319)

- Verifica a taglio Dir. Y [4.2.16] - CC 102 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-1.90
  V,Ed=-1.90 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 102 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=30.94
  V,Ed=30.94 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 102 SLU Xl=0.42 - Classe 1
  Sollecitazioni: N=-61.44 M_y=-196.56 T_y=-3.55 M_z=-13.51
  N,Ed=-61.44 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-196.56 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.06 (sic.=15.990)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-13.51 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=15.990)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-81.44 My,Ed=-189.69 Mz,Ed=-27.43 L=0.70
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.70 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.00 M,cr=55714.00 λ_{LT}=0.24
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=14.31 Ncr,y=2563980.00 λ^*_y=0.16 Curva b: Φ_y=0.51 χ_y=1.00
  λ_z=23.19 Ncr,z=976652.00 λ^*_z=0.27 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.06+0.01=0.07 (sic.=14.559)
  Verifica ZZ: 0.00+0.03+0.02=0.05 (sic.=19.029)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
  $f_{Z,L}$=0.00 (L/18124) (sic.=60.413)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
  $f_{Z,G}$=0.01 (L/10638) (sic.=42.552)

Asta n. 3007 (-84 -85) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=36.83 T_z=-27.40 M_y=-60.68 T_y=14.82 M_z=-20.75
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=110.99 τ=0.00 σ_{max}=112.44 (sic.=23.293)
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=2.25 τ=5.73 τ_{max}=5.73 (sic. >100)
  Tensioni: σ_N=1.45 $\sigma_{m,d}$=110.99 τ=0.00 $\sigma_{ID,max}$=112.44 (sic.=23.293)

- Verifica a taglio Dir. Y [4.2.16] - CC 102 SLU Xl=1.40 - Classe 1
  Sollecitazioni: T_y=7.76
  V,Ed=7.76 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 102 SLU Xl=1.40 - Classe 1
  Sollecitazioni: T_z=-189.69
  V,Ed=-189.69 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic.=67.416)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 102 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-61.31 T_z=-87.37 M_y=-193.94 T_y=13.27 M_z=-14.72
  N,Ed=-61.31 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-193.94 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.06 (sic.=16.206)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-14.72 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=16.206)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-80.31 My,Ed=-189.87 Mz,Ed=-27.48 L=1.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=28885.00 λ_{LT}=0.34
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=28.62 Ncr,y=640996.00 λ^*_y=0.33 Curva b: Φ_y=0.58 χ_y=0.95
  λ_z=46.38 Ncr,z=244163.00 λ^*_z=0.53 Curva c: Φ_z=0.72 χ_z=0.82
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.06+0.01=0.07 (sic.=14.530)
  Verifica ZZ: 0.00+0.03+0.02=0.05 (sic.=18.927)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
  $f_{Z,L}$=0.01 (L/14904) (sic.=49.680)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
  $f_{Z,L}$=0.02 (L/8610) (sic.=34.440)

Asta n. 3008 (-68 -69) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.50 - Classe 3
  Sollecitazioni: N=-85.89 M_y=-27.51 M_z=-8.75
  Tensioni: σ_N=-3.39 $\sigma_{m,d}$=-48.61 τ=0.00 σ_{max}=-52.00 (sic.=50.363)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=-3.39 $\sigma_{m,d}$=-48.61 τ=0.00 $\sigma_{ID,max}$=52.00 (sic.=50.363)

- Verifica a taglio Dir. Y [4.2.16] - CC 77 SLU Xl=3.00 - Classe 1
  Sollecitazioni: T_y=43.46
  V,Ed=43.46 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 77 SLU Xl=3.00 - Classe 1
  Sollecitazioni: T_z=-175.56
  V,Ed=-175.56 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic.=72.843)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 77 SLU Xl=1.50 - Classe 1
  Sollecitazioni: N=4.64 M_y=-131.67 M_z=-32.60
  N,Ed=4.64 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-131.67 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.04 (sic.=23.871)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-32.60 Mz,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.02 (sic.=47.350)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=23.871)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
  Sollecitazioni: N,Ed=-81.58 My,Ed=-131.67 Mz,Ed=-32.60 L=3.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=9722.42 λ_{LT}=0.58
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_y=61.33 Ncr,y=139595.00 λ^*_y=0.71 Curva b: Φ_y=0.84 χ_y=0.78
  λ_z=99.38 Ncr,z=53173.30 λ^*_z=1.14 Curva c: Φ_z=1.39 χ_z=0.46
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.04+0.01=0.06 (sic.=18.001)
  Verifica ZZ: 0.00+0.03+0.02=0.05 (sic.=20.859)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
  $f_{Z,G}$=0.05 (L/5714) $f_{Z,L}$=0.05 (L/6446) (sic.=19.047)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{Z,G}$=0.08 (L/3900) $f_{Z,L}$=0.07 (L/4494) (sic.=15.600)

Asta n. 3010 (-51 -52) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.50 - Classe 3
  Sollecitazioni: N=102.92 M_y=-24.42 M_z=-7.77
  Tensioni: σ_N=4.06 $\sigma_{m,d}$=43.15 τ=0.00 σ_{max}=47.21 (sic.=55.478)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=4.06 $\sigma_{m,d}$=43.15 τ=0.00 $\sigma_{ID,max}$=47.21 (sic.=55.478)

- Verifica a taglio Dir. Y [4.2.16] - CC 77 SLU Xl=3.00 - Classe 1
  Sollecitazioni: T_y=27.61
  V,Ed=27.61 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 77 SLU Xl=3.00 - Classe 1
  Sollecitazioni: T_z=-106.26
  V,Ed=-106.26 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 77 SLU Xl=1.50 - Classe 1
  Sollecitazioni: N=-204.67 M_y=-79.69 M_z=-20.71
  N,Ed=-204.67 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-79.69 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=39.439)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-20.71 Mz,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic.=74.534)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=39.439)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 1
  Sollecitazioni: N,Ed=-211.68 My,Ed=-79.69 Mz,Ed=-20.71 L=3.00
  αmy, αmz, αLT=0.95, 0.95, 0.95

L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=9722.42 λ_{LT}=0.58
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
λ_y=61.33 Ncr,y=139595.00 λ^*_y=0.71 Curva b: Φ_y=0.84 χ_y=0.78
λ_z=99.38 Ncr,z=53173.30 λ^*_z=1.14 Curva c: Φ_z=1.39 χ_z=0.46
Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.57, 0.96
Verifica YY: 0.00+0.03+0.01=0.04 (sic.=26.881)
Verifica ZZ: 0.01+0.02+0.01=0.04 (sic.=28.553)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
$f_{Z,G}$=0.03 (L/11398) $f_{Z,L}$=0.02 (L/12866) (sic.=37.993)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
$f_{Z,G}$=0.05 (L/6235) $f_{Z,L}$=0.04 (L/7240) (sic.=24.940)

Asta n. 3010 (-52 -53) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.75 - Classe 3
Sollecitazioni: N=-599.12 M_y=-29.02 M_z=-9.23
Tensioni: σ_N=-23.65 $\sigma_{m,d}$=-51.29 τ=0.00 σ_{max}=-74.93 (sic.=34.952)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=-23.65 $\sigma_{m,d}$=-51.29 τ=0.00 $\sigma_{ID,max}$=74.93 (sic.=34.952)

- Verifica a taglio Dir. Y [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-13.72
V,Ed=-13.72 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 17 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=43.12
V,Ed=43.12 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 17 SLU Xl=1.75 - Classe 1
Sollecitazioni: N=-158.82 M_y=-37.73 M_z=-12.00
N,Ed=-158.82 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-37.73 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.01 (sic.=83.305)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-12.00 Mz,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=83.305)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
Sollecitazioni: N,Ed=-784.14 My,Ed=-37.73 Mz,Ed=-12.00 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=8044.65 λ_{LT}=0.64
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.69 β_{LT}=0.75 f=0.97 χ_{LT}=0.92
λ_y=71.56 Ncr,y=102559.00 λ^*_y=0.82 Curva b: Φ_y=0.95 χ_y=0.71
λ_z=115.94 Ncr,z=39066.10 λ^*_z=1.34 Curva c: Φ_z=1.67 χ_z=0.37
Kyy, Kyz, Kzy, Kzz=0.96, 0.60, 0.58, 0.99
Verifica YY: 0.02+0.01+0.00=0.03 (sic.=29.633)
Verifica ZZ: 0.03+0.01+0.01=0.05 (sic.=21.380)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 138
$f_{Z,L}$=0.00 (L/1835010) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 189
$f_{Z,G}$=0.04 (L/9919) $f_{Z,L}$=0.03 (L/11974) (sic.=39.676)

Asta n. 3010 (-53 -54) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.75 - Classe 3
Sollecitazioni: N=-580.70 M_y=-33.23 M_z=-10.57
Tensioni: σ_N=-22.92 $\sigma_{m,d}$=-58.73 τ=0.00 σ_{max}=-81.65 (sic.=32.078)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=-22.92 $\sigma_{m,d}$=-58.73 τ=0.00 $\sigma_{ID,max}$=81.65 (sic.=32.078)

- Verifica a taglio Dir. Y [4.2.16] - CC 77 SLU Xl=3.50 - Classe 1
Sollecitazioni: T_y=32.21
V,Ed=32.21 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 77 SLU Xl=3.50 - Classe 1
Sollecitazioni: T_z=-123.97
V,Ed=-123.97 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 77 SLU Xl=1.75 - Classe 1
Sollecitazioni: N=-323.27 M_y=-108.47 M_z=-28.19
N,Ed=-323.27 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-108.47 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.03 (sic.=28.975)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-28.19 Mz,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.02 (sic.=54.760)

α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=28.975)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 1
  Sollecitazioni: N,Ed=-596.39 My,Ed=-108.47 Mz,Ed=-28.19 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=8044.65 λ_{LT}=0.64
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.69 β_{LT}=0.75 f=0.97 χ_{LT}=0.92
  λ_y=71.56 Ncr,y=102559.00 λ^*_y=0.82 Curva b: Φ_y=0.95 χ_y=0.71
  λ_z=115.94 Ncr,z=39066.10 λ^*_z=1.34 Curva c: Φ_z=1.67 χ_z=0.37
  Kyy, Kyz, Kzy, Kzz=0.96, 0.59, 0.57, 0.98
  Verifica YY: 0.01+0.04+0.01=0.06 (sic.=16.903)
  Verifica ZZ: 0.02+0.02+0.02=0.06 (sic.=15.775)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 181
  $f_{z,G}$=0.05 (L/7196) $f_{z,L}$=0.04 (L/8120) (sic.=23.987)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
  $f_{z,G}$=0.09 (L/3938) $f_{z,L}$=0.08 (L/4576) (sic.=15.752)

Asta n. 3013 (201 -38) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-862.88 T_z=186.08 M_y=-428.31 T_y=-209.36 M_z=225.72
  Tensioni: σ_N=-11.05 $\sigma_{m,d}$=-187.86 τ=0.00 σ_{max}=-198.91 (sic.=13.167)
  Tensioni: σ_N=-11.05 $\sigma_{m,d}$=-5.07 τ=12.21 τ_{max}=12.21 (sic. >100)
  Tensioni: σ_N=-11.05 $\sigma_{m,d}$=-187.86 τ=0.00 $\sigma_{ID,max}$=198.91 (sic.=13.167)

- Verifica a taglio Dir. Y [4.2.16] - CC 21 SLU Xl=1.15 - Classe 1
  Sollecitazioni: T_y=150.21
  V,Ed=150.21 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=1.15 - Classe 1
  Sollecitazioni: T_z=-265.92
  V,Ed=-265.92 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=-1101.12 T_z=65.54 M_y=52.79 T_y=-329.79 M_z=295.19
  N,Ed=-1101.12 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=52.79 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.00 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=295.19 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.04 (sic.=27.158)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.04 (sic.=27.151)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-862.88 My,Ed=-428.31 Mz,Ed=225.72 L=1.15
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.23 M,cr=1450430.00 λ_{LT}=0.10
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=6.76 Ncr,y=35440800.00 λ^*_y=0.08 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=11.39 Ncr,z=12464500.00 λ^*_z=0.13 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.03+0.04=0.07 (sic.=13.816)
  Verifica ZZ: 0.00+0.02+0.04=0.07 (sic.=14.942)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
  $f_{z,G}$=0.01 (L/12988) $f_{z,L}$=0.00 (L/92541) (sic.=43.293)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 194
  $f_{z,G}$=0.01 (L/12764) $f_{z,L}$=0.00 (L/35822) (sic.=51.056)

Asta n. 3013 (-38 -55) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-818.06 T_z=-293.99 M_y=-316.66 T_y=-40.21 M_z=18.99
  Tensioni: σ_N=-10.48 $\sigma_{m,d}$=-65.07 τ=0.00 σ_{max}=-75.55 (sic.=34.668)
  Tensioni: σ_N=-10.48 $\sigma_{m,d}$=-0.43 τ=19.25 τ_{max}=19.25 (sic.=78.566)
  Tensioni: σ_N=-10.48 $\sigma_{m,d}$=-65.07 τ=0.00 $\sigma_{ID,max}$=75.55 (sic.=34.668)

- Verifica a taglio Dir. Y [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=88.29
  V,Ed=88.29 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-372.68
  V,Ed=-372.68 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-1381.03 T_z=-262.94 M_y=-336.20 T_y=-49.02 M_z=62.61
  N,Ed=-1381.03 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-336.20 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=50.214)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=62.61 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=50.214)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 94 SLU - Classe 1
  Sollecitazioni: N,Ed=-1381.03 My,Ed=-336.20 Mz,Ed=62.61 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.31 M,cr=6066080.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=5.70 Ncr,z=49857900.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.02+0.00=0.03 (sic.=33.234)
  Verifica ZZ: 0.01+0.01+0.01=0.03 (sic.=39.233)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 189
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/242083) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 204
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/201735) (sic.=51.508)

Asta n. 3013 (-55 -72) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-790.87 T_z=-409.72 M_y=89.87 T_y=-33.53 M_z=-1.11
  Tensioni: σ_N=-10.13 $\sigma_{m,d}$=-16.33 τ=0.00 σ_{max}=-26.46 (sic.=98.980)
  Tensioni: σ_N=-10.13 $\sigma_{m,d}$=0.02 τ=26.82 τ_{max}=26.82 (sic.=56.376)
  Tensioni: σ_N=-10.13 $\sigma_{m,d}$=-10.60 τ=25.21 $\sigma_{ID,max}$=48.33 (sic.=54.187)

- Verifica a taglio Dir. Y [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=-1.09
  V,Ed=-1.09 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-558.47
  V,Ed=-558.47 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=67.240)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 76 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-1535.99 T_z=-451.36 M_y=192.97 T_y=25.14 M_z=2.33
  N,Ed=-1535.99 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=192.97 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic.=87.483)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=2.33 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=87.483)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 110 SLU - Classe 1
  Sollecitazioni: N,Ed=-1494.35 My,Ed=185.86 Mz,Ed=-32.59 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.71 M,cr=7914500.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.01+0.00=0.02 (sic.=49.842)
  Verifica ZZ: 0.01+0.01+0.00=0.02 (sic.=57.391)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 214
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/1210410) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 184
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/302603) (sic.=51.508)

Asta n. 3014 (-39 -56) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica a trazione (4.2.4.1.2.1) - CC 13 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=24.27 T_z=-4.91
  Verifica a trazione [4.2.5]
  N,Ed=24.27 Npl,Rd=34598.90 Nu,Rd=40899.70 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 77 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=38.36
  V,Ed=38.36 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 86 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=23.62
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=5.37 τ_{max}=5.37 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=5.37 $\sigma_{ID,max}$=9.30 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-24.23 My,Ed=-5.53 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172145.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
  Verifica YY: 0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 151
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/403471) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 161
  $f_{Z,G}$=0.00 (L/12741) $f_{Z,L}$=0.00 (L/403471) (sic.=50.964)

Asta n. 3014 (-56 -73) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 11 SND Xl=0.58 - Classe 3
  Sollecitazioni: T_z=-4.91
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.12 τ_{max}=1.12 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.12 $\sigma_{ID,max}$=1.93 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 74 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-30.11
  V,Ed=-30.11 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 74 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-30.11
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.84 τ_{max}=6.84 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.84 $\sigma_{ID,max}$=11.86 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-12.44 My,Ed=-5.53 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
  Verifica YY: 0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 156
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/1210410) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 209
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/1210410) (sic.=52.060)

Asta n. 3015 (-24 -27) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-87.62 M_y=-2.80 T_y=4.39 M_z=2.53
  Tensioni: σ_N=-6.63 $\sigma_{m,d}$=-34.57 τ=0.00 σ_{max}=-41.21 (sic.=63.560)
  Tensioni: σ_N=-6.63 $\sigma_{m,d}$=3.13 τ=0.74 τ_{max}=0.74 (sic. >100)
  Tensioni: σ_N=-6.63 $\sigma_{m,d}$=-34.57 τ=0.00 $\sigma_{ID,max}$=41.21 (sic.=63.560)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=43.73
  V,Ed=43.73 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 67 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-27.79 T_z=1.37 M_y=-3.05 T_y=6.35 M_z=3.67
  N,Ed=-27.79 Nc,Rd=34598.90 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-3.05 My,V,c,Rd=1595.68 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.00 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=3.67 Mz,V,c,Rd=356.17 MNz,c,Rd=356.17 Mz,Ed/MNz,c,Rd=0.01 (sic.=97.134)

α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.01 (sic.=97.099)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-90.09 My,Ed=-2.80 Mz,Ed=2.53 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.28
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.00+0.01=0.02 (sic.=65.992)
  Verifica ZZ: 0.00+0.00+0.01=0.02 (sic.=66.432)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
  $f_{Z,G}$=0.00 (L/13157) $f_{Z,L}$=0.00 (L/403471) (sic.=43.857)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 136
  $f_{Z,G}$=0.00 (L/13157) $f_{Z,L}$=0.00 (L/605207) (sic.=52.628)

Asta n. 3015 (-27 -40) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-87.10 M_y=-2.72 T_y=-4.39 M_z=2.53
  Tensioni: σ_N=-6.59 $\sigma_{m,d}$=-34.42 τ=0.00 σ_{max}=-41.01 (sic.=63.864)
  Tensioni: σ_N=-6.59 $\sigma_{m,d}$=3.28 τ=0.74 τ_{max}=0.74 (sic. >100)
  Tensioni: σ_N=-6.59 $\sigma_{m,d}$=-34.42 τ=0.00 $\sigma_{ID,max}$=41.01 (sic.=63.864)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-35.08
  V,Ed=-35.08 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 67 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-27.13 M_y=-2.69 T_y=-6.35 M_z=3.67
  N,Ed=-27.13 Nc,Rd=34598.90 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-2.69 My,c,Rd=1595.68 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.00 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=3.67 Mz,V,c,Rd=356.17 MNz,c,Rd=356.17 Mz,Ed/MNz,c,Rd=0.01 (sic.=97.134)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.01 (sic.=97.107)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-87.10 My,Ed=-2.72 Mz,Ed=2.53 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.28
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172145.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.00+0.01=0.02 (sic.=66.623)
  Verifica ZZ: 0.00+0.00+0.01=0.01 (sic.=67.063)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/605206) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 179
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/302603) (sic.=52.060)

Asta n. 3015 (-40 -57) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica a compressione (4.2.4.1.2.2) - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-42.72 T_z=3.88
  Verifica a compressione [4.2.9]
  N,Ed=-42.72 Nc,Rd=-34598.90 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 77 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=21.03
  V,Ed=21.03 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a compressione (4.2.4.1.2.2) - CC 87 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-91.94 T_z=21.03
  Verifica a compressione [4.2.9]
  N,Ed=-91.94 Nc,Rd=-34598.90 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 1
  Sollecitazioni: N,Ed=-91.94 My,Ed=-3.03 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00

λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=39.88 Ncr,z=172145.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.00=0.00 (sic. >100)
Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 151
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/605206) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 151
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/302603) (sic.=51.508)

Asta n. 3015 (-57 -74) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.58 - Classe 3
Sollecitazioni: T_z=-4.91
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.12 τ_{max}=1.12 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.12 $\sigma_{ID,max}$=1.93 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 77 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=38.36
V,Ed=38.36 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 77 SLU Xl=0.29 - Classe 1
Sollecitazioni: N=-30.86 M_y=-5.53
My,Ed=-5.53 My,c,Rd=1595.68
N,Ed=-30.86 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.00 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 1
Sollecitazioni: N,Ed=-46.24 My,Ed=-5.53 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.00=0.00 (sic. >100)
Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 136
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/605207) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 141
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/605207) (sic.=52.060)

Asta n. 3016 (204 -28) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
Sollecitazioni: N=-87.21 T_z=2.80 M_y=-3.54 T_y=3.45 M_z=1.73
Tensioni: σ_N=-6.60 $\sigma_{m,d}$=-26.65 τ=0.00 σ_{max}=-33.25 (sic.=78.760)
Tensioni: σ_N=-6.60 $\sigma_{m,d}$=-1.37 τ=0.64 τ_{max}=0.64 (sic. >100)
Tensioni: σ_N=-6.60 $\sigma_{m,d}$=-26.65 τ=0.00 $\sigma_{ID,max}$=33.25 (sic.=78.760)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.08 - Classe 1
Sollecitazioni: T_y=1.34
V,Ed=1.34 Vc,Rd=13761.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.08 - Classe 1
Sollecitazioni: T_z=75.08
V,Ed=75.08 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 92 SLU Xl=0.58 - Classe 1
Sollecitazioni: N=-94.40 T_z=8.50 M_y=-20.93 T_y=1.34
My,Ed=-20.93 My,V,c,Rd=1595.68
N,Ed=-94.40 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01
(sic.=76.227)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
Sollecitazioni: N,Ed=-110.20 My,Ed=-20.93 Mz,Ed=0.67 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.00=0.02 (sic.=59.797)
Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=78.098)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 208
  $f_{Z,L}$=0.02 (L/2832) (sic.=9.440)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 145
  $f_{Z,L}$=0.02 (L/2779) (sic.=11.116)

Asta n. 3016 (-28 -41) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-86.18 M_y=-3.30 T_y=-2.99 M_z=1.73
  Tensioni: σ_N=-6.52 $\sigma_{m,d}$=-26.20 τ=0.00 σ_{max}=-32.72 (sic.=80.038)
  Tensioni: σ_N=-6.52 $\sigma_{m,d}$=-0.49 τ=0.51 τ_{max}=0.51 (sic. >100)
  Tensioni: σ_N=-6.52 $\sigma_{m,d}$=-26.20 τ=0.00 $\sigma_{ID,max}$=32.72 (sic.=80.038)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-73.55
  V,Ed=-73.55 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 107 SLU Xl=0.02 - Classe 1
  Sollecitazioni: N=32.69 M_y=-20.35
  My,Ed=-20.35 My,c,Rd=1595.68
  N,Ed=32.69 Nc,Rd=34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01 (sic.=78.403)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 102 SLU - Classe 1
  Sollecitazioni: N,Ed=-22.58 My,Ed=-20.05 Mz,Ed=1.97 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=39.88 Ncr,z=172145.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.02 (sic.=63.512)
  Verifica ZZ: 0.00+0.01+0.01=0.01 (sic.=76.058)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/302603) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 141
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/403471) (sic.=51.508)

Asta n. 3017 (205 -29) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-692.01 T_z=442.57 M_y=682.88 T_y=-468.47 M_z=337.22
  Tensioni: σ_N=-8.86 $\sigma_{m,d}$=-288.21 τ=0.00 σ_{max}=-297.07 (sic.=8.816)
  Tensioni: σ_N=-8.86 $\sigma_{m,d}$=-7.57 τ=29.03 τ_{max}=29.03 (sic.=52.092)
  Tensioni: σ_N=-8.86 $\sigma_{m,d}$=-288.21 τ=0.00 $\sigma_{ID,max}$=297.07 (sic.=8.816)

- Verifica a taglio Dir. Y [4.2.16] - CC 114 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=-182.34
  V,Ed=-182.34 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=652.48
  V,Ed=652.48 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=57.552)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 114 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=-1193.11 T_z=652.48 M_y=672.65 T_y=-182.34 M_z=189.67
  N,Ed=-1193.11 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=672.65 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.04 (sic.=25.098)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=189.67 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=42.267)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.04 (sic.=25.098)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-692.01 My,Ed=682.88 Mz,Ed=337.22 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.16 M,cr=5384810.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.04+0.06=0.11 (sic.=9.265)
  Verifica ZZ: 0.00+0.03+0.06=0.10 (sic.=10.077)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
  $f_{Z,G}$=0.00 (L/12476) $f_{Z,L}$=0.00 (L/72184) (sic.=41.587)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/12632) $f_{Z,L}$=0.00 (L/202114) (sic.=50.528)

Asta n. 3017 (-29 -42) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-681.00 T_z=407.98 M_y=475.78 T_y=235.09 M_z=112.89
  Tensioni: σ_N=-8.72 $\sigma_{m,d}$=-139.87 τ=0.00 σ_{max}=-148.59 (sic.=17.625)
  Tensioni: σ_N=-8.72 $\sigma_{m,d}$=-2.54 τ=26.72 τ_{max}=26.72 (sic.=56.586)
  Tensioni: σ_N=-8.72 $\sigma_{m,d}$=-139.87 τ=0.00 $\sigma_{ID,max}$=148.59 (sic.=17.625)

- Verifica a taglio Dir. Y [4.2.16] - CC 114 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-146.21
  V,Ed=-146.21 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=569.21
  V,Ed=569.21 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=65.971)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 66 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-368.69 T_z=412.85 M_y=461.06 T_y=-169.51 M_z=109.97
  N,Ed=-368.69 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=461.06 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=36.615)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=109.97 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic.=72.897)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=36.615)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-681.00 My,Ed=475.78 Mz,Ed=112.89 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.68 M,cr=12391800.00 λ_{LT}=0.04
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.01 χ_{LT}=1.00
  λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=5.70 Ncr,z=49857900.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.03+0.02=0.05 (sic.=18.494)
  Verifica ZZ: 0.00+0.02+0.02=0.05 (sic.=20.828)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 151
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/403471) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 151
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/302603) (sic.=51.508)

Asta n. 3017 (-42 -59) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-652.66 T_z=273.43 M_y=-347.17 T_y=-58.51 M_z=55.63
  Tensioni: σ_N=-8.36 $\sigma_{m,d}$=-88.72 τ=0.00 σ_{max}=-97.08 (sic.=26.979)
  Tensioni: σ_N=-8.36 $\sigma_{m,d}$=-1.25 τ=17.90 τ_{max}=17.90 (sic.=84.471)
  Tensioni: σ_N=-8.36 $\sigma_{m,d}$=-88.72 τ=0.00 $\sigma_{ID,max}$=97.08 (sic.=26.979)

- Verifica a taglio Dir. Y [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=-15.26
  V,Ed=-15.26 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-343.46
  V,Ed=-343.46 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-1453.67 T_z=-299.64 M_y=-428.79 T_y=-15.26 M_z=9.19
  N,Ed=-1453.67 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-428.79 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=39.371)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=9.19 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=39.371)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-652.66 My,Ed=-347.17 Mz,Ed=55.63 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.26 M,cr=5819060.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=5.70 Ncr,z=49857900.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.04 (sic.=28.269)
Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=32.307)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
$f_{Z,G}$=0.00 (L/12741) $f_{Z,L}$=0.00 (L/242083) (sic.=42.470)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 141
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/134490) (sic.=52.060)

Asta n. 3017 (-59 -76) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-625.62 T_z=-363.70 M_y=-194.28 T_y=-38.86 M_z=22.08
Tensioni: σ_N=-8.01 $\sigma_{m,d}$=-45.13 τ=0.00 σ_{max}=-53.14 (sic.=49.284)
Tensioni: σ_N=-8.01 $\sigma_{m,d}$=-0.50 τ=23.81 τ_{max}=23.81 (sic.=63.508)
Tensioni: σ_N=-8.01 $\sigma_{m,d}$=-45.13 τ=0.00 $\sigma_{ID,max}$=53.14 (sic.=49.284)

- Verifica a taglio Dir. Y [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
Sollecitazioni: T_y=-2.53
V,Ed=-2.53 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
Sollecitazioni: T_z=-636.22
V,Ed=-636.22 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=59.023)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-1061.92 T_z=-433.85 M_y=-247.76 T_y=-35.17 M_z=17.75
N,Ed=-1061.92 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-247.76 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic.=68.137)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=17.75 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=68.137)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
Sollecitazioni: N,Ed=-1423.61 My,Ed=-243.32 Mz,Ed=-1.08 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.21 M,cr=10251900.00 λ_{LT}=0.04
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.01+0.01+0.00=0.02 (sic.=48.275)
Verifica ZZ: 0.01+0.01+0.00=0.02 (sic.=65.382)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/605207) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 136
$f_{Z,G}$=0.00 (L/13157) $f_{Z,L}$=0.00 (L/302603) (sic.=52.628)

Asta n. 3018 (206 -30) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
Sollecitazioni: N=-77.81 T_z=2.60 M_y=-3.38 T_y=2.37 M_z=1.19
Tensioni: σ_N=-5.89 $\sigma_{m,d}$=-20.10 τ=0.00 σ_{max}=-25.99 (sic. >100)
Tensioni: σ_N=-5.89 $\sigma_{m,d}$=-0.94 τ=0.59 τ_{max}=0.59 (sic. >100)
Tensioni: σ_N=-5.89 $\sigma_{m,d}$=-20.10 τ=0.00 $\sigma_{ID,max}$=25.99 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.08 - Classe 1
Sollecitazioni: T_z=70.27
V,Ed=70.27 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 92 SLU Xl=0.58 - Classe 1
Sollecitazioni: N=-11.93 T_z=7.70 M_y=-19.53
My,Ed=-19.53 My,V,c,Rd=1595.68
N,Ed=-11.93 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01
(sic.=81.714)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
Sollecitazioni: N,Ed=-82.46 My,Ed=-19.44 Mz,Ed=0.61 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.00=0.01 (sic.=66.964)

Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=89.146)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 208
  $f_{Z,L}$=0.01 (L/3660) (sic.=12.200)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 124
  $f_{Z,L}$=0.01 (L/3525) (sic.=14.100)

Asta n. 3018 (-30 -43) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-76.85 M_y=-3.16 T_y=-2.05 M_z=1.19
  Tensioni: σ_N=-5.82 $\sigma_{m,d}$=-19.68 τ=0.00 σ_{max}=-25.49 (sic. >100)
  Tensioni: σ_N=-5.82 $\sigma_{m,d}$=-2.02 τ=0.35 τ_{max}=0.35 (sic. >100)
  Tensioni: σ_N=-5.82 $\sigma_{m,d}$=-19.68 τ=0.00 $\sigma_{ID,max}$=25.49 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 107 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=-1.06
  V,Ed=-1.06 Vc,Rd=13761.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-68.50
  V,Ed=-68.50 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 107 SLU Xl=0.03 - Classe 1
  Sollecitazioni: N=-65.47 M_y=-18.78 T_y=-1.06
  My,Ed=-18.78 My,c,Rd=1595.68
  N,Ed=-65.47 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01
(sic.=84.961)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-66.33 My,Ed=-18.78 Mz,Ed=0.61 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172145.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=71.042)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=95.550)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/302603) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 189
  $f_{Z,G}$=0.00 (L/12608) $f_{Z,L}$=0.00 (L/172916) (sic.=50.432)

Asta n. 3019 (207 -31) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-26.70 T_z=2.62 M_y=-3.39 T_y=-1.29
  Tensioni: σ_N=-2.02 $\sigma_{m,d}$=-6.40 τ=0.00 σ_{max}=-8.42 (sic. >100)
  Tensioni: σ_N=-2.02 $\sigma_{m,d}$=-0.00 τ=0.60 τ_{max}=0.60 (sic. >100)
  Tensioni: σ_N=-2.02 $\sigma_{m,d}$=-6.40 τ=0.22 $\sigma_{ID,max}$=8.43 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 87 SLU Xl=0.08 - Classe 1
  Sollecitazioni: T_z=70.55
  V,Ed=70.55 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 87 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-26.45 T_z=7.98 M_y=-19.67
  My,Ed=-19.67 My,V,c,Rd=1595.68
  N,Ed=-26.45 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01
(sic.=81.127)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 97 SLU - Classe 1
  Sollecitazioni: N,Ed=-28.33 My,Ed=-19.63 Mz,Ed=0.60 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=74.256)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 213
  $f_{Z,L}$=0.02 (L/2345) $f_{Z,G}$=0.02 (L/2466) (sic.=7.817)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 124
  $f_{Z,L}$=0.02 (L/2259) $f_{Z,G}$=0.02 (L/2371) (sic.=9.036)

Asta n. 3019 (-31 -44) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-25.74 M_y=-3.11 T_y=1.12
  Tensioni: σ_N=-1.95 $\sigma_{m,d}$=-5.88 τ=0.00 σ_{max}=-7.83 (sic. >100)
  Tensioni: σ_N=-1.95 $\sigma_{m,d}$=-5.88 τ=0.19 τ_{max}=0.19 (sic. >100)
  Tensioni: σ_N=-1.95 $\sigma_{m,d}$=-5.88 τ=0.19 $\sigma_{ID,max}$=7.84 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 83 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-55.00
  V,Ed=-55.00 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 112 SLU Xl=0.03 - Classe 1
  Sollecitazioni: N=-2.02 M_y=-18.66
  My,Ed=-18.66 My,c,Rd=1595.68
  N,Ed=-2.02 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01
(sic.=85.507)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 102 SLU - Classe 1
  Sollecitazioni: N,Ed=-13.30 My,Ed=-18.60 Mz,Ed=0.58 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172145.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=80.752)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/403471) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 179
  $f_{Z,G}$=0.00 (L/12741) $f_{Z,L}$=0.00 (L/151302) (sic.=50.964)

Asta n. 3020 (208 -32) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-10.55 T_z=2.65 M_y=-3.41 T_y=1.13
  Tensioni: σ_N=-0.80 $\sigma_{m,d}$=-6.43 τ=0.00 σ_{max}=-7.23 (sic. >100)
  Tensioni: σ_N=-0.80 $\sigma_{m,d}$=-0.00 τ=0.60 τ_{max}=0.60 (sic. >100)
  Tensioni: σ_N=-0.80 $\sigma_{m,d}$=-6.43 τ=0.19 $\sigma_{ID,max}$=7.24 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 87 SLU Xl=0.08 - Classe 1
  Sollecitazioni: T_z=70.54
  V,Ed=70.54 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 87 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-14.64 T_z=7.97 M_y=-19.66
  My,Ed=-19.66 My,V,c,Rd=1595.68
  N,Ed=-14.64 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01
(sic.=81.149)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 97 SLU - Classe 1
  Sollecitazioni: N,Ed=-29.04 My,Ed=-19.60 Mz,Ed=0.50 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=75.097)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 213
  $f_{Z,L}$=0.02 (L/2501) (sic.=8.337)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 124
  $f_{Z,L}$=0.02 (L/2335) (sic.=9.340)

Asta n. 3020 (-32 -45) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-9.59 M_y=-3.14
  Tensioni: σ_N=-0.73 $\sigma_{m,d}$=-5.93 τ=0.00 σ_{max}=-6.66 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=-0.73 $\sigma_{m,d}$=-5.93 τ=0.00 $\sigma_{ID,max}$=6.66 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-68.26
  V,Ed=-68.26 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 112 SLU Xl=0.03 - Classe 1
  Sollecitazioni: N=-10.08 M_y=-18.65
  My,Ed=-18.65 My,c,Rd=1595.68
  N,Ed=-10.08 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01
(sic.=85.543)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 102 SLU - Classe 1
  Sollecitazioni: N,Ed=-11.92 My,Ed=-18.63 Mz,Ed=0.52 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172145.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=81.468)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/605206) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 151
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/403471) (sic.=52.060)

Asta n. 3021 (209 -33) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-92.98 T_z=2.61 M_y=-3.38 T_y=1.43
  Tensioni: σ_N=-7.04 $\sigma_{m,d}$=-6.39 τ=0.00 σ_{max}=-13.43 (sic. >100)
  Tensioni: σ_N=-7.04 $\sigma_{m,d}$=-0.00 τ=0.59 τ_{max}=0.59 (sic. >100)
  Tensioni: σ_N=-7.04 $\sigma_{m,d}$=-6.39 τ=0.24 $\sigma_{ID,max}$=13.44 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 87 SLU Xl=0.08 - Classe 1
  Sollecitazioni: T_z=70.26
  V,Ed=70.26 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 87 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-63.55 T_z=7.69 M_y=-19.52
  My,Ed=-19.52 My,V,c,Rd=1595.68
  N,Ed=-63.55 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01
(sic.=81.732)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
  Sollecitazioni: N,Ed=-87.83 My,Ed=-19.50 Mz,Ed=-0.11 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=69.837)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=99.331)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 170
  $f_{Z,L}$=0.01 (L/5150) (sic.=17.167)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 124
  $f_{Z,L}$=0.01 (L/4088) (sic.=16.352)

Asta n. 3021 (-33 -46) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-92.02 M_y=-3.15 T_y=-1.24
  Tensioni: σ_N=-6.97 $\sigma_{m,d}$=-5.95 τ=0.00 σ_{max}=-12.92 (sic. >100)
  Tensioni: σ_N=-6.97 $\sigma_{m,d}$=-5.95 τ=0.21 τ_{max}=0.21 (sic. >100)
  Tensioni: σ_N=-6.97 $\sigma_{m,d}$=-5.95 τ=0.21 $\sigma_{ID,max}$=12.92 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 112 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-68.57
  V,Ed=-68.57 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 112 SLU Xl=0.03 - Classe 1
  Sollecitazioni: N=-21.78 M_y=-18.82
  My,Ed=-18.82 My,c,Rd=1595.68
  N,Ed=-21.78 Nc,Rd=-34598.90 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01

(sic.=84.787)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
  Sollecitazioni: N,Ed=-71.69 My,Ed=-18.71 Mz,Ed=-0.11 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=39.88 Ncr,z=172145.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=74.717)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/403471) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 161
  $f_{Z,G}$=0.00 (L/12741) $f_{Z,L}$=0.00 (L/302603) (sic.=50.964)

Asta n. 3022 (210 -34) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-917.90 T_z=75.25 M_y=-43.82 T_y=137.90 M_z=66.45
  Tensioni: σ_N=-11.76 $\sigma_{m,d}$=-40.86 τ=0.00 σ_{max}=-52.62 (sic.=49.776)
  Tensioni: σ_N=-11.76 $\sigma_{m,d}$=-1.49 τ=4.95 τ_{max}=4.95 (sic. >100)
  Tensioni: σ_N=-11.76 $\sigma_{m,d}$=-40.86 τ=0.00 $\sigma_{ID,max}$=52.62 (sic.=49.776)

- Verifica a taglio Dir. Y [4.2.16] - CC 114 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=34.06
  V,Ed=34.06 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=374.84
  V,Ed=374.84 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a compressione (4.2.4.1.2.2) - CC 87 SLU Xl=0.10 - Classe 1
  Sollecitazioni: N=-2449.86 T_z=181.15 T_y=-8.38
  Verifica a compressione [4.2.9]
  N,Ed=-2449.86 Nc,Rd=-204503.00 N,Ed/Nc,Rd=0.01 (sic.=83.475)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 94 SLU - Classe 1
  Sollecitazioni: N,Ed=-2283.70 My,Ed=-20.90 Mz,Ed=-90.88 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=8104500.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.00+0.01=0.02 (sic.=53.280)
  Verifica ZZ: 0.01+0.00+0.01=0.02 (sic.=44.278)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
  $f_{Z,L}$=0.01 (L/4767) (sic.=15.890)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 122
  $f_{Z,L}$=0.01 (L/3357) (sic.=13.428)

Asta n. 3022 (-34 -47) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-916.94 T_z=72.23 M_y=-44.42 T_y=118.90 M_z=66.45
  Tensioni: σ_N=-11.74 $\sigma_{m,d}$=-40.97 τ=0.00 σ_{max}=-52.71 (sic.=49.689)
  Tensioni: σ_N=-11.74 $\sigma_{m,d}$=-1.49 τ=4.75 τ_{max}=4.75 (sic. >100)
  Tensioni: σ_N=-11.74 $\sigma_{m,d}$=-40.97 τ=0.00 $\sigma_{ID,max}$=52.71 (sic.=49.689)

- Verifica a taglio Dir. Y [4.2.16] - CC 114 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-14.21
  V,Ed=-14.21 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=293.19
  V,Ed=293.19 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 114 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-1465.58 T_z=200.07 M_y=-304.96 T_y=-14.21 M_z=8.21
  N,Ed=-1465.58 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-304.96 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=55.357)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=8.21 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)

α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.02 (sic.=55.357)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 109 SLU - Classe 1
  Sollecitazioni: N,Ed=-1509.31 My,Ed=-302.01 Mz,Ed=78.53 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.27 M,cr=5903420.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=5.70 Ncr,z=49857900.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.02+0.01=0.03 (sic.=33.423)
  Verifica ZZ: 0.01+0.01+0.01=0.03 (sic.=37.260)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/302603) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/403471) (sic.=52.060)

Asta n. 3022 (-47 -64) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-964.74 T_z=-123.93 M_y=-75.12 T_y=-42.07 M_z=40.14
  Tensioni: σ_N=-12.36 $\sigma_{m,d}$=-33.22 τ=0.00 σ_{max}=-45.58 (sic.=57.461)
  Tensioni: σ_N=-12.36 $\sigma_{m,d}$=-0.90 τ=8.11 τ_{max}=8.11 (sic. >100)
  Tensioni: σ_N=-12.36 $\sigma_{m,d}$=-33.22 τ=0.00 $\sigma_{ID,max}$=45.58 (sic.=57.461)

- Verifica a taglio Dir. Y [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=-35.14
  V,Ed=-35.14 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-397.71
  V,Ed=-397.71 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=94.420)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 114 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-1422.64 T_z=-60.12 M_y=-304.76 T_y=21.16 M_z=8.21
  N,Ed=-1422.64 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-304.76 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=55.394)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=8.21 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.02 (sic.=55.394)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-1888.68 My,Ed=-271.53 Mz,Ed=29.28 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.20 M,cr=5557390.00 λ_{LT}=0.06
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=5.70 Ncr,z=49857900.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.02+0.00=0.03 (sic.=37.642)
  Verifica ZZ: 0.01+0.01+0.00=0.02 (sic.=45.777)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/151302) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/403471) (sic.=52.060)

Asta n. 3022 (-64 -81) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-923.71 T_z=-262.65 M_y=198.65 T_y=-38.00 M_z=-2.57
  Tensioni: σ_N=-11.83 $\sigma_{m,d}$=-36.16 τ=0.00 σ_{max}=-47.99 (sic.=54.576)
  Tensioni: σ_N=-11.83 $\sigma_{m,d}$=0.06 τ=17.19 τ_{max}=17.19 (sic.=87.941)
  Tensioni: σ_N=-11.83 $\sigma_{m,d}$=-36.16 τ=0.00 $\sigma_{ID,max}$=47.99 (sic.=54.576)

- Verifica a taglio Dir. Y [4.2.16] - CC 87 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=12.26
  V,Ed=12.26 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 87 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-650.86
  V,Ed=-650.86 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=57.695)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 89 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-2276.41 T_z=-644.89 M_y=568.05 T_y=25.04
  My,Ed=568.05 My,V,c,Rd=16881.90
  N,Ed=-2276.41 Nc,Rd=-204503.00 YY n=N,Ed/Nc,Rd=0.01 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=29.719)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
  Sollecitazioni: N,Ed=-2296.40 My,Ed=568.05 Mz,Ed=-15.39 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.38 M,cr=6411600.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.94
  Verifica YY: 0.01+0.03+0.00=0.04 (sic.=22.611)
  Verifica ZZ: 0.01+0.02+0.00=0.03 (sic.=31.067)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 194
  $f_{z,G}$=0.00 (L/12877) $f_{z,L}$=0.00 (L/201736) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 194
  $f_{z,G}$=0.00 (L/12608) $f_{z,L}$=0.00 (L/110038) (sic.=50.432)

Asta n. 3023 (211 -35) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-107.29 T_z=4.07 M_y=-4.12 T_y=3.10 M_z=1.55
  Tensioni: σ_N=-8.12 $\sigma_{m,d}$=-25.71 τ=0.00 σ_{max}=-33.83 (sic.=77.412)
  Tensioni: σ_N=-8.12 $\sigma_{m,d}$=-1.23 τ=0.93 τ_{max}=0.93 (sic. >100)
  Tensioni: σ_N=-8.12 $\sigma_{m,d}$=-25.71 τ=0.00 $\sigma_{ID,max}$=33.83 (sic.=77.412)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.08 - Classe 1
  Sollecitazioni: T_y=-3.97
  V,Ed=-3.97 Vc,Rd=13761.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.08 - Classe 1
  Sollecitazioni: T_z=72.32
  V,Ed=72.32 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-82.79 T_z=9.75 M_y=-20.56 T_y=-3.97 M_z=-1.99
  N,Ed=-82.79 Nc,Rd=34598.90 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-20.56 My,V,c,Rd=1595.68 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01 (sic.=77.621)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-1.99 Mz,V,c,Rd=356.17 MNz,c,Rd=356.17 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=77.621)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
  Sollecitazioni: N,Ed=-97.68 My,Ed=-20.56 Mz,Ed=-1.99 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.02 (sic.=54.808)
  Verifica ZZ: 0.00+0.01+0.01=0.02 (sic.=63.363)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 170
  $f_{z,L}$=0.02 (L/3263) (sic.=10.877)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 145
  $f_{z,L}$=0.02 (L/2613) (sic.=10.452)

Asta n. 3023 (-35 -48) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-107.59 T_z=-2.71 M_y=-3.77 T_y=-2.69 M_z=1.55
  Tensioni: σ_N=-8.14 $\sigma_{m,d}$=-25.05 τ=0.00 σ_{max}=-33.19 (sic.=78.902)
  Tensioni: σ_N=-8.14 $\sigma_{m,d}$=-1.23 τ=0.62 τ_{max}=0.62 (sic. >100)
  Tensioni: σ_N=-8.14 $\sigma_{m,d}$=-25.05 τ=0.00 $\sigma_{ID,max}$=33.19 (sic.=78.902)

- Verifica a taglio Dir. Y [4.2.16] - CC 107 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=-3.09
  V,Ed=-3.09 Vc,Rd=13761.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-53.96

V,Ed=-53.96 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=18.67 T_z=-14.20 M_y=-19.67 T_y=-3.09 M_z=1.79
  N,Ed=18.67 Nc,Rd=34598.90 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-19.67 My,V,c,Rd=1595.68 MNy,c,Rd=1595.68 My,Ed/MNy,c,Rd=0.01 (sic.=81.126)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=1.79 Mz,V,c,Rd=356.17 MNz,c,Rd=356.17 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=81.126)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
  Sollecitazioni: N,Ed=-81.75 My,Ed=-19.11 Mz,Ed=-1.99 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=39.88 Ncr,z=172145.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.02 (sic.=59.095)
  Verifica ZZ: 0.00+0.01+0.01=0.01 (sic.=67.782)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/12741) $f_{Z,L}$=0.00 (L/605206) (sic.=42.470)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 151
  $f_{Z,G}$=0.00 (L/12478) $f_{Z,L}$=0.00 (L/242083) (sic.=49.912)

Asta n. 3024 (-25 -36) - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.58 - Classe 3
  Sollecitazioni: T_z=-3.17
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.23 τ_{max}=1.23 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.23 $\sigma_{ID,max}$=2.13 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 82 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-33.96
  V,Ed=-33.96 Vc,Rd=4355.00 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 77 SLU Xl=0.29 - Classe 1
  Sollecitazioni: N=-9.44 M_y=-4.90
  My,Ed=-4.90 My,c,Rd=204.50
  N,Ed=-9.44 Nc,Rd=-15085.70 YY n=N,Ed/Nc,Rd=0.00 MNy,c,Rd=204.50 My,Ed/MNy,c,Rd=0.02 (sic.=41.737)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 1
  Sollecitazioni: N,Ed=-18.27 My,Ed=-4.90 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=39.03 Ncr,y=78364.00 λ^*_y=0.45 Curva a: Φ_y=0.63 χ_y=0.94
  λ_z=39.03 Ncr,z=78364.00 λ^*_z=0.45 Curva a: Φ_z=0.63 χ_z=0.94
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
  Verifica YY: 0.00+0.02=0.02 (sic.=41.565)
  Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 211
  $f_{Z,G}$=0.00 (L/11752) $f_{Z,L}$=0.00 (L/15926) (sic.=39.173)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 181
  $f_{Z,G}$=0.01 (L/10712) $f_{Z,L}$=0.00 (L/13913) (sic.=42.848)

Asta n. 3025 (-26 -37) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-102.05 T_z=2.09 M_y=-4.92 T_y=12.42 M_z=7.17
  Tensioni: σ_N=-4.03 $\sigma_{m,d}$=-23.25 τ=0.00 σ_{max}=-27.28 (sic.=96.012)
  Tensioni: σ_N=-4.03 $\sigma_{m,d}$=-8.48 τ=0.91 τ_{max}=0.91 (sic. >100)
  Tensioni: σ_N=-4.03 $\sigma_{m,d}$=-23.25 τ=0.00 $\sigma_{ID,max}$=27.28 (sic.=96.012)

- Verifica a taglio Dir. Y [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=23.98
  V,Ed=23.98 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=49.04
  V,Ed=49.04 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 100 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-56.27 T_z=2.33 M_y=-10.81 T_y=47.32 M_z=27.31

N,Ed=-56.27 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-10.81 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.00 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=27.31 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.02 (sic.=56.513)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^{2}+(Mz,Ed/MNz,c,Rd)^{1}$=0.02 (sic.=56.475)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 100 SLU - Classe 1
Sollecitazioni: N,Ed=-63.82 My,Ed=-10.81 Mz,Ed=27.31 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=140048.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=11.80 Ncr,y=3771410.00 λ^*_y=0.14 Curva b: Φ_y=0.50 χ_y=1.00
λ_z=19.12 Ncr,z=1436580.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.00+0.01=0.01 (sic.=69.862)
Verifica ZZ: 0.00+0.00+0.02=0.02 (sic.=50.659)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/605207) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 166
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/403471) (sic.=52.060)

Asta n. 3025 (-37 -49) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-100.48 T_z=-3.17 M_y=-4.99 T_y=-12.42 M_z=7.17
Tensioni: σ_N=-3.97 $\sigma_{m,d}$=-23.32 τ=0.00 σ_{max}=-27.28 (sic.=95.999)
Tensioni: σ_N=-3.97 $\sigma_{m,d}$=-8.53 τ=0.92 τ_{max}=0.92 (sic. >100)
Tensioni: σ_N=-3.97 $\sigma_{m,d}$=-23.32 τ=0.00 $\sigma_{ID,max}$=27.28 (sic.=95.999)

- Verifica a taglio Dir. Y [4.2.16] - CC 102 SLU Xl=0.58 - Classe 1
Sollecitazioni: T_y=10.08
V,Ed=10.08 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 102 SLU Xl=0.58 - Classe 1
Sollecitazioni: T_z=-32.88
V,Ed=-32.88 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 100 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-55.62 T_z=-11.65 M_y=-10.83 T_y=-47.32 M_z=27.31
N,Ed=-55.62 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-10.83 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.00 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=27.31 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.02 (sic.=56.513)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^{2}+(Mz,Ed/MNz,c,Rd)^{1}$=0.02 (sic.=56.475)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 100 SLU - Classe 1
Sollecitazioni: N,Ed=-55.62 My,Ed=-10.83 Mz,Ed=27.31 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=140048.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=11.80 Ncr,y=3771410.00 λ^*_y=0.14 Curva b: Φ_y=0.50 χ_y=1.00
λ_z=19.12 Ncr,z=1436580.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.00+0.01=0.01 (sic.=70.442)
Verifica ZZ: 0.00+0.00+0.02=0.02 (sic.=50.972)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 199
$f_{Z,G}$=0.00 (L/12741) $f_{Z,L}$=0.00 (L/302603) (sic.=42.470)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 209
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/605206) (sic.=51.508)

Asta n. 3025 (-49 -67) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
Sollecitazioni: N=-28.95 T_z=12.78 M_y=-10.53 T_y=10.56 M_z=6.09
Tensioni: σ_N=-1.14 $\sigma_{m,d}$=-25.74 τ=0.00 σ_{max}=-26.88 (sic.=97.429)
Tensioni: σ_N=-1.14 $\sigma_{m,d}$=-0.66 τ=2.67 τ_{max}=2.67 (sic. >100)
Tensioni: σ_N=-1.14 $\sigma_{m,d}$=-25.74 τ=0.00 $\sigma_{ID,max}$=26.88 (sic.=97.429)

- Verifica a taglio Dir. Y [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=7.00
V,Ed=7.00 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 107 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=53.32
  V,Ed=53.32 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 107 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-52.82 T_z=39.10 M_y=-26.67 T_y=7.00 M_z=4.04
  N,Ed=-52.82 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-26.67 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.01 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=4.04 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-57.34 My,Ed=-26.67 Mz,Ed=4.04 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=140048.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=11.80 Ncr,y=3771420.00 λ^*_y=0.14 Curva b: Φ_y=0.50 χ_y=1.00
  λ_z=19.12 Ncr,z=1436580.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=95.991)
  Verifica ZZ: 0.00+0.00+0.00=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
  $f_{z,G}$=0.00 (L/13015) $f_{z,L}$=0.00 (L/605206) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 141
  $f_{z,G}$=0.00 (L/12877) $f_{z,L}$=0.00 (L/403471) (sic.=51.508)

Asta n. 3025 (-67 -84) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-31.41 T_z=-11.93 M_y=-10.60 T_y=-10.56 M_z=6.09
  Tensioni: σ_N=-1.24 $\sigma_{m,d}$=-25.80 τ=0.00 σ_{max}=-27.04 (sic.=96.856)
  Tensioni: σ_N=-1.24 $\sigma_{m,d}$=-0.66 τ=2.50 τ_{max}=2.50 (sic. >100)
  Tensioni: σ_N=-1.24 $\sigma_{m,d}$=-25.80 τ=0.00 $\sigma_{ID,max}$=27.04 (sic.=96.856)

- Verifica a taglio Dir. Y [4.2.16] - CC 92 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=6.15
  V,Ed=6.15 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 92 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-69.42
  V,Ed=-69.42 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 92 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-17.75 T_z=-22.86 M_y=-26.63 T_y=6.15 M_z=-3.55
  N,Ed=-17.75 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-26.63 My,V,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.01 (sic. >100)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-3.55 Mz,V,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-44.41 My,Ed=-26.62 Mz,Ed=4.04 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=140048.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=11.80 Ncr,y=3771410.00 λ^*_y=0.14 Curva b: Φ_y=0.50 χ_y=1.00
  λ_z=19.12 Ncr,z=1436580.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=97.958)
  Verifica ZZ: 0.00+0.00+0.00=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 136
  $f_{z,G}$=0.00 (L/13157) $f_{z,L}$=0.00 (L/1210410) (sic.=43.857)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 136
  $f_{z,G}$=0.00 (L/13157) $f_{z,L}$=0.00 (L/242083) (sic.=52.628)

Asta n. 3026 (215 -50) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.10 - Classe 3
  Sollecitazioni: N=-992.40 T_z=-514.71 M_y=-1244.27 T_y=-455.77 M_z=428.20
  Tensioni: σ_N=-12.71 $\sigma_{m,d}$=-432.18 τ=0.00 σ_{max}=-444.88 (sic.=5.887)

Tensioni: σ_N=-12.71 $\sigma_{m,d}$=-9.62 τ=33.74 τ_{max}=33.74 (sic.=44.817)
Tensioni: σ_N=-12.71 $\sigma_{m,d}$=-432.18 τ=0.00 $\sigma_{ID,max}$=444.88 (sic.=5.887)

- Verifica a taglio Dir. Y [4.2.16] - CC 41 SLU Xl=1.15 - Classe 1
Sollecitazioni: T_y=-196.46
V,Ed=-196.46 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 41 SLU Xl=1.15 - Classe 1
Sollecitazioni: T_z=-507.81
V,Ed=-507.81 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=73.948)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.10 - Classe 1
Sollecitazioni: N=-1697.19 T_z=-415.04 M_y=-963.91 T_y=-265.07 M_z=284.40
N,Ed=-1697.19 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-963.91 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.06 (sic.=17.514)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=284.40 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.04 (sic.=28.189)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=17.514)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-992.40 My,Ed=-1244.27 Mz,Ed=428.20 L=1.15
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.27 M,cr=1496820.00 λ_{LT}=0.10
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=6.76 Ncr,y=35440800.00 λ^*_y=0.08 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=11.39 Ncr,z=12464500.00 λ^*_z=0.13 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.08+0.08=0.16 (sic.=6.186)
Verifica ZZ: 0.00+0.06+0.08=0.15 (sic.=6.858)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 146
$f_{Z,G}$=0.01 (L/12271) $f_{Z,L}$=0.00 (L/25529) (sic.=40.903)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 194
$f_{Z,G}$=0.01 (L/10887) $f_{Z,L}$=0.01 (L/19655) (sic.=43.548)

Asta n. 3026 (-50 -85) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-979.50 T_z=-634.95 M_y=-666.13 T_y=-64.87 M_z=76.95
Tensioni: σ_N=-12.54 $\sigma_{m,d}$=-155.35 τ=0.00 σ_{max}=-167.90 (sic.=15.599)
Tensioni: σ_N=-12.54 $\sigma_{m,d}$=-1.73 τ=41.57 τ_{max}=41.57 (sic.=36.378)
Tensioni: σ_N=-12.54 $\sigma_{m,d}$=-155.35 τ=0.00 $\sigma_{ID,max}$=167.90 (sic.=15.599)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=1.15 - Classe 1
Sollecitazioni: T_z=-685.97
V,Ed=-685.97 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.02 (sic.=54.742)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-1302.88 T_z=-489.82 M_y=-535.16 T_y=107.48 M_z=-121.46
N,Ed=-1302.88 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-535.16 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=31.546)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-121.46 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.02 (sic.=66.004)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=31.546)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-979.50 My,Ed=-666.13 Mz,Ed=76.95 L=1.15
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.93 M,cr=2264270.00 λ_{LT}=0.08
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=6.76 Ncr,y=35440800.00 λ^*_y=0.08 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=11.39 Ncr,z=12464500.00 λ^*_z=0.13 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.01=0.06 (sic.=16.352)
Verifica ZZ: 0.00+0.03+0.01=0.05 (sic.=18.986)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 136
$f_{Z,G}$=0.01 (L/13015) $f_{Z,L}$=0.00 (L/142402) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 136
$f_{Z,G}$=0.01 (L/12809) $f_{Z,L}$=0.00 (L/86458) (sic.=51.236)

Asta n. 3039 (-70 -71) - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.75 - Classe 3

Sollecitazioni: N=41.60 M_y=-37.44 M_z=-11.91
Tensioni: σ_N=1.64 $\sigma_{m,d}$=66.17 τ=0.00 σ_{max}=67.81 (sic.=38.623)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=1.64 $\sigma_{m,d}$=66.17 τ=0.00 $\sigma_{ID,max}$=67.81 (sic.=38.623)

- Verifica a taglio Dir. Y [4.2.16] - CC 77 SLU Xl=3.50 - Classe 1
Sollecitazioni: T_y=50.71
V,Ed=50.71 Vc,Rd=32718.30 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 77 SLU Xl=3.50 - Classe 1
Sollecitazioni: T_z=-204.82
V,Ed=-204.82 Vc,Rd=12788.10 V,Ed/Vc,Rd=0.02 (sic.=62.437)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 77 SLU Xl=1.75 - Classe 1
Sollecitazioni: N=31.95 M_y=-179.21 M_z=-44.37
N,Ed=31.95 Nc,Rd=66358.60 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-179.21 My,c,Rd=3142.99 MNy,c,Rd=3142.99 My,Ed/MNy,c,Rd=0.06 (sic.=17.538)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-44.37 Mz,c,Rd=1543.47 MNz,c,Rd=1543.47 Mz,Ed/MNz,c,Rd=0.03 (sic.=34.788)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.06 (sic.=17.538)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
Sollecitazioni: N,Ed=-40.37 My,Ed=-179.21 Mz,Ed=-44.37 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=8044.65 λ_{LT}=0.64
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.69 β_{LT}=0.75 f=0.97 χ_{LT}=0.92
λ_y=71.56 Ncr,y=102559.00 λ^*_y=0.82 Curva b: Φ_y=0.95 χ_y=0.71
λ_z=115.94 Ncr,z=39066.10 λ^*_z=1.34 Curva c: Φ_z=1.67 χ_z=0.37
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.06+0.02=0.08 (sic.=13.178)
Verifica ZZ: 0.00+0.04+0.03=0.06 (sic.=15.586)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 181
$f_{Z,G}$=0.10 (L/3600) $f_{Z,L}$=0.09 (L/4062) (sic.=12.000)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
$f_{Z,G}$=0.14 (L/2457) $f_{Z,L}$=0.12 (L/2829) (sic.=9.828)

Asta n. 3044 (-72 -68) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=-796.02 T_z=399.21 M_y=88.94 T_y=-42.97 M_z=-1.30
Tensioni: σ_N=-10.19 $\sigma_{m,d}$=-16.26 τ=0.00 σ_{max}=-26.46 (sic.=98.996)
Tensioni: σ_N=-10.19 $\sigma_{m,d}$=0.03 τ=26.13 τ_{max}=26.13 (sic.=57.859)
Tensioni: σ_N=-10.19 $\sigma_{m,d}$=-10.49 τ=24.57 $\sigma_{ID,max}$=47.31 (sic.=55.359)

- Verifica a taglio Dir. Y [4.2.16] - CC 109 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-39.01
V,Ed=-39.01 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 109 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=529.70
V,Ed=529.70 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=70.891)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 76 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-1554.22 T_z=414.33 M_y=192.98 T_y=-46.85 M_z=2.28
N,Ed=-1554.22 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=192.98 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic.=87.482)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=2.28 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=87.482)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 90 SLU - Classe 1
Sollecitazioni: N,Ed=-1494.21 My,Ed=184.83 Mz,Ed=-48.03 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.65 M,cr=7632850.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.01+0.01+0.00=0.02 (sic.=47.396)
Verifica ZZ: 0.01+0.01+0.01=0.02 (sic.=52.050)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 179
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/302603) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/201735) (sic.=52.060)

Asta n. 3044 (-68 -51) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-830.02 T_z=292.35 M_y=-311.67 T_y=47.17 M_z=-28.20
  Tensioni: σ_N=-10.63 $\sigma_{m,d}$=-68.79 τ=0.00 σ_{max}=-79.42 (sic.=32.976)
  Tensioni: σ_N=-10.63 $\sigma_{m,d}$=0.63 τ=19.14 τ_{max}=19.14 (sic.=79.005)
  Tensioni: σ_N=-10.63 $\sigma_{m,d}$=-68.79 τ=0.00 $\sigma_{ID,max}$=79.42 (sic.=32.976)

- Verifica a taglio Dir. Y [4.2.16] - CC 61 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-85.59
  V,Ed=-85.59 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 61 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=376.25
  V,Ed=376.25 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=99.803)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 114 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-1432.49 T_z=251.53 M_y=-307.80 T_y=30.59 M_z=34.52
  N,Ed=-1432.49 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-307.80 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=54.848)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=34.52 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=54.848)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 109 SLU - Classe 1
  Sollecitazioni: N,Ed=-1559.78 My,Ed=-303.70 Mz,Ed=-68.88 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.38 M,cr=6398550.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.02+0.00=0.03 (sic.=33.811)
  Verifica ZZ: 0.01+0.01+0.01=0.03 (sic.=38.459)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 136
  $f_{Z,G}$=0.00 (L/13157) $f_{Z,L}$=0.00 (L/605207) (sic.=43.857)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 194
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/403471) (sic.=51.508)

Asta n. 3044 (-51 225) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=1.06 - Classe 3
  Sollecitazioni: N=-860.35 T_z=197.03 M_y=-553.33 T_y=-131.86 M_z=-156.50
  Tensioni: σ_N=-11.02 $\sigma_{m,d}$=-175.25 τ=0.00 σ_{max}=-186.27 (sic.=14.060)
  Tensioni: σ_N=-11.02 $\sigma_{m,d}$=3.52 τ=12.91 τ_{max}=12.91 (sic. >100)
  Tensioni: σ_N=-11.02 $\sigma_{m,d}$=-175.25 τ=0.00 $\sigma_{ID,max}$=186.27 (sic.=14.060)

- Verifica a taglio Dir. Y [4.2.16] - CC 61 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_y=-49.30
  V,Ed=-49.30 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 61 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=305.88
  V,Ed=305.88 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=1.06 - Classe 1
  Sollecitazioni: N=-1043.64 T_z=224.10 M_y=-571.26 T_y=-49.30 M_z=-119.19
  N,Ed=-1043.64 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-571.26 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=29.552)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-119.19 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic.=67.259)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.03 (sic.=29.552)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-860.35 My,Ed=-553.33 Mz,Ed=-156.50 L=1.15
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.25 M,cr=1473160.00 λ_{LT}=0.10
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=6.76 Ncr,y=35440800.00 λ^*_y=0.08 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=11.39 Ncr,z=12464500.00 λ^*_z=0.13 Curva c: Φ_z=0.00 χ_z=1.00

Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.03=0.07 (sic.=14.751)
Verifica ZZ: 0.00+0.03+0.03=0.06 (sic.=16.462)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 161
$f_{Z,G}$=0.01 (L/12005) $f_{Z,L}$=0.00 (L/45326) (sic.=40.017)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 161
$f_{Z,G}$=0.01 (L/11689) $f_{Z,L}$=0.00 (L/32188) (sic.=46.756)

Asta n. 3047 (-58 -75) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: T_z=4.91
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.12 τ_{max}=1.12 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.12 $\sigma_{ID,max}$=1.93 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 77 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=38.36
V,Ed=38.36 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a flessione YY [4.2.12] - CC 77 SLU Xl=0.29 - Classe 1
Sollecitazioni: M_y=-5.53
My,Ed=-5.53 My,c,Rd=1595.68 My,Ed/My,c,Rd=0.00 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 1
Sollecitazioni: N,Ed=-9.55 My,Ed=-5.53 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.00=0.00 (sic. >100)
Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 136
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/1210410) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 136
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/1210410) (sic.=52.060)

Asta n. 3048 (-76 -69) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
Sollecitazioni: N=-637.62 T_z=334.15 M_y=-179.91 T_y=-35.45 M_z=-22.37 M_x=1.05
Tensioni: σ_N=-8.17 $\sigma_{m,d}$=-42.75 τ=2.97 σ_{max}=-50.92 (sic.=51.438)
Tensioni: σ_N=-8.17 $\sigma_{m,d}$=0.50 τ=22.09 τ_{max}=22.09 (sic.=68.441)
Tensioni: σ_N=-8.17 $\sigma_{m,d}$=-42.75 τ=2.97 $\sigma_{ID,max}$=51.18 (sic.=51.177)

- Verifica a taglio Dir. Y [4.2.16] - CC 109 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-40.89
V,Ed=-40.89 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 109 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=420.01
V,Ed=420.01 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=89.406)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 109 SLU Xl=0.58 - Classe 1
Sollecitazioni: N=-1410.21 T_z=376.19 M_y=-151.00 T_y=-40.89 M_z=-24.35
N,Ed=-1410.21 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-151.00 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-24.35 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-637.62 My,Ed=-179.91 Mz,Ed=-22.37 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.92 M,cr=8874110.00 λ_{LT}=0.04
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.01+0.00=0.02 (sic.=53.688)
Verifica ZZ: 0.00+0.01+0.00=0.02 (sic.=61.219)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/605206) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/403471) (sic.=52.060)

Asta n. 3048 (-69 -52) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=-660.01 T_z=263.76 M_y=-341.78 T_y=-113.26 M_z=-85.64 M_x=1.05
  Tensioni: σ_N=-8.45 $\sigma_{m,d}$=-102.75 τ=2.97 σ_{max}=-111.20 (sic.=23.552)
  Tensioni: σ_N=-8.45 $\sigma_{m,d}$=1.92 τ=17.60 τ_{max}=17.60 (sic.=85.924)
  Tensioni: σ_N=-8.45 $\sigma_{m,d}$=-102.75 τ=2.97 $\sigma_{ID,max}$=111.32 (sic.=23.527)

- Verifica a taglio Dir. Y [4.2.16] - CC 94 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=-91.79
  V,Ed=-91.79 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-281.83
  V,Ed=-281.83 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=-546.21 T_z=227.90 M_y=-285.69 T_y=17.19 M_z=-12.01
  N,Ed=-546.21 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-285.69 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=59.093)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-12.01 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=59.093)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-660.01 My,Ed=-341.78 Mz,Ed=-85.64 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.28 M,cr=5929870.00 λ_{LT}=0.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.02+0.02=0.04 (sic.=24.690)
  Verifica ZZ: 0.00+0.02+0.02=0.04 (sic.=27.664)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/605207) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 194
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/403471) (sic.=52.060)

Asta n. 3048 (-52 229) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.06 - Classe 3
  Sollecitazioni: N=-709.72 T_z=-404.52 M_y=682.40 T_y=431.78 M_z=386.46 M_x=1.06
  Tensioni: σ_N=-9.09 $\sigma_{m,d}$=-312.70 τ=3.00 σ_{max}=-321.79 (sic.=8.139)
  Tensioni: σ_N=-9.09 $\sigma_{m,d}$=8.68 τ=26.89 τ_{max}=26.89 (sic.=56.242)
  Tensioni: σ_N=-9.09 $\sigma_{m,d}$=-312.70 τ=3.00 $\sigma_{ID,max}$=321.83 (sic.=8.138)

- Verifica a taglio Dir. Y [4.2.16] - CC 94 SLU Xl=1.06 - Classe 1
  Sollecitazioni: T_y=389.97
  V,Ed=389.97 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 94 SLU Xl=1.06 - Classe 1
  Sollecitazioni: T_z=-495.13
  V,Ed=-495.13 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=75.842)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=1.06 - Classe 1
  Sollecitazioni: N=-1348.18 T_z=-495.13 M_y=703.92 T_y=389.97 M_z=363.56
  N,Ed=-1348.18 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=703.92 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.04 (sic.=23.983)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=363.56 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.05 (sic.=22.051)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.05 (sic.=21.237)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-709.72 My,Ed=682.40 Mz,Ed=386.46 L=1.15
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.30 M,cr=2701140.00 λ_{LT}=0.08

$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=6.76 Ncr,y=35440800.00 λ^*_y=0.08 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=11.39 Ncr,z=12464500.00 λ^*_z=0.13 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.07=0.12 (sic.=8.553)
Verifica ZZ: 0.00+0.03+0.07=0.11 (sic.=9.240)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 194
$f_{Z,G}$=0.01 (L/10995) $f_{Z,L}$=0.00 (L/28474) (sic.=36.650)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 194
$f_{Z,G}$=0.01 (L/10834) $f_{Z,L}$=0.00 (L/30847) (sic.=43.336)

Asta n. 3049 (-60 -77) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: T_z=4.78
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 τ_{max}=1.09 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 $\sigma_{ID,max}$=1.88 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 72 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=28.35
V,Ed=28.35 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 72 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=28.35
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.44 τ_{max}=6.44 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.44 $\sigma_{ID,max}$=11.16 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
Sollecitazioni: N,Ed=-4.73 My,Ed=-5.20 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.00=0.00 (sic. >100)
Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/1210410) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 209
$f_{Z,G}$=0.00 (L/12741) $f_{Z,L}$=0.00 (L/403471) (sic.=50.964)

Asta n. 3050 (-61 -78) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
Sollecitazioni: T_z=4.78
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 τ_{max}=1.09 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 $\sigma_{ID,max}$=1.88 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 72 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=28.35
V,Ed=28.35 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 72 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=28.35
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.44 τ_{max}=6.44 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.44 $\sigma_{ID,max}$=11.16 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
Sollecitazioni: N,Ed=-2.80 My,Ed=-5.20 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.00=0.00 (sic. >100)
Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131

$f_{Z,G}$=0.00 (L/13157) $f_{Z,L}$=0.00 (L/605207) (sic.=43.857)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 179
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/605207) (sic.=51.508)

Asta n. 3051 (-62 -79) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
  Sollecitazioni: T_z=4.78
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 τ_{max}=1.09 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 $\sigma_{ID,max}$=1.88 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 78 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=28.89
  V,Ed=28.89 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 78 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=28.89
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.57 τ_{max}=6.57 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.57 $\sigma_{ID,max}$=11.38 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-2.38 My,Ed=-5.20 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
  Verifica YY: 0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 146
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/1210410) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 146
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/605207) (sic.=52.060)

Asta n. 3052 (-63 -80) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.00 - Classe 3
  Sollecitazioni: T_z=4.78
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 τ_{max}=1.09 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 $\sigma_{ID,max}$=1.88 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 75 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=28.35
  V,Ed=28.35 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 75 SLU Xl=0.00 - Classe 1
  Sollecitazioni: T_z=28.35
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.44 τ_{max}=6.44 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.44 $\sigma_{ID,max}$=11.16 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
  Sollecitazioni: N,Ed=-5.36 My,Ed=-5.20 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
  Verifica YY: 0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
  $f_{Z,G}$=0.00 (L/13157) $f_{Z,L}$=0.00 (L/1210410) (sic.=43.857)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 194
  $f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/403471) (sic.=51.508)

Asta n. 3053 (-81 -70) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-934.31 T_z=220.56 M_y=198.82 T_y=-30.67 M_z=-2.21 M_x=1.38

Tensioni: σ_N=-11.97 $\sigma_{m,d}$=-36.01 τ=3.89 σ_{max}=-47.97 (sic.=54.594)
Tensioni: σ_N=-11.97 $\sigma_{m,d}$=0.05 τ=14.98 τ_{max}=14.98 (sic. >100)
Tensioni: σ_N=-11.97 $\sigma_{m,d}$=-36.01 τ=3.89 $\sigma_{ID,max}$=48.44 (sic.=54.064)

- Verifica a taglio Dir. Y [4.2.16] - CC 89 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=27.04
V,Ed=27.04 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=534.05
V,Ed=534.05 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic.=70.314)

- Verifica a presso o tenso-flessione retta YY (4.2.4.1.2.7) - CC 89 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-2322.12 T_z=534.05 M_y=568.33 T_y=27.04
My,Ed=568.33 My,V,c,Rd=16881.90
N,Ed=-2322.12 Nc,Rd=-204503.00 YY n=N,Ed/Nc,Rd=0.01 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=29.704)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
Sollecitazioni: N,Ed=-2336.06 My,Ed=568.33 Mz,Ed=15.02 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.32 M,cr=6090900.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.94
Verifica YY: 0.01+0.03+0.00=0.04 (sic.=22.518)
Verifica ZZ: 0.01+0.02+0.00=0.03 (sic.=30.914)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/403471) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 161
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/201735) (sic.=51.508)

Asta n. 3053 (-70 -53) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.58 - Classe 3
Sollecitazioni: N=-969.38 T_z=110.34 M_y=-44.84 T_y=-64.65 M_z=-54.68 M_x=1.38
Tensioni: σ_N=-12.41 $\sigma_{m,d}$=-35.17 τ=3.89 σ_{max}=-47.58 (sic.=55.044)
Tensioni: σ_N=-12.41 $\sigma_{m,d}$=1.23 τ=8.32 τ_{max}=8.32 (sic. >100)
Tensioni: σ_N=-12.41 $\sigma_{m,d}$=-35.17 τ=3.89 $\sigma_{ID,max}$=48.06 (sic.=54.501)

- Verifica a taglio Dir. Y [4.2.16] - CC 89 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=24.13
V,Ed=24.13 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 89 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=323.90
V,Ed=323.90 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 21 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-1099.01 T_z=281.66 M_y=302.97 T_y=24.91 M_z=2.12
N,Ed=-1099.01 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=302.97 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=55.722)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=2.12 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=55.722)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
Sollecitazioni: N,Ed=-2378.83 My,Ed=272.89 Mz,Ed=28.95 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.41 M,cr=6529030.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.94
Verifica YY: 0.01+0.02+0.00=0.03 (sic.=34.474)
Verifica ZZ: 0.01+0.01+0.00=0.02 (sic.=41.253)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/1210410) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 136
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/403471) (sic.=52.060)

Asta n. 3053 (-53 236) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
  Sollecitazioni: N=-992.01 T_z=39.19 M_y=-44.68 T_y=50.28 M_z=-54.68 M_x=1.38
  Tensioni: σ_N=-12.70 $\sigma_{m,d}$=-35.14 τ=3.89 σ_{max}=-47.84 (sic.=54.742)
  Tensioni: σ_N=-12.70 $\sigma_{m,d}$=4.03 τ=5.08 τ_{max}=5.08 (sic. >100)
  Tensioni: σ_N=-12.70 $\sigma_{m,d}$=-35.14 τ=3.89 $\sigma_{ID,max}$=48.32 (sic.=54.208)

- Verifica a taglio Dir. Y [4.2.16] - CC 114 SLU Xl=1.09 - Classe 1
  Sollecitazioni: T_y=48.12
  V,Ed=48.12 Vc,Rd=99836.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 114 SLU Xl=1.09 - Classe 1
  Sollecitazioni: T_z=-240.29
  V,Ed=-240.29 Vc,Rd=37551.30 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 114 SLU Xl=0.00 - Classe 1
  Sollecitazioni: N=-1495.97 T_z=-157.70 M_y=-216.43 T_y=48.12 M_z=-52.33
  N,Ed=-1495.97 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-216.43 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.01 (sic.=78.001)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=-52.33 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic.=78.001)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 114 SLU - Classe 1
  Sollecitazioni: N,Ed=-1522.24 My,Ed=-216.43 Mz,Ed=-52.33 L=1.15
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=2056250.00 λ_{LT}=0.09
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_y=6.76 Ncr,y=35440800.00 λ^*_y=0.08 Curva b: Φ_y=0.00 χ_y=1.00
  λ_z=11.39 Ncr,z=12464500.00 λ^*_z=0.13 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.01+0.00=0.02 (sic.=42.875)
  Verifica ZZ: 0.01+0.01+0.01=0.02 (sic.=47.777)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 188
  $f_{Z,G}$=0.06 (L/1782) $f_{Z,L}$=0.06 (L/1844) (sic.=5.940)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 188
  $f_{Z,G}$=0.09 (L/1178) (sic.=4.712)

Asta n. 3054 (-65 -82) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.58 - Classe 3
  Sollecitazioni: T_z=-4.78
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 τ_{max}=1.09 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 $\sigma_{ID,max}$=1.88 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 72 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-28.35
  V,Ed=-28.35 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 72 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_z=-28.35
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.44 τ_{max}=6.44 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.44 $\sigma_{ID,max}$=11.16 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 77 SLU - Classe 1
  Sollecitazioni: N,Ed=-12.51 My,Ed=-5.20 L=0.58
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
  Verifica YY: 0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 161
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/605207) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 151
  $f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/605207) (sic.=52.060)

Asta n. 3055 (-66 -83) - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.58 - Classe 3

Sollecitazioni: T_z=-4.78
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 τ_{max}=1.09 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=1.09 $\sigma_{ID,max}$=1.88 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 83 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=28.89
V,Ed=28.89 Vc,Rd=9535.17 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica in termini tensionali [4.2.4] - CC 83 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=28.89
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.57 τ_{max}=6.57 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=6.57 $\sigma_{ID,max}$=11.38 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 102 SLU - Classe 1
Sollecitazioni: N,Ed=-15.32 My,Ed=-5.20 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=18890.40 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=11.77 Ncr,y=1977020.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=39.88 Ncr,z=172144.00 λ^*_z=0.46 Curva b: Φ_z=0.65 χ_z=0.90
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.00, 0.95
Verifica YY: 0.00+0.00=0.00 (sic. >100)
Verifica ZZ: 0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 131
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/403471) (sic.=42.923)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 131
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/605207) (sic.=51.508)

Asta n. 3057 (-85 -71) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.58 - Classe 3
Sollecitazioni: N=-980.27 T_z=673.14 M_y=-293.73 T_y=76.58 M_z=45.60 M_x=-1.41
Tensioni: σ_N=-12.55 $\sigma_{m,d}$=-74.33 τ=3.97 σ_{max}=-86.88 (sic.=30.145)
Tensioni: σ_N=-12.55 $\sigma_{m,d}$=-1.02 τ=44.27 τ_{max}=44.27 (sic.=34.155)
Tensioni: σ_N=-12.55 $\sigma_{m,d}$=-74.33 τ=3.97 $\sigma_{ID,max}$=87.15 (sic.=30.051)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 109 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=-10.36 M_x=-2.22
V,Ed=-10.36 Vc,Rd,Red=99671.70 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 109 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=755.42 M_x=-2.22
V,Ed=755.42 Vc,Rd,Red=37489.20 V,Ed/Vc,Rd,Red=0.02 (sic.=49.627)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 90 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-1780.64 T_z=358.93 M_y=310.95 T_y=106.72 M_z=3.31 M_x=-2.01
N,Ed=-1780.64 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=310.95 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=54.291)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=3.31 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.02 (sic.=54.291)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-980.27 My,Ed=-293.73 Mz,Ed=45.60 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.17 M,cr=10065800.00 λ_{LT}=0.04
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.02+0.01=0.03 (sic.=31.488)
Verifica ZZ: 0.00+0.01+0.01=0.03 (sic.=35.693)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 141
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/134490) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 161
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/110038) (sic.=51.508)

Asta n. 3057 (-71 -54) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.58 - Classe 3

Sollecitazioni: N=-1004.98 T_z=595.49 M_y=-647.50 T_y=52.99 M_z=76.07 M_x=-1.41
Tensioni: σ_N=-12.87 $\sigma_{m,d}$=-151.64 τ=3.97 σ_{max}=-164.51 (sic.=15.920)
Tensioni: σ_N=-12.87 $\sigma_{m,d}$=-1.71 τ=39.21 τ_{max}=39.21 (sic.=38.569)
Tensioni: σ_N=-12.87 $\sigma_{m,d}$=-151.64 τ=3.97 $\sigma_{ID,max}$=164.66 (sic.=15.906)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 61 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=43.02 M_x=-1.92
V,Ed=43.02 Vc,Rd,Red=99694.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 61 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=576.05 M_x=-1.92
V,Ed=576.05 Vc,Rd,Red=37497.60 V,Ed/Vc,Rd,Red=0.02 (sic.=65.094)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 114 SLU Xl=0.58 - Classe 1
Sollecitazioni: N=-1256.83 T_z=372.93 M_y=-507.14 T_y=-74.57 M_z=-85.88 M_x=-1.79
N,Ed=-1256.83 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-507.14 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.03 (sic.=33.289)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-85.88 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.01 (sic.=93.347)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.03 (sic.=33.289)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-1004.98 My,Ed=-647.50 Mz,Ed=76.07 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.29 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.34 M,cr=6184270.00 λ_{LT}=0.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.44 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=3.38 Ncr,y=141763000.00 λ^*_y=0.04 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=5.70 Ncr,z=49857800.00 λ^*_z=0.07 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.01=0.06 (sic.=16.687)
Verifica ZZ: 0.00+0.03+0.01=0.05 (sic.=19.350)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 146
$f_{Z,G}$=0.00 (L/13015) $f_{Z,L}$=0.00 (L/302603) (sic.=43.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 204
$f_{Z,G}$=0.00 (L/12877) $f_{Z,L}$=0.00 (L/172916) (sic.=51.508)

Asta n. 3057 (-54 242) - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=1.06 - Classe 3
Sollecitazioni: N=-1037.04 T_z=494.74 M_y=-1204.62 T_y=-507.32 M_z=-464.68 M_x=-1.41
Tensioni: σ_N=-13.28 $\sigma_{m,d}$=-443.42 τ=3.97 σ_{max}=-456.70 (sic.=5.735)
Tensioni: σ_N=-13.28 $\sigma_{m,d}$=-10.44 τ=32.92 τ_{max}=32.92 (sic.=45.931)
Tensioni: σ_N=-13.28 $\sigma_{m,d}$=-443.42 τ=3.97 $\sigma_{ID,max}$=456.75 (sic.=5.734)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 61 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=87.27 M_x=-1.92
V,Ed=87.27 Vc,Rd,Red=99694.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 61 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=501.53 M_x=-1.92
V,Ed=501.53 Vc,Rd,Red=37497.60 V,Ed/Vc,Rd,Red=0.01 (sic.=74.766)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=1.06 - Classe 1
Sollecitazioni: N=-1888.74 T_z=-207.05 M_y=307.98 T_y=-619.47 M_z=-523.16 M_x=-1.85
N,Ed=-1888.74 Nc,Rd=204503.00 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=307.98 My,V,c,Rd=16881.90 MNy,c,Rd=16881.90 My,Ed/MNy,c,Rd=0.02 (sic.=54.815)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=-523.16 Mz,V,c,Rd=8016.92 MNz,c,Rd=8016.92 Mz,Ed/MNz,c,Rd=0.07 (sic.=15.324)
α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.07 (sic.=15.246)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=-1037.04 My,Ed=-1204.62 Mz,Ed=-464.68 L=1.15
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.27 M,cr=1494890.00 λ_{LT}=0.10
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=6.76 Ncr,y=35440800.00 λ^*_y=0.08 Curva b: Φ_y=0.00 χ_y=1.00
λ_Z=11.39 Ncr,z=12464500.00 λ^*_z=0.13 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.08+0.08=0.17 (sic.=6.025)
Verifica ZZ: 0.01+0.06+0.08=0.15 (sic.=6.639)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 161
$f_{Z,G}$=0.01 (L/10834) $f_{Z,L}$=0.00 (L/27085) (sic.=36.113)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 161
  $f_{Z,G}$=0.01 (L/10282) $f_{Z,L}$=0.00 (L/21774) (sic.=41.128)

Asta n. 5001 (-20 -21) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica a compressione (4.2.4.1.2.2) - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-13.38 T_y=2.05
  Verifica a compressione [4.2.9]
  N,Ed=-13.38 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 17 SLU Xl=0.36
  Sollecitazioni: T_y=-2.67
  V,Ed=-2.67 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a compressione (4.2.4.1.2.2) - CC 84 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-5.66 T_y=2.67
  Verifica a compressione [4.2.9]
  N,Ed=-5.66 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-13.38 Mz,Ed=0.16 L=0.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=6.97 Ncr,y=7011060.00 λ^*_y=0.08 Curva a: Φ_y=0.49 χ_y=1.00
  λ_z=24.19 Ncr,z=581860.00 λ^*_z=0.28 Curva b: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00+0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 208
  $f_{Z,L}$=0.00 (L/8202) $f_{Z,G}$=0.00 (L/55575) (sic.=27.340)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 208
  $f_{Z,L}$=0.00 (L/7981) $f_{Z,G}$=0.00 (L/63514) (sic.=31.924)

Asta n. 5012 (27 -14) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=1.07 - Classe 3
  Sollecitazioni: N=-116.76 M_z=9.52
  Tensioni: σ_N=-7.11 $\sigma_{m,d}$=-77.40 τ=0.00 σ_{max}=-84.50 (sic.=30.994)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
  Tensioni: σ_N=-7.11 $\sigma_{m,d}$=-77.40 τ=0.00 $\sigma_{ID,max}$=84.50 (sic.=30.994)

- Verifica a taglio Dir. Y [4.2.16] - CC 21 SLU Xl=2.10 - Classe 1
  Sollecitazioni: T_y=-25.03
  V,Ed=-25.03 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 21 SLU Xl=2.10 - Classe 1
  Sollecitazioni: T_z=38.69
  V,Ed=38.69 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 23 SLU Xl=1.07 - Classe 1
  Sollecitazioni: M_y=-19.96 M_z=12.91
  N,Ed=0.00 Nc,Rd=43021.20 n=N,Ed/Nc,Rd=0.00
  My,Ed=-19.96 My,c,Rd=2320.00 My,Ed/My,c,Rd=0.01 (sic. >100) My,Ed/My,c,Rd=0.01 (sic. >100)
  Mz,Ed=12.91 Mz,c,Rd=504.58 Mz,Ed/Mz,c,Rd=0.03 (sic.=39.072) Mz,Ed/Mz,c,Rd=0.03 (sic.=39.072)
  α=2.00 β=1.00 $(My,Ed/My,c,Rd)^2+(Mz,Ed/Mz,c,Rd)^1$=0.03 (sic.=38.960)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-116.76 Mz,Ed=9.52 L=2.20
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=38.33 Ncr,y=231771.00 λ^*_y=0.44 Curva a: Φ_y=0.62 χ_y=0.94
  λ_z=133.04 Ncr,z=19235.00 λ^*_z=1.53 Curva b: Φ_z=1.90 χ_z=0.33
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.03=0.03 (sic.=32.160)
  Verifica ZZ: 0.01+0.03=0.04 (sic.=27.456)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 145
  $f_{Z,L}$=0.01 (L/21746) $f_{Z,G}$=0.00 (L/208553) (sic.=72.487)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 135
  $f_{Z,G}$=0.05 (L/4369) $f_{Z,L}$=0.01 (L/28284) (sic.=17.476)

Asta n. 5013 (-15 17) - Sez. 15 (Traversi secondari_facciata vetrata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.74 - Classe 3
  Sollecitazioni: N=-93.21 M_z=9.46
  Tensioni: σ_N=-2.74 $\sigma_{m,d}$=-17.88 τ=0.00 σ_{max}=-20.62 (sic. >100)
  Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)

Tensioni: σ_N=-2.74 $\sigma_{m,d}$=-17.88 τ=0.00 $\sigma_{ID,max}$=20.62 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 20 SLU Xl=1.39 - Classe 1
Sollecitazioni: T_y=-40.57
V,Ed=-40.57 Vc,Rd=44150.20 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 20 SLU Xl=1.39 - Classe 1
Sollecitazioni: T_z=90.94
V,Ed=90.94 Vc,Rd=16576.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 22 SLU Xl=0.74 - Classe 1
Sollecitazioni: N=-12.99 M_y=-29.33 M_z=13.08
N,Ed=-12.99 Nc,Rd=89065.70 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=-29.33 My,c,Rd=4340.46 MNy,c,Rd=4340.46 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=13.08 Mz,c,Rd=2122.91 MNz,c,Rd=2122.91 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 56 SLU - Classe 1
Sollecitazioni: N,Ed=-82.60 My,Ed=-29.33 Mz,Ed=13.08 L=1.45
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=42827.00 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=28.76 Ncr,y=852102.00 λ^*_y=0.33 Curva b: Φ_y=0.58 χ_y=0.95
λ_z=47.45 Ncr,z=313009.00 λ^*_z=0.55 Curva c: Φ_z=0.73 χ_z=0.82
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.00=0.01 (sic.=91.666)
Verifica ZZ: 0.00+0.00+0.01=0.01 (sic.=92.194)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
$f_{z,L}$=0.02 (L/7948) $f_{z,G}$=0.00 (L/59133) (sic.=26.493)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 203
$f_{z,L}$=0.02 (L/7862) $f_{z,G}$=0.00 (L/32206) (sic.=31.448)

Asta n. 5027 (18 45) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.54 - Classe 3
Sollecitazioni: N=16.03 T_z=30.66 T_y=-8.38 M_z=-5.42
Tensioni: σ_N=0.98 $\sigma_{m,d}$=44.02 τ=0.00 σ_{max}=45.00 (sic.=58.207)
Tensioni: σ_N=0.98 $\sigma_{m,d}$=2.83 τ=5.53 τ_{max}=5.53 (sic. >100)
Tensioni: σ_N=0.98 $\sigma_{m,d}$=44.02 τ=0.26 $\sigma_{ID,max}$=45.00 (sic.=58.204)

- Verifica a taglio Dir. Y [4.2.16] - CC 104 SLU Xl=0.09 - Classe 1
Sollecitazioni: T_y=-18.72
V,Ed=-18.72 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 104 SLU Xl=0.09 - Classe 1
Sollecitazioni: T_z=66.51
V,Ed=66.51 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 104 SLU Xl=0.54 - Classe 1
Sollecitazioni: N=-17.56 T_z=59.03 T_y=-18.72 M_z=-9.96
Mz,Ed=-9.96 Mz,V,c,Rd=504.58
N,Ed=-17.56 Nc,Rd=-43021.20 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.02
(sic.=50.651)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 104 SLU - Classe 1
Sollecitazioni: N,Ed=-17.56 My,Ed=27.77 Mz,Ed=-9.96 L=0.54
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.54 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.76 M,cr=40152.00 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=9.33 Ncr,y=3907760.00 λ^*_y=0.11 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=32.40 Ncr,z=324311.00 λ^*_z=0.37 Curva b: Φ_z=0.60 χ_z=0.94
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.01=0.02 (sic.=43.419)
Verifica ZZ: 0.00+0.01+0.02=0.03 (sic.=38.441)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 175
$f_{z,L}$=0.00 (L/98496) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 155
$f_{z,L}$=0.00 (L/89115) (sic. >100)

Asta n. 5028 (45 19) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.00 - Classe 3
Sollecitazioni: N=17.07 T_z=24.23 T_y=5.98 M_z=-5.42

Tensioni: σ_N=1.04 $\sigma_{m,d}$=44.02 τ=0.00 σ_{max}=45.06 (sic.=58.125)
Tensioni: σ_N=1.04 $\sigma_{m,d}$=2.83 τ=4.37 τ_{max}=4.37 (sic. >100)
Tensioni: σ_N=1.04 $\sigma_{m,d}$=44.02 τ=0.21 $\sigma_{ID,max}$=45.06 (sic.=58.123)

- Verifica a taglio Dir. Y [4.2.16] - CC 104 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_y=15.29
V,Ed=15.29 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 104 SLU Xl=0.00 - Classe 1
Sollecitazioni: T_z=49.39
V,Ed=49.39 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 104 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=-15.20 T_z=49.39 T_y=15.29 M_z=-9.96
Mz,Ed=-9.96 Mz,V,c,Rd=504.58
N,Ed=-15.20 Nc,Rd=-43021.20 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.02 (sic.=50.651)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 104 SLU - Classe 1
Sollecitazioni: N,Ed=-15.20 My,Ed=-23.50 Mz,Ed=-9.96 L=0.58
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.58 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.74 M,cr=33930.80 λ_{LT}=0.27
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=10.14 Ncr,y=3308890.00 λ^*_y=0.12 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=35.21 Ncr,z=274610.00 λ^*_z=0.41 Curva b: Φ_z=0.62 χ_z=0.92
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.01=0.02 (sic.=47.104)
Verifica ZZ: 0.00+0.01+0.02=0.02 (sic.=40.140)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 175
$f_{Z,L}$=0.00 (L/108152) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 155
$f_{Z,L}$=0.00 (L/144203) (sic. >100)

Asta n. 5029 (19 21) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 5 SND Xl=0.06 - Classe 3
Sollecitazioni: N=-42.84 T_z=19.41 M_y=6.74 T_y=11.21 M_z=-5.52
Tensioni: σ_N=-2.61 $\sigma_{m,d}$=-53.59 τ=0.00 σ_{max}=-56.19 (sic.=46.608)
Tensioni: σ_N=-2.61 $\sigma_{m,d}$=2.89 τ=3.50 τ_{max}=3.50 (sic. >100)
Tensioni: σ_N=-2.61 $\sigma_{m,d}$=-53.59 τ=0.00 $\sigma_{ID,max}$=56.19 (sic.=46.608)

- Verifica a taglio Dir. Y [4.2.16] - CC 104 SLU Xl=0.06 - Classe 1
Sollecitazioni: T_y=-13.53
V,Ed=-13.53 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 104 SLU Xl=0.06 - Classe 1
Sollecitazioni: T_z=46.87
V,Ed=46.87 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 84 SLU Xl=0.06 - Classe 1
Sollecitazioni: N=-41.23 T_z=2.98 T_y=15.02 M_z=-7.46
Mz,Ed=-7.46 Mz,V,c,Rd=504.58
N,Ed=-41.23 Nc,Rd=-43021.20 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.01 (sic.=67.675)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 56 SLU - Classe 1
Sollecitazioni: N,Ed=-90.41 My,Ed=-22.43 Mz,Ed=7.10 L=0.99
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.99 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.50 M,cr=18814.20 λ_{LT}=0.36
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=17.25 Ncr,y=1144660.00 λ^*_y=0.20 Curva a: Φ_y=0.52 χ_y=1.00
λ_z=59.87 Ncr,z=94997.50 λ^*_z=0.69 Curva b: Φ_z=0.82 χ_z=0.79
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.01=0.02 (sic.=51.736)
Verifica ZZ: 0.00+0.01+0.01=0.02 (sic.=46.349)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 146
$f_{Z,G}$=0.02 (L/5424) $f_{Z,L}$=0.00 (L/102156) (sic.=18.080)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 131
$f_{Z,G}$=0.02 (L/5473) $f_{Z,L}$=0.00 (L/459702) (sic.=21.892)

Asta n. 5030 (19 46) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.06 - Classe 3
Sollecitazioni: N=12.54 T_z=-23.72 M_y=-12.53 T_y=-4.73 M_z=-3.26
Tensioni: σ_N=0.76 $\sigma_{m,d}$=42.72 τ=0.00 σ_{max}=43.48 (sic.=60.234)

Tensioni: σ_N=0.76 $\sigma_{m,d}$=1.71 τ=4.28 τ_{max}=4.28 (sic. >100)
Tensioni: σ_N=0.76 $\sigma_{m,d}$=42.72 τ=0.00 $\sigma_{ID,max}$=43.48 (sic.=60.234)

- Verifica a taglio Dir. Y [4.2.16] - CC 104 SLU Xl=0.53 - Classe 1
Sollecitazioni: T_y=21.00
V,Ed=21.00 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 104 SLU Xl=0.53 - Classe 1
Sollecitazioni: T_z=-40.83
V,Ed=-40.83 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 36 SLU Xl=0.53 - Classe 1
Sollecitazioni: N=47.87 T_z=-15.11 T_y=-42.01 M_z=-14.02
Mz,Ed=-14.02 Mz,V,c,Rd=504.58
N,Ed=47.87 Nc,Rd=43021.20 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.03 (sic.=35.993)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 99 SLU - Classe 1
Sollecitazioni: N,Ed=-21.97 My,Ed=-11.33 Mz,Ed=6.54 L=0.53
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.53 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.74 M,cr=40082.00 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.30 Ncr,y=3937390.00 λ^*_y=0.11 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=32.28 Ncr,z=326771.00 λ^*_z=0.37 Curva b: Φ_z=0.60 χ_z=0.94
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.00+0.01=0.01 (sic.=79.736)
Verifica ZZ: 0.00+0.00+0.01=0.02 (sic.=63.909)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 127
$f_{Z,L}$=0.00 (L/116935) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 155
$f_{Z,G}$=0.00 (L/132527) (sic. >100)

Asta n. 5031 (46 23) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.00 - Classe 3
Sollecitazioni: N=11.26 T_z=-36.42 T_y=7.23 M_z=-5.06
Tensioni: σ_N=0.69 $\sigma_{m,d}$=41.14 τ=0.00 σ_{max}=41.82 (sic.=62.624)
Tensioni: σ_N=0.69 $\sigma_{m,d}$=2.65 τ=6.57 τ_{max}=6.57 (sic. >100)
Tensioni: σ_N=0.69 $\sigma_{m,d}$=41.14 τ=0.31 $\sigma_{ID,max}$=41.83 (sic.=62.619)

- Verifica a taglio Dir. Y [4.2.16] - CC 104 SLU Xl=0.52 - Classe 1
Sollecitazioni: T_y=-11.85
V,Ed=-11.85 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 104 SLU Xl=0.52 - Classe 1
Sollecitazioni: T_z=-59.47
V,Ed=-59.47 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 36 SLU Xl=0.00 - Classe 1
Sollecitazioni: N=80.74 T_z=-24.99 T_y=25.49 M_z=-14.02
Mz,Ed=-14.02 Mz,V,c,Rd=504.58
N,Ed=80.74 Nc,Rd=43021.20 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.03 (sic.=35.993)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 99 SLU - Classe 1
Sollecitazioni: N,Ed=-52.63 My,Ed=21.89 Mz,Ed=6.54 L=0.61
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.61 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=31164.30 λ_{LT}=0.28
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=10.66 Ncr,y=2995410.00 λ^*_y=0.12 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=37.01 Ncr,z=248594.00 λ^*_z=0.43 Curva b: Φ_z=0.63 χ_z=0.92
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.01=0.02 (sic.=56.887)
Verifica ZZ: 0.00+0.01+0.01=0.02 (sic.=52.534)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 127
$f_{Z,L}$=0.00 (L/104332) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 155
$f_{Z,L}$=0.00 (L/104332) (sic. >100)

Asta n. 5032 (3 4) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.36 - Classe 3
Sollecitazioni: T_y=-2.05
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.28 τ_{max}=0.28 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.28 $\sigma_{ID,max}$=0.49 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 17 SLU Xl=0.36

Sollecitazioni: T_y=-2.67
V,Ed=-2.67 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 84 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=3.33 T_y=2.67
Verifica a trazione [4.2.5]
N,Ed=3.33 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-7.27 Mz,Ed=0.16 L=0.40
αmy, αmz, αLT=0.95, 0.95, 0.95
λ_y=6.97 Ncr,y=7011060.00 λ^*_y=0.08 Curva a: Φ_y=0.49 χ_y=1.00
λ_z=24.19 Ncr,z=581860.00 λ^*_z=0.28 Curva b: Φ_z=0.55 χ_z=0.97
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.00=0.00 (sic. >100)
Verifica ZZ: 0.00+0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 208
$f_{Z,L}$=0.00 (L/10208) $f_{Z,G}$=0.00 (L/53352) (sic.=34.027)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 208
$f_{Z,L}$=0.00 (L/9956) $f_{Z,G}$=0.00 (L/63514) (sic.=39.824)

Asta n. 5043 (26 -16) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
Sollecitazioni: N=52.17 T_y=19.35 M_z=-9.33
Tensioni: σ_N=3.18 $\sigma_{m,d}$=75.83 τ=0.00 σ_{max}=79.01 (sic.=33.148)
Tensioni: σ_N=3.18 $\sigma_{m,d}$=-19.43 τ=2.68 τ_{max}=2.68 (sic. >100)
Tensioni: σ_N=3.18 $\sigma_{m,d}$=75.83 τ=0.00 $\sigma_{ID,max}$=79.01 (sic.=33.148)

- Verifica a taglio Dir. Y [4.2.16] - CC 46 SLU Xl=1.90 - Classe 1
Sollecitazioni: T_y=-11.90
V,Ed=-11.90 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 46 SLU Xl=1.90 - Classe 1
Sollecitazioni: T_z=33.68
V,Ed=33.68 Vc,Rd=11556.80 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 85 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-8.14 T_y=27.79 M_z=-16.17
Mz,Ed=-16.17 Mz,V,c,Rd=504.58
N,Ed=-8.14 Nc,Rd=-43021.20 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.03 (sic.=31.207)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 75 SLU - Classe 1
Sollecitazioni: N,Ed=-2.15 My,Ed=-30.19 Mz,Ed=-12.49 L=2.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=4455.60 λ_{LT}=0.74
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.76 β_{LT}=0.75 f=0.97 χ_{LT}=0.88
λ_y=34.84 Ncr,y=280443.00 λ^*_y=0.40 Curva a: Φ_y=0.60 χ_y=0.95
λ_z=120.95 Ncr,z=23274.40 λ^*_z=1.39 Curva b: Φ_z=1.67 χ_z=0.38
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.01=0.03 (sic.=35.351)
Verifica ZZ: 0.00+0.01+0.02=0.03 (sic.=31.124)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 135
$f_{Z,L}$=0.01 (L/15206) $f_{Z,G}$=0.01 (L/24013) (sic.=50.687)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 130
$f_{Z,G}$=0.01 (L/13883) $f_{Z,L}$=0.01 (L/16490) (sic.=55.532)

Asta n. 5043 (-17 26) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.16 - Classe 3
Sollecitazioni: N=52.17 T_y=-99.43 M_z=-6.77
Tensioni: σ_N=3.18 $\sigma_{m,d}$=55.02 τ=0.00 σ_{max}=58.20 (sic.=45.004)
Tensioni: σ_N=3.18 $\sigma_{m,d}$=-14.09 τ=13.78 τ_{max}=13.78 (sic. >100)
Tensioni: σ_N=3.18 $\sigma_{m,d}$=55.02 τ=0.00 $\sigma_{ID,max}$=58.20 (sic.=45.004)

- Verifica a taglio Dir. Y [4.2.16] - CC 85 SLU Xl=0.16 - Classe 1
Sollecitazioni: T_y=-269.24
V,Ed=-269.24 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.02 (sic.=62.639)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 85 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=-8.14 T_y=-266.63 M_z=26.67
Mz,Ed=26.67 Mz,V,c,Rd=504.58
N,Ed=-8.14 Nc,Rd=-43021.20 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.05 (sic.=18.918)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 85 SLU - Classe 1

Sollecitazioni: N,Ed=-8.14 My,Ed=0.03 Mz,Ed=26.67 L=0.20
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.03 M,cr=161299.00 λ_{LT}=0.12
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.46 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=3.48 Ncr,y=28044200.00 λ^*_y=0.04 Curva a: Φ_y=0.00 χ_y=1.00
λ_z=12.09 Ncr,z=2327430.00 λ^*_z=0.14 Curva b: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.00+0.03=0.03 (sic.=32.972)
Verifica ZZ: 0.00+0.05=0.05 (sic.=19.838)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 184
$f_{Z,G}$=0.00 (L/28036) (sic.=93.453)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 184
$f_{Z,G}$=0.00 (L/29593) (sic. >100)

Asta n. 5043 (28 -17) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.36 - Classe 3
Sollecitazioni: N=-7.80 T_y=30.44 M_z=10.49
Tensioni: σ_N=-0.47 $\sigma_{m,d}$=-85.21 τ=0.00 σ_{max}=-85.69 (sic.=30.565)
Tensioni: σ_N=-0.47 $\sigma_{m,d}$=21.83 τ=4.22 τ_{max}=4.22 (sic. >100)
Tensioni: σ_N=-0.47 $\sigma_{m,d}$=-85.21 τ=0.00 $\sigma_{ID,max}$=85.69 (sic.=30.565)

- Verifica a taglio Dir. Y [4.2.16] - CC 85 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=103.49
V,Ed=103.49 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 85 SLU Xl=0.36 - Classe 1
Sollecitazioni: N=-16.84 T_y=98.08 M_z=32.50
Mz,Ed=32.50 Mz,V,c,Rd=504.58
N,Ed=-16.84 Nc,Rd=-43021.20 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=504.58 Mz,Ed/MNz,c,Rd=0.06
(sic.=15.524)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 115 SLU - Classe 1
Sollecitazioni: N,Ed=-16.82 My,Ed=-12.28 Mz,Ed=31.07 L=0.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=69906.70 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=6.97 Ncr,y=7011070.00 λ^*_y=0.08 Curva a: Φ_y=0.49 χ_y=1.00
λ_z=24.19 Ncr,z=581860.00 λ^*_z=0.28 Curva b: Φ_z=0.55 χ_z=0.97
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.04=0.04 (sic.=24.683)
Verifica ZZ: 0.00+0.00+0.06=0.06 (sic.=16.152)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
$f_{Z,L}$=0.02 (L/1775) $f_{Z,G}$=0.00 (L/30742) (sic.=5.917)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
$f_{Z,L}$=0.02 (L/1771) $f_{Z,G}$=0.00 (L/19747) (sic.=7.084)

Asta n. 5063 (43 6) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.66 - Classe 3
Sollecitazioni: T_y=-3.60
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.50 τ_{max}=0.50 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.50 $\sigma_{ID,max}$=0.86 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 17 SLU Xl=0.66
Sollecitazioni: T_y=-4.69
V,Ed=-4.69 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a compressione (4.2.4.1.2.2) - CC 37 SLU Xl=0.10 - Classe 1
Sollecitazioni: N=-1.63 T_y=4.69
Verifica a compressione [4.2.9]
N,Ed=-1.63 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-1.09 Mz,Ed=0.50 L=0.70
αmy, αmz, αLT=0.95, 0.95, 0.95
λ_y=12.19 Ncr,y=2289330.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_z=42.33 Ncr,z=189995.00 λ^*_z=0.49 Curva b: Φ_z=0.67 χ_z=0.89
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.00=0.00 (sic. >100)
Verifica ZZ: 0.00+0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
$f_{Z,G}$=0.01 (L/8781) $f_{Z,L}$=0.00 (L/12347) (sic.=29.270)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 203
  $f_{Z,G}$=0.01 (L/8030) $f_{Z,L}$=0.00 (L/11427) (sic.=32.120)

Asta n. 5074 (30 -18) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=382.45 T_y=548.90 M_z=-143.78
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=258.52 τ=0.00 σ_{max}=270.69 (sic.=9.675)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=-54.47 τ=33.01 τ_{max}=33.01 (sic.=45.809)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=258.52 τ=0.00 $\sigma_{ID,max}$=270.69 (sic.=9.675)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 46 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=136.87 M_x=-14.41
  V,Ed=136.87 Vc,Rd,Red=38051.10 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 46 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=238.15 M_x=-14.41
  V,Ed=238.15 Vc,Rd,Red=14616.40 V,Ed/Vc,Rd,Red=0.02 (sic.=61.374)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 79 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=797.10 T_y=502.32 M_z=-131.25
  Mz,Ed=-131.25 Mz,V,c,Rd=2224.38
  N,Ed=797.10 Nc,Rd=82282.30 ZZ n=N,Ed/Nc,Rd=0.01 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.06
(sic.=16.948)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 37 SLU - Classe 1
  Sollecitazioni: N,Ed=-25.40 My,Ed=0.00 Mz,Ed=-56.22 L=0.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=557235.00 λ_{LT}=0.09
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.45 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=6.98 Ncr,y=13383300.00 λ^*_y=0.08 Curva b: Φ_y=0.00 χ_y=1.00
  λ_Z=11.36 Ncr,z=5043210.00 λ^*_z=0.13 Curva c: Φ_z=0.00 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01=0.01 (sic.=67.963)
  Verifica ZZ: 0.00+0.02=0.02 (sic.=41.124)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
  $f_{Z,L}$=0.01 (L/3003) $f_{Z,G}$=0.00 (L/73680) (sic.=10.010)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 203
  $f_{Z,G}$=0.01 (L/2043) $f_{Z,L}$=0.00 (L/42508) (sic.=8.172)

Asta n. 5074 (31 30) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=382.45 T_y=-299.44 M_z=-152.89
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=274.89 τ=0.00 σ_{max}=287.06 (sic.=9.124)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=-57.92 τ=18.01 τ_{max}=18.01 (sic.=83.973)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=274.89 τ=0.00 $\sigma_{ID,max}$=287.06 (sic.=9.124)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 46 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-20.07 M_x=-12.81
  V,Ed=-20.07 Vc,Rd,Red=38255.40 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 46 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=187.97 M_x=-12.81
  V,Ed=187.97 Vc,Rd,Red=14694.90 V,Ed/Vc,Rd,Red=0.01 (sic.=78.178)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 79 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=797.10 T_y=-230.81 M_z=-141.16
  Mz,Ed=-141.16 Mz,V,c,Rd=2224.38
  N,Ed=797.10 Nc,Rd=82282.30 ZZ n=N,Ed/Nc,Rd=0.01 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.06
(sic.=15.758)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 67 SLU - Classe 1
  Sollecitazioni: N,Ed=-39.17 My,Ed=-108.31 Mz,Ed=-41.98 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.35 M,cr=183062.00 λ_{LT}=0.16
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00
  λ_Z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.02+0.01=0.03 (sic.=29.590)
  Verifica ZZ: 0.00+0.01+0.02=0.03 (sic.=31.308)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 145
  $f_{Z,L}$=0.00 (L/24938) $f_{Z,G}$=0.00 (L/74009) (sic.=83.127)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 178

$f_{Z,G}$=0.00 (L/16388) $f_{Z,L}$=0.00 (L/1147140) (sic.=65.552)

Asta n. 5074 (32 31) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=384.02 T_y=-57.03 M_z=-47.47
  Tensioni: σ_N=12.22 $\sigma_{m,d}$=85.36 τ=0.00 σ_{max}=97.58 (sic.=26.839)
  Tensioni: σ_N=12.22 $\sigma_{m,d}$=-17.99 τ=3.43 τ_{max}=3.43 (sic. >100)
  Tensioni: σ_N=12.22 $\sigma_{m,d}$=85.36 τ=0.00 $\sigma_{ID,max}$=97.58 (sic.=26.839)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 46 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-28.87 M_x=-9.78
  V,Ed=-28.87 Vc,Rd,Red=38639.50 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 46 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=143.09 M_x=-9.78
  V,Ed=143.09 Vc,Rd,Red=14842.50 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 66 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=129.96 T_z=-143.08 M_y=-270.60 T_y=-26.60 M_z=3.28 M_x=9.75
  N,Ed=129.96 Nc,Rd=82282.30 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-270.60 My,V,c,Rd=4560.12 MNy,c,Rd=4560.12 My,Ed/MNy,c,Rd=0.06 (sic.=16.852)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=3.28 Mz,V,c,Rd=2224.38 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.00 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.06 (sic.=16.852)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 95 SLU - Classe 1
  Sollecitazioni: N,Ed=-1.39 My,Ed=162.34 Mz,Ed=-24.21 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.16 M,cr=156247.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00
  λ_z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.03+0.01=0.04 (sic.=24.974)
  Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=32.627)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 120
  $f_{Z,L}$=0.00 (L/15094) $f_{Z,G}$=0.00 (L/764761) (sic.=50.313)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 120
  $f_{Z,L}$=0.00 (L/15094) $f_{Z,G}$=0.00 (L/127460) (sic.=60.376)

Asta n. 5074 (33 32) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=382.45 T_y=-45.07 M_z=31.93
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=57.41 τ=0.00 σ_{max}=69.58 (sic.=37.639)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=12.10 τ=2.71 τ_{max}=2.71 (sic. >100)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=57.41 τ=0.00 $\sigma_{ID,max}$=69.58 (sic.=37.639)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-50.13 M_x=-6.74
  V,Ed=-50.13 Vc,Rd,Red=39022.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=98.23 M_x=-6.74
  V,Ed=98.23 Vc,Rd,Red=14989.40 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=738.12 T_z=98.22 M_y=332.93 T_y=-50.28 M_z=31.72 M_x=-6.73
  N,Ed=738.12 Nc,Rd=82282.30 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=332.93 My,V,c,Rd=4560.12 MNy,c,Rd=4560.12 My,Ed/MNy,c,Rd=0.07 (sic.=13.697)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=31.72 Mz,V,c,Rd=2224.38 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.01 (sic.=70.117)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.07 (sic.=13.697)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 95 SLU - Classe 1
  Sollecitazioni: N,Ed=-1.39 My,Ed=199.75 Mz,Ed=34.60 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.08 M,cr=146123.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00
  λ_z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.04+0.01=0.05 (sic.=19.803)

Verifica ZZ: 0.00+0.02+0.01=0.04 (sic.=25.149)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 122
  $f_{Z,L}$=0.00 (L/11826) $f_{Z,G}$=0.00 (L/2294290) (sic.=39.420)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 122
  $f_{Z,L}$=0.00 (L/11706) $f_{Z,G}$=0.00 (L/67479) (sic.=46.824)

Asta n. 5074 (34 33) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=382.45 T_y=-34.15 M_z=43.83
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=78.81 τ=0.00 σ_{max}=90.99 (sic.=28.785)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=16.61 τ=2.05 τ_{max}=2.05 (sic. >100)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=78.81 τ=0.00 $\sigma_{ID,max}$=90.99 (sic.=28.785)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-42.04 M_x=-3.71
  V,Ed=-42.04 Vc,Rd,Red=39398.70 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=53.35 M_x=-3.71
  V,Ed=53.35 Vc,Rd,Red=15134.10 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 89 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=738.12 T_z=53.35 M_y=367.50 T_y=-40.80 M_z=62.80 M_x=-3.71
  N,Ed=738.12 Nc,Rd=82282.30 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=367.50 My,V,c,Rd=4560.12 MNy,c,Rd=4560.12 My,Ed/MNy,c,Rd=0.08 (sic.=12.408)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=62.80 Mz,V,c,Rd=2224.38 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.03 (sic.=35.417)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=12.408)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 95 SLU - Classe 1
  Sollecitazioni: N,Ed=-1.39 My,Ed=220.50 Mz,Ed=64.90 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.04 M,cr=140333.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00
  λ_z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.05+0.02=0.06 (sic.=15.978)
  Verifica ZZ: 0.00+0.03+0.03=0.06 (sic.=18.084)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 126
  $f_{Z,L}$=0.01 (L/10429) $f_{Z,G}$=0.00 (L/286786) (sic.=34.763)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 208
  $f_{Z,L}$=0.01 (L/10429) $f_{Z,G}$=0.00 (L/23899) (sic.=41.716)

Asta n. 5074 (36 34) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=384.02 T_y=-35.22 M_z=65.57
  Tensioni: σ_N=12.22 $\sigma_{m,d}$=117.90 τ=0.00 σ_{max}=130.13 (sic.=20.127)
  Tensioni: σ_N=12.22 $\sigma_{m,d}$=24.84 τ=2.12 τ_{max}=2.12 (sic. >100)
  Tensioni: σ_N=12.22 $\sigma_{m,d}$=117.90 τ=0.00 $\sigma_{ID,max}$=130.13 (sic.=20.127)

- Verifica a taglio Dir. Y [4.2.16] - CC 97 SLU Xl=0.58 - Classe 1
  Sollecitazioni: T_y=-72.29
  V,Ed=-72.29 Vc,Rd=39855.60 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=192.94 T_z=8.48 M_y=374.32 T_y=-38.97 M_z=96.01
  N,Ed=192.94 Nc,Rd=82282.30 n=N,Ed/Nc,Rd=0.00
  Pressoflessione retta YY [4.2.33]:
  My,Ed=374.32 My,V,c,Rd=4560.12 MNy,c,Rd=4560.12 My,Ed/MNy,c,Rd=0.08 (sic.=12.182)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=96.01 Mz,V,c,Rd=2224.38 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.04 (sic.=23.168)
  α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=12.182)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 95 SLU - Classe 1
  Sollecitazioni: N,Ed=-1.39 My,Ed=224.60 Mz,Ed=90.80 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.01 M,cr=136004.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00

λ_z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.05+0.02=0.07 (sic.=14.270)
Verifica ZZ: 0.00+0.03+0.04=0.07 (sic.=14.954)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 120
$f_{z,L}$=0.01 (L/10063) $f_{z,G}$=0.00 (L/229428) (sic.=33.543)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 140
$f_{z,L}$=0.01 (L/9975) $f_{z,G}$=0.00 (L/19119) (sic.=39.900)

Asta n. 5074 (37 36) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.36 - Classe 3
Sollecitazioni: N=384.02 T_y=23.42 M_z=66.77
Tensioni: σ_N=12.22 $\sigma_{m,d}$=120.06 τ=0.00 σ_{max}=132.28 (sic.=19.799)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=25.30 τ=1.41 τ_{max}=1.41 (sic. >100)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=120.06 τ=0.00 $\sigma_{ID,max}$=132.28 (sic.=19.799)

- Verifica a taglio Dir. Y [4.2.16] - CC 77 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=50.12
V,Ed=50.12 Vc,Rd=39855.60 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 94 SLU Xl=0.36 - Classe 1
Sollecitazioni: N=192.94 T_z=-14.06 M_y=374.09 T_y=21.58 M_z=96.64
N,Ed=192.94 Nc,Rd=82282.30 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=374.09 My,V,c,Rd=4560.12 MNy,c,Rd=4560.12 My,Ed/MNy,c,Rd=0.08 (sic.=12.190)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=96.64 Mz,V,c,Rd=2224.38 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.04 (sic.=23.016)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=12.190)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 95 SLU - Classe 1
Sollecitazioni: N,Ed=-1.39 My,Ed=224.46 Mz,Ed=91.43 L=0.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.40 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.01 M,cr=320195.00 λ_{LT}=0.12
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.46 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_y=6.98 Ncr,y=13383300.00 λ^*_y=0.08 Curva b: Φ_y=0.00 χ_y=1.00
λ_z=11.36 Ncr,z=5043210.00 λ^*_z=0.13 Curva c: Φ_z=0.00 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.05+0.02=0.07 (sic.=14.243)
Verifica ZZ: 0.00+0.03+0.04=0.07 (sic.=14.898)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 120
$f_{z,L}$=0.00 (L/14591) $f_{z,G}$=0.00 (L/274308) (sic.=48.637)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 145
$f_{z,L}$=0.00 (L/14287) $f_{z,G}$=0.00 (L/24937) (sic.=57.148)

Asta n. 5074 (38 37) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.55 - Classe 3
Sollecitazioni: N=384.02 T_y=22.81 M_z=64.59
Tensioni: σ_N=12.22 $\sigma_{m,d}$=116.13 τ=0.00 σ_{max}=128.35 (sic.=20.405)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=24.47 τ=1.37 τ_{max}=1.37 (sic. >100)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=116.13 τ=0.00 $\sigma_{ID,max}$=128.35 (sic.=20.405)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 114 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=42.31 M_x=-2.34
V,Ed=42.31 Vc,Rd,Red=39567.60 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 114 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_z=36.53 M_x=-2.34
V,Ed=36.53 Vc,Rd,Red=15198.90 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.58 - Classe 1
Sollecitazioni: N=675.14 T_z=36.52 M_y=-367.67 T_y=10.25 M_z=64.44 M_x=-2.36
N,Ed=675.14 Nc,Rd=82282.30 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-367.67 My,V,c,Rd=4560.12 MNy,c,Rd=4560.12 My,Ed/MNy,c,Rd=0.08 (sic.=12.403)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=64.44 Mz,V,c,Rd=2224.38 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.03 (sic.=34.521)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=12.403)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 95 SLU - Classe 1
Sollecitazioni: N,Ed=-1.39 My,Ed=220.61 Mz,Ed=82.94 L=0.62
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.03 M,cr=138666.00 λ_{LT}=0.19

$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00
λ_z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.05+0.02=0.07 (sic.=14.874)
Verifica ZZ: 0.00+0.03+0.04=0.06 (sic.=15.869)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 122
$f_{Z,L}$=0.01 (L/10524) $f_{Z,G}$=0.00 (L/327755) (sic.=35.080)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 120
$f_{Z,L}$=0.01 (L/10429) $f_{Z,G}$=0.00 (L/20485) (sic.=41.716)

Asta n. 5074 (39 38) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.58 - Classe 3
Sollecitazioni: N=384.02 T_y=27.74 M_z=60.84
Tensioni: σ_N=12.22 $\sigma_{m,d}$=109.40 τ=0.00 σ_{max}=121.62 (sic.=21.534)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=23.05 τ=1.67 τ_{max}=1.67 (sic. >100)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=109.40 τ=0.00 $\sigma_{ID,max}$=121.62 (sic.=21.534)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 114 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=46.26 M_x=-5.37
V,Ed=46.26 Vc,Rd,Red=39192.50 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 114 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_z=81.40 M_x=-5.37
V,Ed=81.40 Vc,Rd,Red=15054.90 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.58 - Classe 1
Sollecitazioni: N=675.14 T_z=81.39 M_y=-343.49 T_y=17.79 M_z=52.37 M_x=-5.38
N,Ed=675.14 Nc,Rd=82282.30 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-343.49 My,V,c,Rd=4560.12 MNy,c,Rd=4560.12 My,Ed/MNy,c,Rd=0.08 (sic.=13.276)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=52.37 Mz,V,c,Rd=2224.38 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.02 (sic.=42.475)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.08 (sic.=13.276)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 95 SLU - Classe 1
Sollecitazioni: N,Ed=-1.39 My,Ed=206.09 Mz,Ed=62.99 L=0.62
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.06 M,cr=143809.00 λ_{LT}=0.18
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00
λ_z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.04+0.02=0.06 (sic.=16.923)
Verifica ZZ: 0.00+0.03+0.03=0.05 (sic.=18.983)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 120
$f_{Z,L}$=0.00 (L/11826) $f_{Z,G}$=0.00 (L/458857) (sic.=39.420)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 124
$f_{Z,L}$=0.00 (L/11706) $f_{Z,G}$=0.00 (L/27979) (sic.=46.824)

Asta n. 5074 (40 39) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.58 - Classe 3
Sollecitazioni: N=384.02 T_y=47.41 M_z=55.45
Tensioni: σ_N=12.22 $\sigma_{m,d}$=99.70 τ=0.00 σ_{max}=111.93 (sic.=23.400)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=21.01 τ=2.85 τ_{max}=2.85 (sic. >100)
Tensioni: σ_N=12.22 $\sigma_{m,d}$=99.70 τ=0.00 $\sigma_{ID,max}$=111.93 (sic.=23.400)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 66 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_y=53.94 M_x=-8.42
V,Ed=53.94 Vc,Rd,Red=38811.70 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 66 SLU Xl=0.04 - Classe 1
Sollecitazioni: T_z=126.27 M_x=-8.42
V,Ed=126.27 Vc,Rd,Red=14908.60 V,Ed/Vc,Rd,Red=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 61 SLU Xl=0.58 - Classe 1
Sollecitazioni: N=675.14 T_z=126.26 M_y=-291.57 T_y=32.14 M_z=35.38 M_x=-8.41
N,Ed=675.14 Nc,Rd=82282.30 n=N,Ed/Nc,Rd=0.01
Pressoflessione retta YY [4.2.33]:
My,Ed=-291.57 My,V,c,Rd=4560.12 MNy,c,Rd=4560.12 My,Ed/MNy,c,Rd=0.06 (sic.=15.640)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=35.38 Mz,V,c,Rd=2224.38 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.02 (sic.=62.874)

α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.06 (sic.=15.640)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 95 SLU - Classe 1
  Sollecitazioni: N,Ed=-1.39 My,Ed=174.93 Mz,Ed=40.47 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.12 M,cr=151933.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00
  λ_Z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.04+0.01=0.05 (sic.=21.354)
  Verifica ZZ: 0.00+0.02+0.02=0.04 (sic.=25.531)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 126
  $f_{Z,L}$=0.00 (L/14898) $f_{Z,G}$=0.00 (L/573571) (sic.=49.660)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 120
  $f_{Z,L}$=0.00 (L/14898) $f_{Z,G}$=0.00 (L/48815) (sic.=59.592)

Asta n. 5074 (41 40) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 1 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=384.02 T_y=-117.87 M_z=46.68
  Tensioni: σ_N=12.22 $\sigma_{m,d}$=83.93 τ=0.00 σ_{max}=96.15 (sic.=27.239)
  Tensioni: σ_N=12.22 $\sigma_{m,d}$=17.68 τ=7.09 τ_{max}=7.09 (sic. >100)
  Tensioni: σ_N=12.22 $\sigma_{m,d}$=83.93 τ=0.00 $\sigma_{ID,max}$=96.15 (sic.=27.239)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 66 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_y=-60.81 M_x=-11.44
  V,Ed=-60.81 Vc,Rd,Red=38429.30 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 66 SLU Xl=0.04 - Classe 1
  Sollecitazioni: T_z=171.14 M_x=-11.44
  V,Ed=171.14 Vc,Rd,Red=14761.70 V,Ed/Vc,Rd,Red=0.01 (sic.=86.255)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 109 SLU Xl=0.58 - Classe 1
  Sollecitazioni: N=774.14 T_z=171.14 M_y=-211.89 T_y=-42.40 M_z=13.18 M_x=-11.42
  N,Ed=774.14 Nc,Rd=82282.30 n=N,Ed/Nc,Rd=0.01
  Pressoflessione retta YY [4.2.33]:
  My,Ed=-211.89 My,V,c,Rd=4560.12 MNy,c,Rd=4560.12 My,Ed/MNy,c,Rd=0.05 (sic.=21.521)
  Pressoflessione retta ZZ [4.2.34]:
  Mz,Ed=13.18 Mz,V,c,Rd=2224.38 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
  α=2.00 β=1.00 (My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1=0.05 (sic.=21.521)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 67 SLU - Classe 1
  Sollecitazioni: N,Ed=-39.17 My,Ed=-127.12 Mz,Ed=54.13 L=0.62
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.26 M,cr=170056.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00
  λ_Z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.03+0.01=0.04 (sic.=24.493)
  Verifica ZZ: 0.00+0.02+0.02=0.04 (sic.=25.329)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 122
  $f_{Z,L}$=0.00 (L/23899) $f_{Z,G}$=0.00 (L/327755) (sic.=79.663)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 120
  $f_{Z,L}$=0.00 (L/23899) $f_{Z,G}$=0.00 (L/62008) (sic.=95.596)

Asta n. 5074 (-19 41) - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 9 SND Xl=0.58 - Classe 3
  Sollecitazioni: N=382.45 T_y=77.28 M_z=40.25
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=72.36 τ=0.00 σ_{max}=84.54 (sic.=30.981)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=15.25 τ=4.65 τ_{max}=4.65 (sic. >100)
  Tensioni: σ_N=12.17 $\sigma_{m,d}$=72.36 τ=0.00 $\sigma_{ID,max}$=84.54 (sic.=30.981)

- Verifica a taglio e torsione Dir. Y [4.2.24] - CC 66 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_y=107.04 M_x=-14.47
  V,Ed=107.04 Vc,Rd,Red=38043.00 V,Ed/Vc,Rd,Red=0.00 (sic. >100)

- Verifica a taglio e torsione Dir. Z [4.2.24] - CC 66 SLU Xl=0.10 - Classe 1
  Sollecitazioni: T_z=216.01 M_x=-14.47
  V,Ed=216.01 Vc,Rd,Red=14613.30 V,Ed/Vc,Rd,Red=0.01 (sic.=67.650)

- Verifica a presso o tenso-flessione retta ZZ (4.2.4.1.2.7) - CC 85 SLU Xl=0.58 - Classe 1

Sollecitazioni: N=34.00 T_y=111.17 M_z=57.50
Mz,Ed=57.50 Mz,V,c,Rd=2224.38
N,Ed=34.00 Nc,Rd=82282.30 ZZ n=N,Ed/Nc,Rd=0.00 MNz,c,Rd=2224.38 Mz,Ed/MNz,c,Rd=0.03 (sic.=38.686)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 67 SLU - Classe 1
Sollecitazioni: N,Ed=-39.17 My,Ed=-62.67 Mz,Ed=52.97 L=0.62
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=0.62 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=236675.00 λ_{LT}=0.14
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.46 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=10.81 Ncr,y=5570570.00 λ^*_y=0.12 Curva b: Φ_y=0.49 χ_y=1.00
λ_Z=17.61 Ncr,z=2099150.00 λ^*_z=0.20 Curva c: Φ_z=0.52 χ_z=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.01=0.03 (sic.=36.894)
Verifica ZZ: 0.00+0.01+0.02=0.03 (sic.=32.329)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
$f_{Z,G}$=0.01 (L/5930) $f_{Z,L}$=0.00 (L/67598) (sic.=19.767)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
$f_{Z,G}$=0.02 (L/2763) $f_{Z,L}$=0.00 (L/37555) (sic.=11.052)

Asta n. 5075 (22 -16) - Sez. 15 (Traversi secondari_facciata vetrata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 13 SND Xl=0.70 - Classe 3
Sollecitazioni: N=-93.85 M_z=9.46
Tensioni: σ_N=-2.76 $\sigma_{m,d}$=-17.88 τ=0.00 σ_{max}=-20.64 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 τ_{max}=0.00 (sic. >100)
Tensioni: σ_N=-2.76 $\sigma_{m,d}$=-17.88 τ=0.00 $\sigma_{ID,max}$=20.64 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 20 SLU Xl=1.35 - Classe 1
Sollecitazioni: T_y=-40.57
V,Ed=-40.57 Vc,Rd=44150.20 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Z [4.2.16] - CC 20 SLU Xl=1.35 - Classe 1
Sollecitazioni: T_z=90.94
V,Ed=90.94 Vc,Rd=16576.10 V,Ed/Vc,Rd=0.01 (sic. >100)

- Verifica a presso o tenso flessione biassiale (EC3 6.41) - CC 20 SLU Xl=0.70 - Classe 1
Sollecitazioni: N=-4.78 M_y=29.33 M_z=13.08
N,Ed=-4.78 Nc,Rd=89065.70 n=N,Ed/Nc,Rd=0.00
Pressoflessione retta YY [4.2.33]:
My,Ed=29.33 My,c,Rd=4340.46 MNy,c,Rd=4340.46 My,Ed/MNy,c,Rd=0.01 (sic. >100)
Pressoflessione retta ZZ [4.2.34]:
Mz,Ed=13.08 Mz,c,Rd=2122.91 MNz,c,Rd=2122.91 Mz,Ed/MNz,c,Rd=0.01 (sic. >100)
α=2.00 β=1.00 $(My,Ed/MNy,c,Rd)^2+(Mz,Ed/MNz,c,Rd)^1$=0.01 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 84 SLU - Classe 1
Sollecitazioni: N,Ed=-82.16 My,Ed=29.33 Mz,Ed=13.08 L=1.45
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.45 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=42827.00 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=28.76 Ncr,y=852102.00 λ^*_y=0.33 Curva b: Φ_y=0.58 χ_y=0.95
λ_Z=47.45 Ncr,z=313009.00 λ^*_z=0.55 Curva c: Φ_z=0.73 χ_z=0.82
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.00=0.01 (sic.=91.710)
Verifica ZZ: 0.00+0.00+0.01=0.01 (sic.=92.246)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 155
$f_{Z,L}$=0.02 (L/8073) $f_{Z,G}$=0.00 (L/73614) (sic.=26.910)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 155
$f_{Z,L}$=0.02 (L/8053) $f_{Z,G}$=0.00 (L/36682) (sic.=32.212)

Asta n. 5094 (11 12) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica in termini tensionali [4.2.4] - CC 7 SND Xl=0.36 - Classe 3
Sollecitazioni: T_y=-2.05
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.00 σ_{max}=0.00 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.28 τ_{max}=0.28 (sic. >100)
Tensioni: σ_N=0.00 $\sigma_{m,d}$=0.00 τ=0.28 $\sigma_{ID,max}$=0.49 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 17 SLU Xl=0.36
Sollecitazioni: T_y=-2.67
V,Ed=-2.67 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a trazione (4.2.4.1.2.1) - CC 56 SLU Xl=0.04 - Classe 1
Sollecitazioni: N=3.81 T_y=2.67
Verifica a trazione [4.2.5]

N,Ed=3.81 Npl,Rd=43021.20 Nu,Rd=50855.80 N,Ed/Nt,Rd=0.00 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=-7.12 Mz,Ed=0.16 L=0.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=6.97 Ncr,y=7011060.00 λ^*_y=0.08 Curva a: Φ_y=0.49 χ_y=1.00
  λ_z=24.19 Ncr,z=581859.00 λ^*_z=0.28 Curva b: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00+0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 208
  $f_{z,L}$=0.00 (L/8815) $f_{z,G}$=0.00 (L/266758) (sic.=29.383)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 208
  $f_{z,L}$=0.00 (L/8634) $f_{z,G}$=0.00 (L/74099) (sic.=34.536)

Asta n. 5125 (-22 -23) - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica a compressione (4.2.4.1.2.2) - CC 9 SND Xl=0.04 - Classe 3
  Sollecitazioni: N=-13.99 T_y=2.05
  Verifica a compressione [4.2.9]
  N,Ed=-13.99 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica a taglio Dir. Y [4.2.16] - CC 17 SLU Xl=0.36
  Sollecitazioni: T_y=-2.67
  V,Ed=-2.67 Vc,Rd=16864.90 V,Ed/Vc,Rd=0.00 (sic. >100)

- Verifica a compressione (4.2.4.1.2.2) - CC 56 SLU Xl=0.04 - Classe 1
  Sollecitazioni: N=-6.52 T_y=2.67
  Verifica a compressione [4.2.9]
  N,Ed=-6.52 Nc,Rd=-43021.20 N,Ed/Nc,Rd=0.00 (sic. >100)

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=-13.99 Mz,Ed=0.16 L=0.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  λ_y=6.97 Ncr,y=7011060.00 λ^*_y=0.08 Curva a: Φ_y=0.49 χ_y=1.00
  λ_z=24.19 Ncr,z=581859.00 λ^*_z=0.28 Curva b: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.00=0.00 (sic. >100)
  Verifica ZZ: 0.00+0.00=0.00 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 208
  $f_{z,L}$=0.00 (L/6856) $f_{z,G}$=0.00 (L/333448) (sic.=22.853)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 208
  $f_{z,L}$=0.00 (L/6713) $f_{z,G}$=0.00 (L/74099) (sic.=26.852)
MEMBRATURA Asta 1 Nodi 1 101 -15 201 - Sez. 4 (Colonne principali) - Crit. 4

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 110 SLU - Classe 1
  Sollecitazioni: N,Ed=-3929.80 My,Ed=1443.16 Mz,Ed=1263.84 L=4.76
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=9.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=25643.10 λ_{LT}=0.83
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.83 β_{LT}=0.75 f=0.97 χ_{LT}=0.82
  λ_y=111.46 Ncr,y=130268.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.43
  λ_z=187.95 Ncr,z=45814.90 λ^*_z=2.16 Curva c: Φ_z=3.32 χ_z=0.17
  Kyy, Kyz, Kzy, Kzz=0.98, 0.66, 0.59, 1.10
  Verifica YY: 0.04+0.10+0.10=0.25 (sic.=3.997)
  Verifica ZZ: 0.11+0.06+0.17=0.35 (sic.=2.883)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 160
  Δ=0.31 (L/1517) (sic.=5.057)
MEMBRATURA Asta 3 Nodi 103 3 -20 203 - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 94 SLU - Classe 1
  Sollecitazioni: N,Ed=-103.16 My,Ed=71.85 Mz,Ed=0.52 L=3.76
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
  $\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
  λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
  λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
  Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.57, 0.97
  Verifica YY: 0.00+0.03+0.00=0.03 (sic.=30.125)
  Verifica ZZ: 0.01+0.02+0.00=0.03 (sic.=31.705)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 160
  Δ=0.34 (L/1115) (sic.=3.717)
MEMBRATURA Asta 4 Nodi 104 4 -21 204 - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3

Sollecitazioni: N,Ed=-582.11 My,Ed=0.05 Mz,Ed=4.47 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=0.98
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.96 β_{LT}=0.75 f=0.97 χ_{LT}=0.73
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.95, 0.99, 0.76, 0.99
Verifica YY: 0.01+0.00+0.01=0.02 (sic.=43.606)
Verifica ZZ: 0.07+0.00+0.01=0.08 (sic.=12.381)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 160
Δ=0.32 (L/1193) (sic.=3.977)

MEMBRATURA Asta 5 Nodi 5 105 43 205 - Sez. 4 (Colonne principali) - Crit. 4

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4057.09 My,Ed=970.49 Mz,Ed=1035.79 L=4.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=9.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=25643.10 λ_{LT}=0.78
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.79 β_{LT}=0.75 f=0.97 χ_{LT}=0.85
λ_y=111.46 Ncr,y=130268.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.43
λ_z=187.95 Ncr,z=45814.90 λ^*_z=2.16 Curva c: Φ_z=3.32 χ_z=0.17
Kyy, Kyz, Kzy, Kzz=0.98, 1.02, 0.78, 1.02
Verifica YY: 0.05+0.07+0.20=0.32 (sic.=3.118)
Verifica ZZ: 0.12+0.06+0.20=0.38 (sic.=2.658)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 193
Δ=0.47 (L/1014) (sic.=3.380)

MEMBRATURA Asta 6 Nodi 106 6 206 - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-624.99 My,Ed=0.01 Mz,Ed=0.96 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=0.98
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.96 β_{LT}=0.75 f=0.97 χ_{LT}=0.73
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.96, 0.99, 0.76, 0.99
Verifica YY: 0.01+0.00=0.02 (sic.=62.918)
Verifica ZZ: 0.08+0.00=0.08 (sic.=12.821)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 193
Δ=0.36 (L/1052) (sic.=3.507)

MEMBRATURA Asta 10 Nodi 10 110 210 - Sez. 4 (Colonne principali) - Crit. 4

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-3890.58 My,Ed=1229.96 Mz,Ed=1048.72 L=4.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=9.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=25643.10 λ_{LT}=0.78
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.79 β_{LT}=0.75 f=0.97 χ_{LT}=0.85
λ_y=111.46 Ncr,y=130268.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.43
λ_z=187.95 Ncr,z=45814.90 λ^*_z=2.16 Curva c: Φ_z=3.32 χ_z=0.17
Kyy, Kyz, Kzy, Kzz=0.97, 1.01, 0.78, 1.01
Verifica YY: 0.04+0.09+0.20=0.34 (sic.=2.936)
Verifica ZZ: 0.11+0.08+0.20=0.39 (sic.=2.569)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 193
Δ=0.55 (L/861) (sic.=2.870)

MEMBRATURA Asta 11 Nodi 111 11 -22 211 - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-600.55 My,Ed=0.05 Mz,Ed=4.67 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=0.98
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.96 β_{LT}=0.75 f=0.97 χ_{LT}=0.73
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.95, 0.99, 0.76, 0.99
Verifica YY: 0.01+0.00+0.01=0.02 (sic.=41.996)
Verifica ZZ: 0.07+0.00+0.01=0.08 (sic.=11.978)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 193
Δ=0.45 (L/828) (sic.=2.760)

MEMBRATURA Asta 12 Nodi 112 12 -23 212 - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 115 SLU - Classe 1
Sollecitazioni: N,Ed=-272.78 My,Ed=37.30 Mz,Ed=0.80 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95

L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
λ_y=57.16 Ncr,y=127444.00 λ^*_y=0.66 Curva a: Φ_y=0.76 χ_y=0.87
λ_z=203.91 Ncr,z=10015.20 λ^*_z=2.35 Curva b: Φ_z=3.62 χ_z=0.16
Kyy, Kyz, Kzy, Kzz=0.95, 0.60, 0.57, 0.99
Verifica YY: 0.01+0.02+0.00=0.02 (sic.=44.360)
Verifica ZZ: 0.03+0.01+0.00=0.04 (sic.=22.845)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 193
Δ=0.47 (L/799) (sic.=2.663)

MEMBRATURA Asta 15 Nodi 15 115 215 - Sez. 4 (Colonne principali) - Crit. 4

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 110 SLU - Classe 1
Sollecitazioni: N,Ed=-4313.74 My,Ed=1584.77 Mz,Ed=1316.42 L=4.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=9.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=25643.10 λ_{LT}=0.83
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.83 β_{LT}=0.75 f=0.97 χ_{LT}=0.82
λ_y=111.46 Ncr,y=130268.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.43
λ_z=187.95 Ncr,z=45814.90 λ^*_z=2.16 Curva c: Φ_z=3.32 χ_z=0.17
Kyy, Kyz, Kzy, Kzz=0.99, 0.67, 0.59, 1.11
Verifica YY: 0.05+0.11+0.11=0.27 (sic.=3.695)
Verifica ZZ: 0.12+0.07+0.18=0.37 (sic.=2.676)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 193
Δ=0.41 (L/1154) (sic.=3.847)

MEMBRATURA Asta 18 Nodi 118 18 218 - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
Sollecitazioni: N,Ed=606.41 My,Ed=10.79 Mz,Ed=63.67 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=0.98
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.96 β_{LT}=0.75 f=0.97 χ_{LT}=0.73
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.00+0.14=0.16 (sic.=6.450)
Verifica ZZ: 0.01+0.00+0.14=0.15 (sic.=6.491)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 198
Δ=0.33 (L/1155) (sic.=3.850)

MEMBRATURA Asta 23 Nodi 123 23 223 - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=600.17 My,Ed=14.87 Mz,Ed=65.88 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=0.98
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.96 β_{LT}=0.75 f=0.97 χ_{LT}=0.73
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.01+0.14=0.16 (sic.=6.188)
Verifica ZZ: 0.01+0.01+0.14=0.16 (sic.=6.240)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 198
Δ=0.35 (L/1084) (sic.=3.613)

MEMBRATURA Asta 25 Nodi 25 125 -14 -16 225 - Sez. 4 (Colonne principali) - Crit. 4

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-3317.66 My,Ed=569.29 Mz,Ed=933.79 L=4.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=9.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=25643.10 λ_{LT}=0.78
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.79 β_{LT}=0.75 f=0.97 χ_{LT}=0.85
λ_y=111.46 Ncr,y=130268.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.43
λ_z=187.95 Ncr,z=45814.90 λ^*_z=2.16 Curva c: Φ_z=3.32 χ_z=0.17
Kyy, Kyz, Kzy, Kzz=0.97, 1.00, 0.78, 1.00
Verifica YY: 0.04+0.04+0.18=0.26 (sic.=3.854)
Verifica ZZ: 0.09+0.03+0.18=0.31 (sic.=3.243)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 198
Δ=0.34 (L/1398) (sic.=4.660)

MEMBRATURA Asta 27 Nodi 127 27 -17 - Sez. 6 (Montanti principali_facciata) - Crit. 6

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 188
Δ=0.13 (L/748) (sic.=2.493)

MEMBRATURA Asta 28 Nodi 128 28 228 - Sez. 12 (Montanti secondari) - Crit. 10

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 114 SLU - Classe 1
Sollecitazioni: N,Ed=82.86 My,Ed=71.67 Mz,Ed=8.60 L=3.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.76 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3111.37 λ_{LT}=1.05
$\lambda_{LT,0}$=0.40 Φ_{LT}=1.02 β_{LT}=0.75 f=0.97 χ_{LT}=0.69
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95

Verifica YY: 0.00+0.03+0.01=0.04 (sic.=25.571)
Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=31.517)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 193
Δ=0.33 (L/1155) (sic.=3.850)

MEMBRATURA Asta 29 Nodi 29 129 -18 229 - Sez. 4 (Colonne principali) - Crit. 4

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-4727.95 My,Ed=891.59 Mz,Ed=1401.76 L=4.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=9.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=25643.10 λ_{LT}=0.78
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.79 β_{LT}=0.75 f=0.97 χ_{LT}=0.85
λ_y=111.46 Ncr,y=130268.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.43
λ_z=187.95 Ncr,z=45814.90 λ^*_z=2.16 Curva c: Φ_z=3.32 χ_z=0.17
Kyy, Kyz, Kzy, Kzz=0.98, 1.03, 0.78, 1.03
Verifica YY: 0.05+0.07+0.27=0.40 (sic.=2.524)
Verifica ZZ: 0.14+0.05+0.27=0.46 (sic.=2.153)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 188
Δ=0.47 (L/1012) (sic.=3.373)

MEMBRATURA Asta 42 Nodi 42 142 -19 242 - Sez. 4 (Colonne principali) - Crit. 4

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 90 SLU - Classe 1
Sollecitazioni: N,Ed=-4929.29 My,Ed=1575.63 Mz,Ed=1305.59 L=4.76
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=9.52 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=25643.10 λ_{LT}=0.83
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.83 β_{LT}=0.75 f=0.97 χ_{LT}=0.82
λ_y=111.46 Ncr,y=130268.00 λ^*_y=1.28 Curva b: Φ_y=1.51 χ_y=0.43
λ_z=187.95 Ncr,z=45814.90 λ^*_z=2.16 Curva c: Φ_z=3.32 χ_z=0.17
Kyy, Kyz, Kzy, Kzz=0.99, 0.68, 0.60, 1.14
Verifica YY: 0.06+0.11+0.11=0.28 (sic.=3.585)
Verifica ZZ: 0.14+0.07+0.19=0.39 (sic.=2.541)

- Verifica spostamento relativo membratura (4.2.4.2.2) - CC 188
Δ=0.40 (L/1189) (sic.=3.963)

MEMBRATURA Asta 1001 Nodi 101 102 103 104 105 - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-295.49 My,Ed=1160.26 Mz,Ed=308.26 L=3.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.08 M,cr=80924.70 λ_{LT}=0.32
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=20.14 Ncr,y=2312440.00 λ^*_y=0.23 Curva b: Φ_y=0.53 χ_y=0.99
λ_z=33.18 Ncr,z=851711.00 λ^*_z=0.38 Curva c: Φ_z=0.62 χ_z=0.91
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.14+0.11=0.25 (sic.=3.924)
Verifica ZZ: 0.00+0.11+0.11=0.23 (sic.=4.418)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 184
$f_{z,L}$=0.02 (L/14368) (sic.=47.893)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 184
$f_{z,L}$=0.02 (L/12762) (sic.=51.048)

MEMBRATURA Asta 1001 Nodi 105 106 107 108 109 110 - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-115.55 My,Ed=937.48 Mz,Ed=80.16 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.04 M,cr=58810.50 λ_{LT}=0.37
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=23.50 Ncr,y=1698930.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.97
λ_z=38.72 Ncr,z=625747.00 λ^*_z=0.45 Curva c: Φ_z=0.66 χ_z=0.87
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.12+0.03=0.15 (sic.=6.890)
Verifica ZZ: 0.00+0.09+0.03=0.12 (sic.=8.190)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 183
$f_{z,L}$=0.01 (L/39357) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
$f_{z,L}$=0.01 (L/24165) (sic.=96.660)

MEMBRATURA Asta 1001 Nodi 110 111 112 113 114 115 - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-280.14 My,Ed=1131.41 Mz,Ed=280.85 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95

L_{cr}=1.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.06 M,cr=60097.60 λ_{LT}=0.37
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=23.50 Ncr,y=1698930.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.97
λ_z=38.72 Ncr,z=625747.00 λ^*_z=0.45 Curva c: Φ_z=0.66 χ_z=0.87
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.14+0.10=0.24 (sic.=4.141)
Verifica ZZ: 0.00+0.11+0.10=0.21 (sic.=4.677)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 204
$f_{z,G}$=0.02 (L/15033) (sic.=50.110)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 204
$f_{z,G}$=0.03 (L/11109) (sic.=44.436)

MEMBRATURA Asta 1012 Nodi 125 127 128 129 - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=522.74 My,Ed=1138.73 Mz,Ed=300.64 L=3.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.86 M,cr=214788.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.14+0.11=0.25 (sic.=3.980)
Verifica ZZ: 0.00+0.11+0.11=0.22 (sic.=4.482)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 136
$f_{z,L}$=0.04 (L/8247) (sic.=27.490)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 136
$f_{z,L}$=0.04 (L/8434) (sic.=33.736)

MEMBRATURA Asta 1012 Nodi 129 130 135 - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
Sollecitazioni: N,Ed=-641.99 My,Ed=865.69 Mz,Ed=77.51 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.17 M,cr=66361.80 λ_{LT}=0.35
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=23.50 Ncr,y=1698930.00 λ^*_y=0.27 Curva b: Φ_y=0.55 χ_y=0.97
λ_z=38.72 Ncr,z=625747.00 λ^*_z=0.45 Curva c: Φ_z=0.66 χ_z=0.87
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.01+0.11+0.03=0.14 (sic.=7.142)
Verifica ZZ: 0.01+0.09+0.03=0.12 (sic.=8.385)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 184
$f_{z,G}$=0.02 (L/17628) (sic.=58.760)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 184
$f_{z,G}$=0.04 (L/9959) (sic.=39.836)

MEMBRATURA Asta 1013 Nodi 101 -1 117 -6 122 -11 125 - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
Sollecitazioni: N,Ed=-372.09 My,Ed=786.34 Mz,Ed=360.42 L=4.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.20 M,cr=45828.20 λ_{LT}=0.42
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.57 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_y=29.54 Ncr,y=1075000.00 λ^*_y=0.34 Curva b: Φ_y=0.58 χ_y=0.95
λ_z=48.67 Ncr,z=395940.00 λ^*_z=0.56 Curva c: Φ_z=0.75 χ_z=0.81
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.10+0.13=0.23 (sic.=4.387)
Verifica ZZ: 0.00+0.08+0.13=0.21 (sic.=4.783)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 190
$f_{z,L}$=0.06 (L/7102) (sic.=23.673)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 210
$f_{z,G}$=0.09 (L/4833) (sic.=19.332)

MEMBRATURA Asta 1017 Nodi 105 -2 -4 -7 -9 -12 129 - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 58 SLU - Classe 1
Sollecitazioni: N,Ed=-2340.04 My,Ed=2977.85 Mz,Ed=21.90 L=4.40
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.08 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.19 M,cr=5884.72 λ_{LT}=1.02
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.99 β_{LT}=0.75 f=0.97 χ_{LT}=0.71
λ_y=37.29 Ncr,y=424562.00 λ^*_y=0.43 Curva a: Φ_y=0.62 χ_y=0.94
λ_z=137.77 Ncr,z=31105.20 λ^*_z=1.59 Curva b: Φ_z=1.99 χ_z=0.31
Kyy, Kyz, Kzy, Kzz=0.96, 0.65, 0.57, 1.08
Verifica YY: 0.03+0.69+0.01=0.74 (sic.=1.353)
Verifica ZZ: 0.10+0.42+0.02=0.54 (sic.=1.863)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 162
  $f_{z,G}$=0.29 (L/1519) (sic.=5.063)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 162
  $f_{z,G}$=0.34 (L/1279) (sic.=5.116)

MEMBRATURA Asta 1022 Nodi 110 -3 -5 -8 -10 -13 135 - Sez. 10 (Travi secondarie_sottostruttura) - Crit. 8

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 58 SLU - Classe 1
  Sollecitazioni: N,Ed=-2518.60 My,Ed=3071.69 Mz,Ed=25.97 L=4.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.08 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.16 M,cr=5699.83 λ_{LT}=1.03
  $\lambda_{LT,0}$=0.40 Φ_{LT}=1.01 β_{LT}=0.75 f=0.97 χ_{LT}=0.70
  λ_y=37.29 Ncr,y=424562.00 λ^*_y=0.43 Curva a: Φ_y=0.62 χ_y=0.94
  λ_z=137.77 Ncr,z=31105.20 λ^*_z=1.59 Curva b: Φ_z=1.99 χ_z=0.31
  Kyy, Kyz, Kzy, Kzz=0.96, 0.66, 0.57, 1.09
  Verifica YY: 0.04+0.73+0.01=0.78 (sic.=1.287)
  Verifica ZZ: 0.11+0.44+0.02=0.57 (sic.=1.759)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 190
  $f_{z,G}$=0.33 (L/1348) (sic.=4.493)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 190
  $f_{z,L}$=0.39 (L/1134) (sic.=4.536)

MEMBRATURA Asta 1026 Nodi 115 116 118 144 123 124 142 - Sez. 1 (Travi principali_sottostruttura) - Crit. 1

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-454.27 My,Ed=2183.96 Mz,Ed=123.75 L=4.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.10 M,cr=41952.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_y=29.54 Ncr,y=1075000.00 λ^*_y=0.34 Curva b: Φ_y=0.58 χ_y=0.95
  λ_z=48.67 Ncr,z=395940.00 λ^*_z=0.56 Curva c: Φ_z=0.75 χ_z=0.81
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.27+0.04=0.32 (sic.=3.146)
  Verifica ZZ: 0.00+0.22+0.04=0.26 (sic.=3.780)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 190
  $f_{z,L}$=0.06 (L/7347) (sic.=24.490)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 190
  $f_{z,L}$=0.09 (L/4851) (sic.=19.404)

MEMBRATURA Asta 2001 Nodi 201 202 -24 203 204 205 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 1 SND - Classe 3
  Sollecitazioni: N,Ed=108.93 My,Ed=886.78 Mz,Ed=242.32 L=3.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.02 M,cr=195600.00 λ_{LT}=0.28
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.06+0.04=0.10 (sic.=9.913)
  Verifica ZZ: 0.00+0.05+0.04=0.09 (sic.=11.163)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 184
  $f_{z,L}$=0.01 (L/28728) (sic.=95.760)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 184
  $f_{z,L}$=0.01 (L/21546) (sic.=86.184)

MEMBRATURA Asta 2001 Nodi 205 206 207 208 209 210 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=694.84 My,Ed=388.44 Mz,Ed=331.60 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.09 M,cr=159226.00 λ_{LT}=0.31
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.52 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.02+0.06=0.09 (sic.=11.342)
  Verifica ZZ: 0.00+0.02+0.06=0.08 (sic.=12.016)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 204
  $f_{z,L}$=0.01 (L/46456) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 204
  $f_{z,L}$=0.01 (L/29012) (sic. >100)

MEMBRATURA Asta 2001 Nodi 210 211 212 -25 213 -26 214 215 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-563.32 My,Ed=461.73 Mz,Ed=621.10 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.75 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.58 M,cr=379260.00 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=20.49 Ncr,y=3855090.00 λ^*_y=0.24 Curva b: Φ_y=0.53 χ_y=0.99
  λ_z=34.55 Ncr,z=1355830.00 λ^*_z=0.40 Curva c: Φ_z=0.63 χ_z=0.90
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.03+0.11=0.14 (sic.=6.909)
  Verifica ZZ: 0.00+0.02+0.11=0.14 (sic.=7.187)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 204
  $f_{Z,L}$=0.02 (L/23302) (sic.=77.673)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 204
  $f_{Z,L}$=0.02 (L/15584) (sic.=62.336)

MEMBRATURA Asta 2012 Nodi 225 226 228 229 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 9 SND - Classe 3
  Sollecitazioni: N,Ed=240.96 My,Ed=1263.81 Mz,Ed=202.71 L=3.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=2.72 M,cr=523449.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.08+0.04=0.12 (sic.=8.449)
  Verifica ZZ: 0.00+0.06+0.04=0.10 (sic.=9.779)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 203
  $f_{Z,L}$=0.01 (L/43092) (sic. >100)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 183
  $f_{Z,G}$=0.02 (L/18837) (sic.=75.348)

MEMBRATURA Asta 2012 Nodi 229 230 231 232 233 234 236 237 238 239 240 241 242 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-808.40 My,Ed=1086.45 Mz,Ed=631.63 L=7.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.19 M,cr=58631.30 λ_{LT}=0.52
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.62 β_{LT}=0.75 f=0.97 χ_{LT}=0.98
  λ_y=40.98 Ncr,y=963773.00 λ^*_y=0.47 Curva b: Φ_y=0.66 χ_y=0.90
  λ_z=69.10 Ncr,z=338957.00 λ^*_z=0.80 Curva c: Φ_z=0.96 χ_z=0.66
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.07+0.11=0.19 (sic.=5.265)
  Verifica ZZ: 0.01+0.06+0.11=0.18 (sic.=5.640)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
  $f_{Z,L}$=0.06 (L/12399) (sic.=41.330)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
  $f_{Z,L}$=0.26 (L/2648) (sic.=10.592)

MEMBRATURA Asta 2013 Nodi 201 220 225 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=726.60 My,Ed=775.64 Mz,Ed=171.59 L=4.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.09 M,cr=108527.00 λ_{LT}=0.38
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.05+0.03=0.08 (sic.=11.903)
  Verifica ZZ: 0.00+0.04+0.03=0.07 (sic.=13.489)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 210
  $f_{Z,G}$=0.04 (L/9986) (sic.=33.287)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 210
  $f_{Z,G}$=0.07 (L/6711) (sic.=26.844)

MEMBRATURA Asta 2026 Nodi 215 216 218 221 223 224 242 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=789.20 My,Ed=1136.28 Mz,Ed=273.58 L=4.40
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.20 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.07 M,cr=107115.00 λ_{LT}=0.38
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.07+0.05=0.13 (sic.=7.952)
  Verifica ZZ: 0.00+0.06+0.05=0.11 (sic.=8.986)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 190
  $f_{Z,G}$=0.05 (L/9038) (sic.=30.127)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 190
  $f_{z,G}$=0.07 (L/5972) (sic.=23.888)

MEMBRATURA Asta 3002 Nodi -35 -36 -37 - Sez. 7 (Profili per pannelli_copertura) - Crit. 7

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 211
  $f_{z,L}$=0.04 (L/3143) $f_{z,G}$=0.04 (L/3379) (sic.=10.477)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 211
  $f_{z,L}$=0.06 (L/2234) $f_{z,G}$=0.06 (L/2494) (sic.=8.936)

MEMBRATURA Asta 3004 Nodi -38 -39 -40 -41 -42 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-291.71 My,Ed=117.30 Mz,Ed=16.01 L=3.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=9722.42 λ_{LT}=0.58
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_Y=61.33 Ncr,y=139595.00 λ^*_y=0.71 Curva b: Φ_y=0.84 χ_y=0.78
  λ_z=99.38 Ncr,z=53173.30 λ^*_z=1.14 Curva c: Φ_z=1.39 χ_z=0.46
  Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.57, 0.96
  Verifica YY: 0.01+0.04+0.01=0.05 (sic.=20.397)
  Verifica ZZ: 0.01+0.02+0.01=0.04 (sic.=23.831)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 186
  $f_{z,L}$=0.04 (L/7265) $f_{z,G}$=0.03 (L/9861) (sic.=24.217)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 186
  $f_{z,L}$=0.07 (L/4369) $f_{z,G}$=0.06 (L/5327) (sic.=17.476)

MEMBRATURA Asta 3004 Nodi -42 -43 -44 -45 -46 -47 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
  Sollecitazioni: N,Ed=342.62 My,Ed=180.73 Mz,Ed=22.53 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=8044.65 λ_{LT}=0.64
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.69 β_{LT}=0.75 f=0.97 χ_{LT}=0.92
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.06+0.01=0.07 (sic.=13.800)
  Verifica ZZ: 0.01+0.04+0.01=0.05 (sic.=18.386)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 191
  $f_{z,L}$=0.08 (L/4255) $f_{z,G}$=0.07 (L/5038) (sic.=14.183)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 191
  $f_{z,L}$=0.14 (L/2485) $f_{z,G}$=0.12 (L/2953) (sic.=9.940)

MEMBRATURA Asta 3004 Nodi -47 -48 -49 -50 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-505.99 My,Ed=62.40 Mz,Ed=35.81 L=3.50
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=8044.65 λ_{LT}=0.60
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.67 β_{LT}=0.75 f=0.97 χ_{LT}=0.94
  λ_Y=71.56 Ncr,y=102559.00 λ^*_y=0.82 Curva b: Φ_y=0.95 χ_y=0.71
  λ_z=115.94 Ncr,z=39066.10 λ^*_z=1.34 Curva c: Φ_z=1.67 χ_z=0.37
  Kyy, Kyz, Kzy, Kzz=0.96, 0.96, 0.76, 0.96
  Verifica YY: 0.01+0.02+0.03=0.07 (sic.=14.786)
  Verifica ZZ: 0.02+0.02+0.03=0.07 (sic.=13.752)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
  $f_{z,G}$=0.03 (L/11469) $f_{z,L}$=0.03 (L/13443) (sic.=38.230)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
  $f_{z,G}$=0.09 (L/3974) $f_{z,L}$=0.08 (L/4223) (sic.=15.896)

MEMBRATURA Asta 3006 Nodi -55 -56 -57 -58 -59 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
  Sollecitazioni: N,Ed=-19.09 My,Ed=115.45 Mz,Ed=10.46 L=3.00
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=9722.42 λ_{LT}=0.58
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
  λ_Y=61.33 Ncr,y=139595.00 λ^*_y=0.71 Curva b: Φ_y=0.84 χ_y=0.78
  λ_z=99.38 Ncr,z=53173.30 λ^*_z=1.14 Curva c: Φ_z=1.39 χ_z=0.46
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.04+0.00=0.04 (sic.=24.423)
  Verifica ZZ: 0.00+0.02+0.01=0.03 (sic.=34.374)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 186
  $f_{z,L}$=0.04 (L/7077) $f_{z,G}$=0.03 (L/9561) (sic.=23.590)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 186

$f_{Z,L}$=0.07 (L/4409) $f_{Z,G}$=0.06 (L/5405) (sic.=17.636)
MEMBRATURA Asta 3006 Nodi -59 -60 -61 -62 -63 -64 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 112 SLU - Classe 1
Sollecitazioni: N,Ed=-58.15 My,Ed=113.42 Mz,Ed=18.79 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=8044.65 λ_{LT}=0.64
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.69 β_{LT}=0.75 f=0.97 χ_{LT}=0.92
λ_y=71.56 Ncr,y=102559.00 λ^*_y=0.82 Curva b: Φ_y=0.95 χ_y=0.71
λ_z=115.94 Ncr,z=39066.10 λ^*_z=1.34 Curva c: Φ_z=1.67 χ_z=0.37
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.04+0.01=0.05 (sic.=22.078)
Verifica ZZ: 0.00+0.02+0.01=0.04 (sic.=27.623)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 191
$f_{Z,L}$=0.05 (L/7282) $f_{Z,G}$=0.04 (L/7850) (sic.=24.273)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 191
$f_{Z,L}$=0.10 (L/3428) $f_{Z,G}$=0.09 (L/3906) (sic.=13.712)
MEMBRATURA Asta 3006 Nodi -64 -65 -66 -67 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 102 SLU - Classe 1
Sollecitazioni: N,Ed=0.27 My,Ed=38.89 Mz,Ed=12.57 L=2.10
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.10 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=15635.30 λ_{LT}=0.46
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.59 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.00=0.02 (sic.=60.960)
Verifica ZZ: 0.00+0.01+0.01=0.01 (sic.=67.584)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 211
$f_{Z,L}$=0.02 (L/10009) $f_{Z,G}$=0.01 (L/33877) (sic.=33.363)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 211
$f_{Z,L}$=0.03 (L/7232) $f_{Z,G}$=0.01 (L/17407) (sic.=28.928)
MEMBRATURA Asta 3007 Nodi -72 -73 -74 -75 -76 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 1
Sollecitazioni: N,Ed=71.37 My,Ed=133.40 Mz,Ed=24.38 L=3.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=9722.42 λ_{LT}=0.58
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.66 β_{LT}=0.75 f=0.97 χ_{LT}=0.95
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.04+0.01=0.05 (sic.=19.057)
Verifica ZZ: 0.00+0.03+0.01=0.04 (sic.=24.089)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 181
$f_{Z,L}$=0.05 (L/6446) (sic.=21.487)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 176
$f_{Z,L}$=0.07 (L/4220) $f_{Z,G}$=0.07 (L/4289) (sic.=16.880)
MEMBRATURA Asta 3007 Nodi -76 -77 -78 -79 -80 -81 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 82 SLU - Classe 1
Sollecitazioni: N,Ed=-100.41 My,Ed=120.60 Mz,Ed=4.95 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=8044.65 λ_{LT}=0.64
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.69 β_{LT}=0.75 f=0.97 χ_{LT}=0.92
λ_y=71.56 Ncr,y=102559.00 λ^*_y=0.82 Curva b: Φ_y=0.95 χ_y=0.71
λ_z=115.94 Ncr,z=39066.10 λ^*_z=1.34 Curva c: Φ_z=1.67 χ_z=0.37
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.96
Verifica YY: 0.00+0.04+0.00=0.04 (sic.=23.019)
Verifica ZZ: 0.00+0.02+0.00=0.03 (sic.=32.475)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
$f_{Z,L}$=0.05 (L/7119) $f_{Z,G}$=0.04 (L/7842) (sic.=23.730)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
$f_{Z,L}$=0.11 (L/3143) $f_{Z,G}$=0.09 (L/3985) (sic.=12.572)
MEMBRATURA Asta 3007 Nodi -81 -82 -83 -84 -85 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 77 SLU - Classe 1
Sollecitazioni: N,Ed=95.12 My,Ed=191.80 Mz,Ed=38.27 L=3.50
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=3.50 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=8044.65 λ_{LT}=0.64
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.69 β_{LT}=0.75 f=0.97 χ_{LT}=0.92
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.06+0.01=0.08 (sic.=12.784)
Verifica ZZ: 0.00+0.04+0.02=0.06 (sic.=15.982)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 201
  $f_{z,G}$=0.08 (L/4267) $f_{z,L}$=0.08 (L/4366) (sic.=14.223)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
  $f_{z,G}$=0.14 (L/2517) $f_{z,L}$=0.13 (L/2639) (sic.=10.068)

MEMBRATURA Asta 3013 Nodi 201 -38 -55 -72 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-862.88 My,Ed=428.31 Mz,Ed=225.72 L=2.31
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.98 M,cr=614820.00 λ_{LT}=0.16
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=13.52 Ncr,y=8860200.00 λ^*_y=0.16 Curva b: Φ_y=0.50 χ_y=1.00
  λ_z=22.79 Ncr,z=3116120.00 λ^*_z=0.26 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.03+0.04=0.07 (sic.=13.812)
  Verifica ZZ: 0.00+0.02+0.04=0.07 (sic.=14.907)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
  $f_{z,L}$=0.01 (L/19843) $f_{z,G}$=0.01 (L/25753) (sic.=66.143)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
  $f_{z,L}$=0.02 (L/13193) $f_{z,G}$=0.01 (L/18622) (sic.=52.772)

MEMBRATURA Asta 3015 Nodi -24 -27 -40 -57 - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 87 SLU - Classe 1
  Sollecitazioni: N,Ed=-114.30 My,Ed=12.79 Mz,Ed=2.36 L=1.73
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.73 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3291.04 λ_{LT}=0.71
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.74 β_{LT}=0.75 f=0.97 χ_{LT}=0.89
  λ_y=35.30 Ncr,y=219669.00 λ^*_y=0.41 Curva a: Φ_y=0.60 χ_y=0.95
  λ_z=119.64 Ncr,z=19127.20 λ^*_z=1.38 Curva b: Φ_z=1.65 χ_z=0.39
  Kyy, Kyz, Kzy, Kzz=0.95, 0.58, 0.57, 0.96
  Verifica YY: 0.00+0.01+0.00=0.02 (sic.=63.050)
  Verifica ZZ: 0.01+0.01+0.01=0.02 (sic.=50.127)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 186
  $f_{z,L}$=0.03 (L/5953) $f_{z,G}$=0.01 (L/11714) (sic.=19.843)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 186
  $f_{z,L}$=0.05 (L/3515) $f_{z,G}$=0.03 (L/6737) (sic.=14.060)

MEMBRATURA Asta 3016 Nodi 204 -28 -41 - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
  Sollecitazioni: N,Ed=-110.20 My,Ed=20.93 Mz,Ed=0.67 L=1.15
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=5873.77 λ_{LT}=0.53
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.63 β_{LT}=0.75 f=0.97 χ_{LT}=0.97
  λ_y=23.54 Ncr,y=494255.00 λ^*_y=0.27 Curva a: Φ_y=0.54 χ_y=0.98
  λ_z=79.76 Ncr,z=43036.10 λ^*_z=0.92 Curva b: Φ_z=1.04 χ_z=0.65
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.96
  Verifica YY: 0.00+0.01+0.00=0.02 (sic.=58.281)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=69.371)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.02 (L/5251) $f_{z,G}$=0.01 (L/9420) (sic.=17.503)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.03 (L/3358) $f_{z,G}$=0.01 (L/9801) (sic.=13.432)

MEMBRATURA Asta 3017 Nodi 205 -29 -42 -59 -76 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
  Sollecitazioni: N,Ed=-692.01 My,Ed=682.88 Mz,Ed=337.22 L=2.31
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.71 M,cr=530223.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=13.52 Ncr,y=8860200.00 λ^*_y=0.16 Curva b: Φ_y=0.50 χ_y=1.00
  λ_z=22.79 Ncr,z=3116120.00 λ^*_z=0.26 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.04+0.06=0.11 (sic.=9.262)
  Verifica ZZ: 0.00+0.03+0.06=0.10 (sic.=10.062)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
  $f_{z,L}$=0.01 (L/16811) (sic.=56.037)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 188
  $f_{z,L}$=0.02 (L/13193) $f_{z,G}$=0.02 (L/15370) (sic.=52.772)

MEMBRATURA Asta 3018 Nodi 206 -30 -43 - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 107 SLU - Classe 1
  Sollecitazioni: N,Ed=-82.46 My,Ed=19.44 Mz,Ed=0.61 L=1.15
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=5873.77 λ_{LT}=0.53
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.63 β_{LT}=0.75 f=0.97 χ_{LT}=0.97
  λ_y=23.54 Ncr,y=494255.00 λ^*_y=0.27 Curva a: Φ_y=0.54 χ_y=0.98
  λ_z=79.76 Ncr,z=43036.10 λ^*_z=0.92 Curva b: Φ_z=1.04 χ_z=0.65
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.02 (sic.=65.251)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=80.241)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.03 (L/3391) $f_{z,G}$=0.01 (L/10807) (sic.=11.303)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.06 (L/2033) $f_{z,G}$=0.01 (L/11695) (sic.=8.132)

MEMBRATURA Asta 3019 Nodi 207 -31 -44 - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 97 SLU - Classe 1
  Sollecitazioni: N,Ed=-28.33 My,Ed=19.63 Mz,Ed=0.60 L=1.15
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=5873.77 λ_{LT}=0.53
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.63 β_{LT}=0.75 f=0.97 χ_{LT}=0.97
  λ_y=23.54 Ncr,y=494255.00 λ^*_y=0.27 Curva a: Φ_y=0.54 χ_y=0.98
  λ_z=79.76 Ncr,z=43036.10 λ^*_z=0.92 Curva b: Φ_z=1.04 χ_z=0.65
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=72.294)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=99.128)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.05 (L/2150) $f_{z,G}$=0.02 (L/7058) (sic.=7.167)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.09 (L/1296) $f_{z,G}$=0.01 (L/7809) (sic.=5.184)

MEMBRATURA Asta 3020 Nodi 208 -32 -45 - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 97 SLU - Classe 1
  Sollecitazioni: N,Ed=-29.04 My,Ed=19.60 Mz,Ed=0.50 L=1.15
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=5873.77 λ_{LT}=0.53
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.63 β_{LT}=0.75 f=0.97 χ_{LT}=0.97
  λ_y=23.54 Ncr,y=494255.00 λ^*_y=0.27 Curva a: Φ_y=0.54 χ_y=0.98
  λ_z=79.76 Ncr,z=43036.10 λ^*_z=0.92 Curva b: Φ_z=1.04 χ_z=0.65
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=73.092)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic. >100)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.06 (L/2092) $f_{z,G}$=0.02 (L/7495) (sic.=6.973)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.10 (L/1210) $f_{z,G}$=0.01 (L/8867) (sic.=4.840)

MEMBRATURA Asta 3021 Nodi 209 -33 -46 - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
  Sollecitazioni: N,Ed=-87.83 My,Ed=19.50 Mz,Ed=0.11 L=1.15
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=5873.77 λ_{LT}=0.53
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.63 β_{LT}=0.75 f=0.97 χ_{LT}=0.97
  λ_y=23.54 Ncr,y=494255.00 λ^*_y=0.27 Curva a: Φ_y=0.54 χ_y=0.98
  λ_z=79.76 Ncr,z=43036.10 λ^*_z=0.92 Curva b: Φ_z=1.04 χ_z=0.65
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.00=0.01 (sic.=67.972)
  Verifica ZZ: 0.00+0.01+0.00=0.01 (sic.=87.911)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.04 (L/3037) $f_{z,G}$=0.01 (L/15130) (sic.=10.123)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 206
  $f_{z,L}$=0.08 (L/1536) $f_{z,G}$=0.01 (L/21051) (sic.=6.144)

MEMBRATURA Asta 3022 Nodi 210 -34 -47 -64 -81 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 94 SLU - Classe 1
  Sollecitazioni: N,Ed=-2333.14 My,Ed=561.80 Mz,Ed=90.88 L=2.31
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=543142.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_y=13.52 Ncr,y=8860200.00 λ^*_y=0.16 Curva b: Φ_y=0.50 χ_y=1.00

λ_z=22.79 Ncr,z=3116120.00 λ^*_z=0.26 Curva c: Φ_z=0.55 χ_z=0.97
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.01+0.03+0.01=0.05 (sic.=20.217)
Verifica ZZ: 0.01+0.02+0.01=0.04 (sic.=24.095)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 191
$f_{z,L}$=0.01 (L/18066) $f_{z,G}$=0.01 (L/42101) (sic.=60.220)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 201
$f_{z,L}$=0.04 (L/5785) $f_{z,G}$=0.01 (L/45249) (sic.=23.140)

MEMBRATURA Asta 3023 Nodi 211 -35 -48 - Sez. 8 (Travi terziarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 92 SLU - Classe 1
Sollecitazioni: N,Ed=-97.68 My,Ed=20.56 Mz,Ed=1.99 L=1.15
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=5873.77 λ_{LT}=0.53
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.63 β_{LT}=0.75 f=0.97 χ_{LT}=0.97
λ_y=23.54 Ncr,y=494255.00 λ^*_y=0.27 Curva a: Φ_y=0.54 χ_y=0.98
λ_z=79.76 Ncr,z=43036.10 λ^*_z=0.92 Curva b: Φ_z=1.04 χ_z=0.65
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.96
Verifica YY: 0.00+0.01+0.00=0.02 (sic.=53.545)
Verifica ZZ: 0.00+0.01+0.01=0.02 (sic.=57.983)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 211
$f_{z,L}$=0.02 (L/4822) $f_{z,G}$=0.01 (L/11054) (sic.=16.073)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 211
$f_{z,L}$=0.06 (L/1865) $f_{z,G}$=0.01 (L/17800) (sic.=7.460)

MEMBRATURA Asta 3025 Nodi -26 -37 -49 -67 -84 - Sez. 3 (Travi secondarie_copertura) - Crit. 3

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 100 SLU - Classe 1
Sollecitazioni: N,Ed=-63.82 My,Ed=20.70 Mz,Ed=27.31 L=2.31
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=2.31 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=13705.10 λ_{LT}=0.49
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.61 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_y=47.20 Ncr,y=235713.00 λ^*_y=0.54 Curva b: Φ_y=0.71 χ_y=0.86
λ_z=76.48 Ncr,z=89786.10 λ^*_z=0.88 Curva c: Φ_z=1.05 χ_z=0.61
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
Verifica YY: 0.00+0.01+0.01=0.02 (sic.=56.973)
Verifica ZZ: 0.00+0.00+0.02=0.02 (sic.=45.016)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 176
$f_{z,L}$=0.02 (L/9742) $f_{z,G}$=0.01 (L/20174) (sic.=32.473)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 188
$f_{z,L}$=0.07 (L/3243) $f_{z,G}$=0.03 (L/7809) (sic.=12.972)

MEMBRATURA Asta 3026 Nodi 215 -50 -85 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-992.40 My,Ed=1244.27 Mz,Ed=428.20 L=2.31
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.84 M,cr=571956.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=13.52 Ncr,y=8860200.00 λ^*_y=0.16 Curva b: Φ_y=0.50 χ_y=1.00
λ_z=22.79 Ncr,z=3116120.00 λ^*_z=0.26 Curva c: Φ_z=0.55 χ_z=0.97
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.08+0.08=0.16 (sic.=6.184)
Verifica ZZ: 0.01+0.06+0.08=0.15 (sic.=6.849)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
$f_{z,L}$=0.02 (L/11312) $f_{z,G}$=0.02 (L/14453) (sic.=37.707)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
$f_{z,L}$=0.03 (L/8435) $f_{z,G}$=0.02 (L/11528) (sic.=33.740)

MEMBRATURA Asta 3044 Nodi -72 -68 -51 225 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 5 SND - Classe 3
Sollecitazioni: N,Ed=-860.35 My,Ed=553.33 Mz,Ed=156.50 L=2.31
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.93 M,cr=597928.00 λ_{LT}=0.16
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_y=13.52 Ncr,y=8860200.00 λ^*_y=0.16 Curva b: Φ_y=0.50 χ_y=1.00
λ_z=22.79 Ncr,z=3116120.00 λ^*_z=0.26 Curva c: Φ_z=0.55 χ_z=0.97
Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
Verifica YY: 0.00+0.04+0.03=0.07 (sic.=14.747)
Verifica ZZ: 0.00+0.03+0.03=0.06 (sic.=16.421)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 170

$f_{Z,G}$=0.01 (L/28649) (sic.=95.497)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 170
  $f_{Z,G}$=0.01 (L/20258) (sic.=81.032)

MEMBRATURA Asta 3048 Nodi -76 -69 -52 229 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-709.72 My,Ed=682.40 Mz,Ed=386.46 L=2.31
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.71 M,cr=529838.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=13.52 Ncr,y=8860200.00 λ^*_y=0.16 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=22.79 Ncr,z=3116120.00 λ^*_z=0.26 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.00+0.04+0.07=0.12 (sic.=8.551)
  Verifica ZZ: 0.00+0.03+0.07=0.11 (sic.=9.228)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.01 (L/20429) (sic.=68.097)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 160
  $f_{Z,G}$=0.01 (L/21908) (sic.=87.632)

MEMBRATURA Asta 3053 Nodi -81 -70 -53 236 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 89 SLU - Classe 1
  Sollecitazioni: N,Ed=-2440.09 My,Ed=568.33 Mz,Ed=28.95 L=2.31
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=543141.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=13.52 Ncr,y=8860200.00 λ^*_y=0.16 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=22.79 Ncr,z=3116120.00 λ^*_z=0.26 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.01+0.03+0.00=0.05 (sic.=21.761)
  Verifica ZZ: 0.01+0.02+0.00=0.03 (sic.=28.629)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.07 (L/3503) $f_{Z,G}$=0.06 (L/3794) (sic.=11.677)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.15 (L/1563) $f_{Z,G}$=0.09 (L/2432) (sic.=6.252)

MEMBRATURA Asta 3057 Nodi -85 -71 -54 242 - Sez. 2 (Travi principali_copertura) - Crit. 2

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 13 SND - Classe 3
  Sollecitazioni: N,Ed=-1037.04 My,Ed=1204.62 Mz,Ed=464.68 L=2.31
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=1.15 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.85 M,cr=572901.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=13.52 Ncr,y=8860200.00 λ^*_y=0.16 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=22.79 Ncr,z=3116120.00 λ^*_z=0.26 Curva c: Φ_z=0.55 χ_z=0.97
  Kyy, Kyz, Kzy, Kzz=0.95, 0.95, 0.76, 0.95
  Verifica YY: 0.01+0.08+0.08=0.17 (sic.=6.023)
  Verifica ZZ: 0.01+0.06+0.08=0.15 (sic.=6.630)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 208
  $f_{Z,L}$=0.02 (L/15322) $f_{Z,G}$=0.01 (L/16468) (sic.=51.073)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 213
  $f_{Z,G}$=0.02 (L/12288) (sic.=49.152)

MEMBRATURA Asta 5043 Nodi -16 26 -17 28 - Sez. 5 (Traversi_facciata) - Crit. 5

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 115 SLU - Classe 1
  Sollecitazioni: N,Ed=-16.82 My,Ed=18.11 Mz,Ed=31.07 L=2.60
  αmy, αmz, αLT=0.95, 0.95, 0.95
  L_{cr}=2.60 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=3158.97 λ_{LT}=0.88
  $\lambda_{LT,0}$=0.40 Φ_{LT}=0.87 β_{LT}=0.75 f=0.97 χ_{LT}=0.80
  λ_Y=45.30 Ncr,y=165942.00 λ^*_y=0.52 Curva a: Φ_y=0.67 χ_y=0.92
  λ_Z=157.23 Ncr,z=13771.80 λ^*_z=1.81 Curva b: Φ_z=2.41 χ_z=0.25
  Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.95
  Verifica YY: 0.00+0.01+0.04=0.04 (sic.=22.266)
  Verifica ZZ: 0.00+0.01+0.06=0.07 (sic.=15.203)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.08 (L/3464) $f_{Z,G}$=0.01 (L/37092) (sic.=11.547)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 193
  $f_{Z,L}$=0.08 (L/3393) $f_{Z,G}$=0.01 (L/29634) (sic.=13.572)

MEMBRATURA Asta 5074 Nodi -18 30 31 32 33 34 36 37 38 39 40 41 -19 - Sez. 9 (Travi_facciata) - Crit. 5

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 109 SLU - Classe 1

Sollecitazioni: N,Ed=774.14 My,Ed=374.24 Mz,Ed=109.73 L=7.00
αmy, αmz, αLT=0.95, 0.95, 0.95
L_{cr}=7.00 Curva b: α_{imp}=0.34 k_c=0.94 ψ=1.75 M,cr=5747.38 λ_{LT}=0.91
$\lambda_{LT,0}$=0.40 Φ_{LT}=0.90 β_{LT}=0.75 f=0.97 χ_{LT}=0.78
Kyy, Kyz, Kzy, Kzz=0.95, 0.57, 0.57, 0.94
Verifica YY: 0.01+0.10+0.03=0.14 (sic.=7.259)
Verifica ZZ: 0.01+0.06+0.05=0.12 (sic.=8.602)

- Verifica freccia massima per soli carichi accidentali (4.2.4.2.2) - CC 165
$f_{Z,L}$=0.55 (L/1282) $f_{Z,G}$=0.01 (L/139810) (sic.=4.273)

- Verifica freccia massima carichi totali (4.2.4.2.2) - CC 165
$f_{Z,L}$=0.55 (L/1280) $f_{Z,G}$=0.20 (L/3424) (sic.=5.120)

Aste in acciaio

Generali

Verifica aste in acciaio
Numero punti di verifica 10
Numero CC da considerare di tipo I 99

Stati limite D.M. 18
Verifiche con EC3 No
Coeff. amplificativo sollecitazioni per effetti del secondo ordine 1.0

Stampe
Verifiche da riportare in relazione Tutte
Stampa dettaglio verifiche No
Specifici

1	2	3	4	5	6	7	8	9	10

Materiali
CNR 10011

Tipo di acciaio									FE430
FE430	FE430	FE430	FE430	FE430	FE430	FE430	FE430	FE430	
D.M. 18									
Tipo di acciaio per profilati a sezione aperta									S275
S275	S275	S275	S275	S275	S275	S275	S275	S275	
								UNI EN 10025-2	UNI EN 10025-2
	UNI EN 10025-2	UNI EN 10025-2	UNI EN 10025-2	UNI EN 10025-2	UNI EN 10025-2	UNI EN 10025-2	UNI EN 10025-2	UNI EN 10025-2	
Tipo di acciaio per profilati a sezione cava									S275H
S275H	S275H	S275H	S275H	S275H	S275H	S275H	S275H	S275H	
								UNI EN 10210-1	UNI EN 10210-1
	UNI EN 10210-1	UNI EN 10210-1	UNI EN 10210-1	UNI EN 10210-1	UNI EN 10210-1	UNI EN 10210-1	UNI EN 10210-1	UNI EN 10210-1	
EC3									
Tipo di acciaio									S275
S275	S275	S275	S275	S275	S275	S275	S275	S275	
-Fy <daN/cmq>									2750.0
2750.0	2750.0	2750.0	2750.0	2750.0	2750.0	2750.0	2750.0	2750.0	
-Fu <daN/cmq>									4300.0
4300.0	4300.0	4300.0	4300.0	4300.0	4300.0	4300.0	4300.0	4300.0	
-Fy,40 <daN/cmq>									2550.0
2550.0	2550.0	2550.0	2550.0	2550.0	2550.0	2550.0	2550.0	2550.0	
-Fu,40 <daN/cmq>									4100.0
4100.0	4100.0	4100.0	4100.0	4100.0	4100.0	4100.0	4100.0	4100.0	
γ M0									1.0
1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
γ M1									1.0
1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
γ M2									1.2
1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	
γ Rd									1.3
1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3	
γ Ov									1.2
1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	
-Considera come elemento esistente (S.L. D.M. 18/EC3)									No
No	No	No	No	No	No	No	No	No	
-Livello di conoscenza									LC1
LC1	LC1	LC1	LC1	LC1	LC1	LC1	LC1	LC1	
-Fattore di confidenza									1.35
1.35	1.35	1.35	1.35	1.35	1.35	1.35	1.35	1.35	

Parametri per analisi pushover
Considera l'asta nel telaio equivalente Si
Si Si Si Si Si Si Si Si Si
-Non sismo-resistente No
No No No No No No No No No

Verifiche di resistenza
Rapporto fra area effettiva e area nominale 1.0
1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Rapporto fra area netta e area nominale 1.0
1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Coeff. di forma intorno all'asse Y 1.0
1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Coeff. di forma intorno all'asse Z 1.0
1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Verifica le bielle solo con sollecitazioni di trazione moltiplicate per Si
Si Si Si Si Si Si Si Si Si
Valutare la τ per torsione nei punti di spigolo (CNR 10011) No
No No No No No No No No No
-Pari a
Stati limite D.M. 18/EC3
-Elemento dissipativo No
No No No No No No No No No
-Effettua le verifiche della gerarchia delle resistenze per strutture intelaiate No
No No No No No No No No No
-Usa classe 1 in pressoflessione deviata se non presente in archivio No
No No No No No No No No No
-Verifica in campo plastico elemento non dissipativo No
No No No No No No No No No
Stati limite D.M. 18
-Usa prescrizioni EC3 quando più dettagliate Si
Si Si Si Si Si Si Si Si Si
-Considera prescrizioni relative ai ponti No
No No No No No No No No No

Verifiche di resistenza sezioni generiche
Spessore nominale <cm> 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
Momento di inerzia torsionale <cm4> 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
Costante di ingobbamento <cm6> 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
Riduzione resistenza flessionale come per sezioni a I No
No No No No No No No No No
Area resistente a taglio in dir. Y locale <cmq> 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
Area resistente a taglio in dir. Z locale <cmq> 0.0
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

Verifiche di deformabilità
Max valore del rapporto tra la luce e la freccia (totale) 250.0
200.0 200.0 250.0 250.0 250.0 200.0 200.0 200.0 200.0
Max valore del rapporto tra la luce e la freccia (solo accidentali) 300.0
250.0 250.0 300.0 300.0 250.0 250.0 250.0 250.0 250.0
Max valore del rapporto tra altezza e spostamento orizz. (aste) 300.0
300.0 300.0 300.0 300.0 300.0 300.0 300.0 300.0 300.0
Max valore del rapporto tra altezza e spostamento orizz. (membrature) 300.0
500.0 500.0 300.0 300.0 300.0 300.0 300.0 300.0 300.0
Considerare anche spostamento relativo nodi per calcolo freccia No
No No No No No No No No No
Considerare solo la verifica di deformabilità delle membrature No
No No No No No Si No No No
Trascura deformazione dovuta al sisma (T.A.) No
No No No No No No No No No

Verifiche di stabilità
Riduzione lunghezza libera d'inflessione
-Distanza fra i nodi dell'asta x
x x x x x x x x x
-Distanza ridotta delle zone rigide moltiplicate per il valore
Tipo di accoppiamento aste composte
-Separate
-Calastrellate
-Imbottite
-Automatico x
x x x x x x x x x
Calcolo momento medio usando valori assoluti Si
Si Si Si Si Si Si Si Si Si
Interasse calastrelli o imbottiture
-Distanza pari a <m>
-Interasse da normativa moltiplicato per il valore 0.80
0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80

-Aste rigidamente collegate
Curva di stabilità (D.M. 18/EC3) Automatica
Automatica Automatica Automatica Automatica Automatica Automatica Automatica Automatica Automatica
Aste laminate Si
Si Si Si Si Si Si Si Si Si
Sigma max amm. senza verifiche di stabilità (CNR 10011) <%> 2.0
2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0
Verifica nei piani principali Si
Si Si Si Si Si Si Si Si Si
Carichi sull'estradosso (CNR 10011) Si
Si Si Si Si Si Si Si Si Si

Verifiche di stabilità asta
Verifiche di stabilità globale nel piano XZ locale Si
Si Si Si Si Si No Si Si
-Coeff. β intorno all'asse Y 0.5
0.5 1.0 2.0 1.0 1.0 1.0 1.0 1.0
Verifiche di stabilità globale nel piano XY locale Si
Si Si Si Si Si No Si Si
-Coeff. β intorno all'asse Z 0.5
0.5 1.0 2.0 1.0 1.0 1.0 1.0 1.0
Verifiche di stabilità flesso - torsionale Si
Si Si Si Si Si Si No Si Si
-Coeff. per calcolo interasse ritegni torsionali 0.5
0.5 1.0 2.0 1.0 1.0 1.0 1.0 1.0 1.0
Eseguire anche le verifiche al punto 7.3.2 (CNR 10011) Si
Si Si Si Si Si Si Si Si Si
Aste inflesse (D.M. 18/EC3)
-Coeff. Ψ per calcolo momento critico
-Valuta in base ai momenti dell'asta x
x x x x x x x x x
-Utilizza valore imposto
-Fattore correttivo di distribuzione K_c 0.9
0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9
-Snellezza di riferimento $\lambda_{LT,0}$ 0.4
0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4
-Coeff. β 0.8
0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8
Aste pressoinflesse (D.M. 18/EC3)
-Considera come molto deformabile a torsione No
No No No No No No No No No
-Fattore correttivo di distribuzione α_{mY}/C_{mY} 0.9
0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9
-Fattore correttivo di distribuzione α_{mZ}/C_{mZ} 0.9
0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9
-Fattore correttivo di distribuzione α_{mLT}/C_{mLT} 0.9 0.9
0.9 0.9 0.9 0.9 0.9 0.9 0.9
Verifiche di stabilità all'imbozzamento (CNR 10011)
-Numero irrigidimenti orizzontali anima 0
0 0 0 0 0 0 0 0 0
-Interasse irrigidimenti verticali anima
-Numero di suddivisioni
-Distanza non inferiore a <cm>
-Pari alla lunghezza dell'asta x
x x x x x x x x x
-Modalità di calcolo σ cr,id
-Normativa
-Massonet x
x x x x x x x x x
-Ballio

Verifiche di stabilità membratura
Massimo numero aste costituenti unica membratura 5
9 5 5 12 1 1 6 1 3
Sforzo normale di verifica
-Massimo valore fra tutte le aste x
x x x x x x x x x
-Media aritmetica dei valori di tutte le aste
-Media pesata di tutte le aste
Contributo eventuali sforzi di trazione No
No No No No No No No No No
Incremento snellezza Si
Si Si Si Si Si Si Si Si Si
Verifiche di stabilità globale nel piano XZ locale Si
Si Si Si Si No No Si No Si
-Coeff. β intorno all'asse Y calcolato in funzione dello sforzo normale
-Coeff. βintorno all'asse Y 0.5
0.5 1.0 2.0 1.0 0.7 1.0
Verifiche di stabilità globale nel piano XY locale Si
Si Si Si Si No No Si No Si

-Coeff. β intorno all'asse Z calcolato in funzione dello sforzo normale
-Coeff. βintorno all'asse Z 0.5
0.5 1.0 2.0 1.0 0.7 1.0
Verifiche di stabilità flesso - torsionale Si
Si Si Si Si No No Si No Si
-Coeff. per calcolo interasse ritegni torsionali 0.5
0.5 1.0 2.0 1.0 0.7 1.0
Membrature inflesse (D.M. 18/EC3)
-Coeff. Ψ per calcolo momento critico
-Valuta in base ai momenti della membratura x
x x x x x x x x x
-Utilizza valore imposto
-Fattore correttivo di distribuzione K_c 0.9
0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9
-Snellezza di riferimento $\lambda_{LT,0}$ 0.4
0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4
-Coeff. β 0.8
0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8
Membrature pressoinflesse (D.M. 18/EC3)
-Considera come molto deformabile a torsione No
No No No No No No No No No
-Fattore correttivo di distribuzione α_{mY}/C_{mY} 0.9
0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9
-Fattore correttivo di distribuzione α_{mZ}/C_{mZ} 0.9
0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9
-Fattore correttivo di distribuzione α_{mLT}/C_{mLT} 0.9 0.9
0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9

Dati per verifiche di resistenza al fuoco
-Tempo di verifica (REI) <minuti> 120.0
120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0
-Fattore di momento uniforme equivalente β M, y 1.1
1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1
-Fattore di momento uniforme equivalente β M, z 1.1
1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1
-Fattore di momento uniforme equivalente β M, LT 1.1
1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1